

Water Cycle Management Study  
Proposed Rural Residential Subdivision  
No.80 Silverdale Road, The Oaks  
23130 – April 2024



# **WATER CYCLE MANAGEMENT STUDY**

**80 SILVERDALE ROAD, THE OAKS**

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**TABLE OF CONTENTS**

<b>EXECUTIVE SUMMARY .....</b>	<b>4</b>
<b>1      INTRODUCTION.....</b>	<b>5</b>
1.1. Siteplus Engagement.....	5
1.2. Scope of Work .....	5
1.3. Subject Land.....	5
<b>2      DATA COLLECTION .....</b>	<b>7</b>
2.1 Topographic Data .....	7
2.2 DEM Development.....	7
<b>3      HYDROLOGICAL MODELLING .....</b>	<b>9</b>
3.1 Design Rainfall.....	9
3.2 Design Rainfall Losses.....	9
3.3 Sub - Catchments .....	12
3.4 Results of Hydrological Modelling .....	13
<b>4      HYDRAULIC MODELLING .....</b>	<b>14</b>
4.1 Modelling Technique .....	14
4.2 Hydraulic Roughness .....	14
4.3 Boundary Conditions.....	17
4.3.1 Inflow Boundary Condition.....	17
4.3.2 2D Downstream Boundary Condition.....	17
4.4 Hydraulic Structures.....	17
<b>5      MODEL RESULTS.....</b>	<b>22</b>
5.1 Existing Model Results.....	22
5.2 Proposed Model Results .....	22
<b>6      FLOOD PLANNING – WOLLONDILLY COUNCIL DCP 23</b>	
6.1 Flood Risk Precinct Definition .....	23
6.2 Floor Levels .....	23
6.3 Flood Compatible Materials.....	23
6.4 Flood Forces .....	23
6.5 Evacuation .....	23
6.6 Flood Affectation .....	24
6.7 Filling of Land Below the Flood Planning Level .....	24
<b>7      FLOOD PLANNING – WOLLONDILLY LEP .....</b>	<b>25</b>
<b>8      ONSITE DETENTION .....</b>	<b>26</b>
8.1 Onsite Detention Requirements .....	26
8.2 Onsite Detention System .....	26
8.3 Proposed Stormwater Design .....	26
<b>9      WATER QUALITY .....</b>	<b>27</b>
9.1 Meteorological Template.....	27

9.2	Source Nodes .....	27
9.2.1	Existing Site.....	27
9.2.2	Urban Node .....	28
9.3	Proposed Development Sources.....	28
9.3.1	Urban Nodes .....	28
9.4	Treatment Nodes .....	29
9.4.1	Infiltration Trench.....	29
9.4.2	Rainwater Tanks .....	29
9.4.3	Sediment Basin .....	30
9.4.4	MUSIC Results.....	30
9.5	Monitoring and Maintenance Procedures .....	30
9.5.1	Swale areas.....	31
9.6	Treatment Device Life Cycle Costings.....	32
9.6.1	Swale systems .....	32
<b>10</b>	<b>CONCLUSION .....</b>	<b>33</b>
	APPENDIX A Site Survey .....	1
	APPENDIX B Flood Mapping .....	2
	APPENDIX C Flood Impact Mapping .....	3
	APPENDIX D Civil Engineering Plans.....	4

**LIST OF TABLES**

Table 3-1 Design Rainfall Losses .....	9
Table 3-2 Existing Sub-Catchment Summary .....	12
Table 3-3 Proposed Sub-Catchment Summary .....	12
Table 3-4 Existing Peak Flow Summary .....	13
Table 3-5 Proposed Peak Flow Summary .....	13
Table 4-1 Land Use Table .....	14
Table 6-1 Floor Level Summary.....	23

**LIST OF FIGURES**

Figure 1-1 Site Location .....	6
Figure 2-1 Catchment Digital Elevation Model.....	8
Figure 3-1 Existing Sub Catchment Plan .....	10
Figure 3-2 Proposed Sub Catchment Plan .....	11
Figure 4-1 Existing Land Use Delineation.....	15
Figure 4-2 Proposed Land Use Delineation .....	16
Figure 4-3 Existing Model Boundary Conditions .....	18
Figure 4-4 Proposed Modelled Boundary Conditions.....	19
Figure 4-5 Existing Hydraulic Structures.....	20
Figure 4-6 Proposed Hydraulic Structures .....	21

## EXECUTIVE SUMMARY

On behalf of Mr and Mrs Nocera C/- Proficient Constructions (Aust) Pty Ltd a flood study has been prepared to accompany the rezoning for the rural residential subdivision at 80 Silverdale Road, The Oaks.

An XP Rafts Hydrological and TUFLOW 2D Hydraulic models were utilised to develop the flood study for the area surrounding the subject site. Model parameters were adopted based on the Draft Wollondilly Shire Flood Study by Advisian, to ensure an accurate and valid model of the Site.

The subject site is influenced by an overland flow path off Browns Road which bisects the site. An existing basin lies at the northern end of the development extents and is to remain. Road grading from Browns Road diverts the existing flow away from the proposed lots via a perimeter road which caters for the 1%AEP flows into the site.

All proposed lots are located outside the proposed 1% AEP flood extents plus 0.5m freeboard. All flood flows are located within the road reserve and outside of the carriage way.

The proposed development will not impact flooding in or surrounding the site as all dwellings and associated works are outside the flood extents. The existing detention basin is to remain and detain flow prior to discharge off the subject site.

Stormwater peak flows and stormwater quality from the proposed development have been considered. TUFLOW has been used for stormwater quantity assessment and the computer model MUSIC (Model for Urban Stormwater Improvement Conceptualisation) has been used for the stormwater quality assessment.

Stormwater peak flows will be controlled via the existing dam, which acts as onsite detention. The dam adequately attenuates post-development flows to pre-development levels.

A concept WSUD strategy for the site has been developed incorporating elements such rainwater tanks, infiltration swales and the existing dam acting as a sediment basin. The strategy has been designed and assessed to meet and comply with Council's Engineering Design Specifications and WSUD guidelines. The WSUD elements will reduce stormwater pollutant generation to the water quality targets specified by Council.

## 1 INTRODUCTION

### 1.1. Siteplus Engagement

Mr and Mrs Nocera C/- Proficient Constructions (Aust) requested a Water Cycle Management Study to support the proposed Rural Residential Subdivision at No.80 Silverdale Road, The Oaks.

### 1.2. Scope of Work

Siteplus determined the following investigations were required to complete a thorough flood study of the site:

- Construct a Hydrological model to determine the critical flow rate for the 1% AEP and PMF (Probable Maximum Flood) event.
- Develop a 2D TUFLOW model to calculate the 1% AEP and PMF flood extents, levels, velocities and hazards for the existing and proposed development scenarios.
- Evaluate the proposal in terms of Wollondilly Shire Council's Development Control Plan 2016 Volume 1 General – Part 8 Flooding;
- Examine existing site to determine how peak flows and mean annual pollutant loads will be controlled to meet Council standards;
- Provide Council with a drainage concept that complies with all relevant Council policies and requirements;
- Assess the proposed storm water quality devices to meet the environmental standards sought by Council;
- Provide maintenance guidelines and procedures to ensure the functional longevity of the stormwater quality system; and
- Prepare a Water Cycle Management Study which summarising the findings of the analysis.

### 1.3. Subject Land

The lot lies upslope to the north of Wattle Creek, a tributary of the Nepean River. The site is surrounded rural residential properties and the Nepean River Riparian Corridor to the east.

Figure 1-1 illustrates the location of the subject site.



Title:  
**Site Location - 80 Silverdale Road, The Oaks**

Figure: **1.1** Rev: **B**



0 100 200 300 400 500 m

**siteplus**

## 2 DATA COLLECTION

### 2.1 Topographic Data

Topographic Data was collated and used for the study which includes:

- 2019, 1.0m DEM, ALS data provided by NSW Government Spatial Services.
- Detailed survey of the site and surround area. Appendix A.

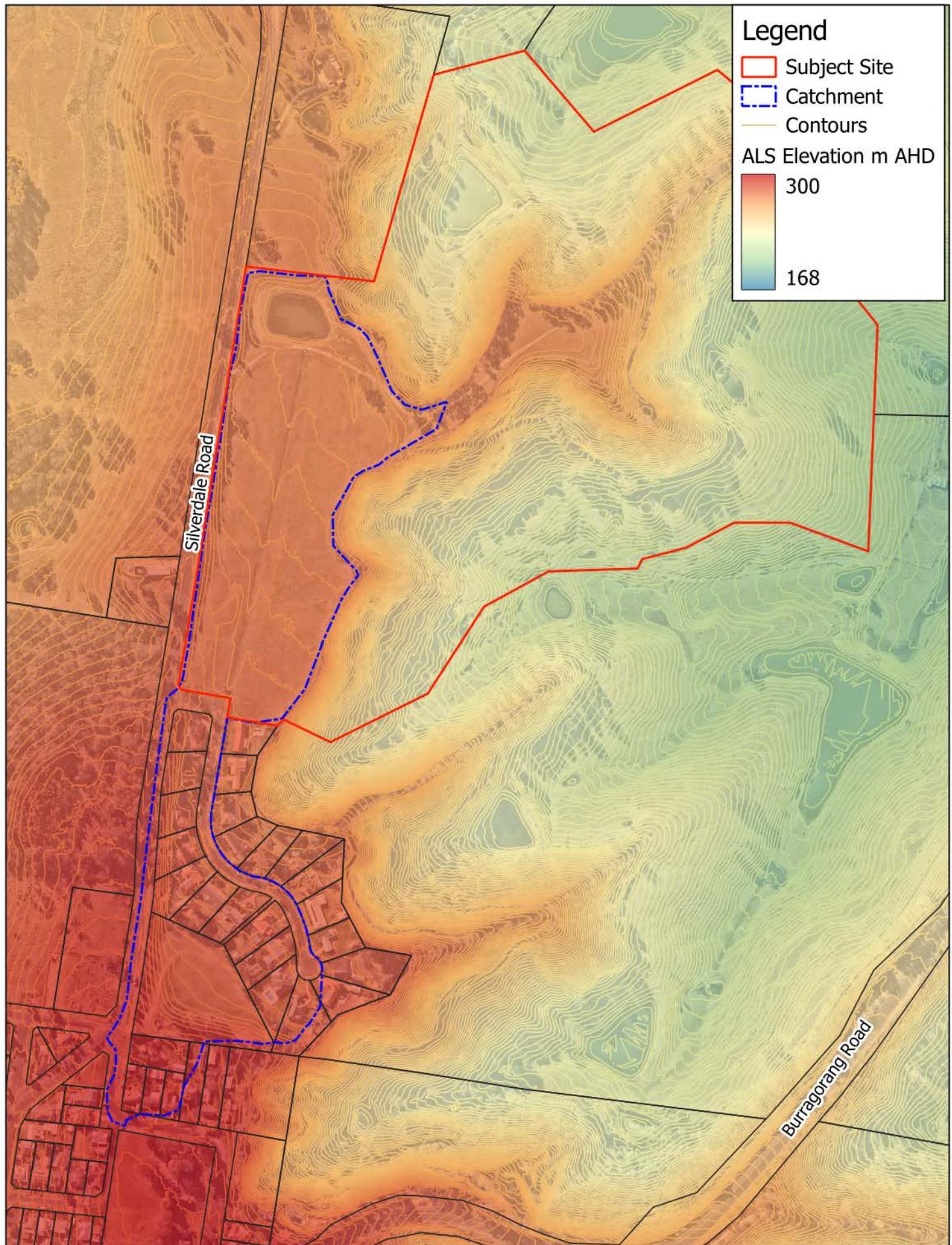
The above sources have been ground proven through onsite delineation.

### 2.2 DEM Development

The DEM data provided by the NSW Government Spatial Service was fed directly into the TUFLOW model and formed the existing topography. Modifications were made to the surface via the site survey to accurately model the existing land topography.

Figure 2-1 shows the ALS data used to define the catchment and sub catchments. The elevation ranges within the catchment from 200m AHD to 300m AHD.

Figure 4-5 illustrates the DEM used within the TUFLOW Model.



Title:  
**Catchment Digital Elevation Model**

Figure: **2.1** Rev: **B**



0

100

200

300

400

500 m

### 3 HYDROLOGICAL MODELLING

XP Rafts was chosen as the hydrological model for the subject study. XP RAFTS has been used in several council adopted flood studies and is considered appropriate for the catchment size and type.

Figure 3-1 and Figure 3-2 Illustrates the contributing sub catchments to the subject site. The sub catchments were defined by the catchment topography and hydraulic structures such as roads and existing overland flow paths.

#### 3.1 Design Rainfall

Using ARR16 design rainfall parameters were utilised for the model with a nearest grid cell latitude of 34.0625(S) and Longitude of 150.5625 (E).

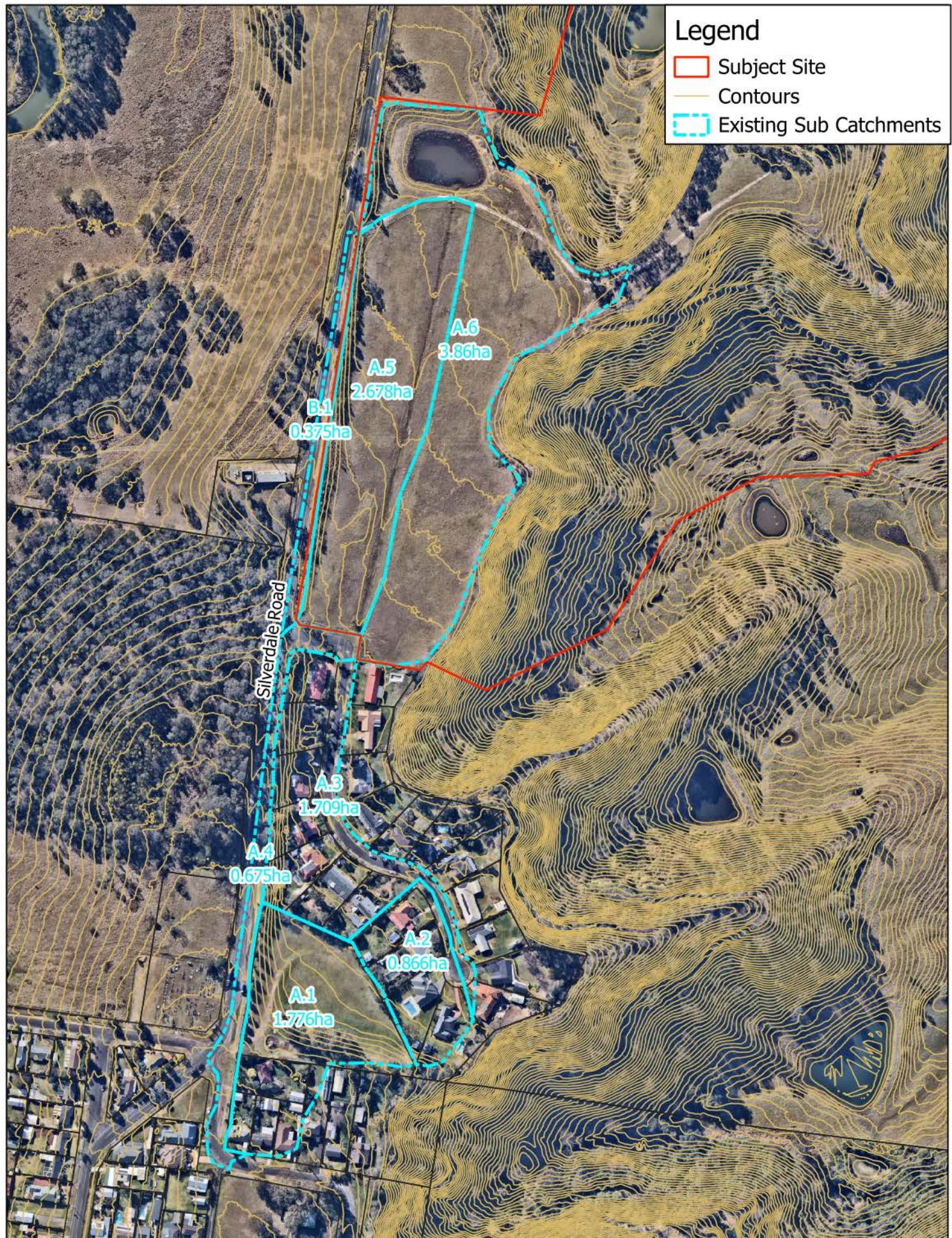
ARR16 East Coast rainfall patterns were produced and used within the model.

#### 3.2 Design Rainfall Losses

Design Rainfall losses were applied to the XP Rafts model as per Table 3-1. These numbers are based on the draft Wollondilly Shire Flood Study by Advision in 2021.

**Table 3-1 Design Rainfall Losses**

<b>Design Flood Event</b>	<b>Loss Parameter</b>	<b>Value (mm/hr)</b>
1% AEP	Initial Loss (Pervious)	12.8
	Initial Loss (Impervious)	1.0
	Continuing Loss (Pervious)	1.56
	Continuing Loss (Impervious)	0.0
PMF	Initial Loss (Pervious)	0.0
	Initial Loss (Impervious)	1.0
	Continuing Loss (Pervious)	1.0
	Continuing Loss (Impervious)	0.0



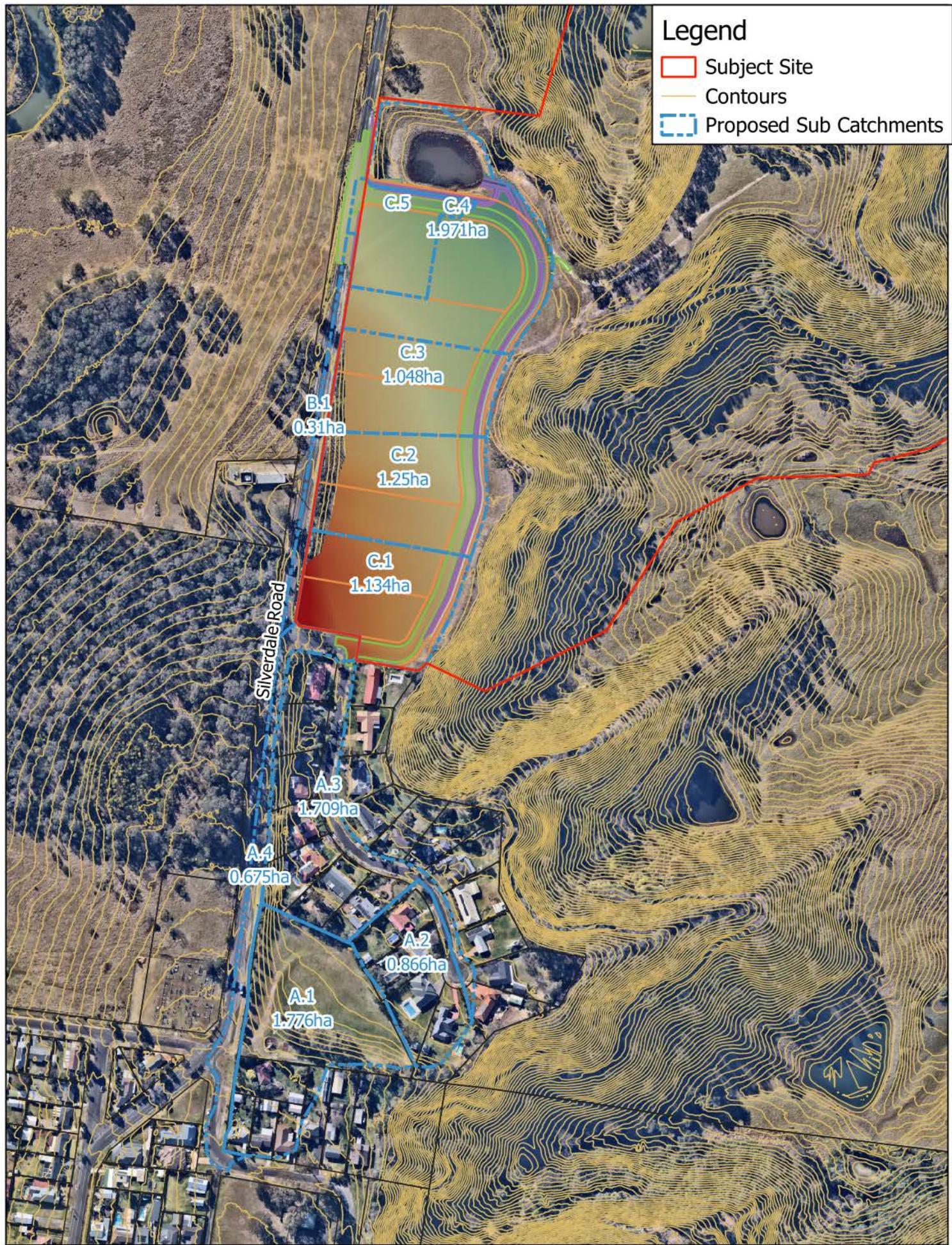
Title:  
**Existing Sub Catchment Plan**

Figure: **3.1** Rev: **B**



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**siteplus**



Title:  
**Proposed Sub Catchment Plan**

Figure: **3.2**

Rev: **B**



0 50 100 150 200 250 m

**siteplus**

### 3.3 Sub - Catchments

The subject catchment was divided into six (6) and ten (10) sub catchments in the existing and proposed scenarios.

In order to identify the catchment boundaries a 1.0m DEM was accessed via ASL 2019 data provided by the NSW Government Spatial Service.

The DEM was used to determine the sub-catchment boundaries and overland flow paths.

**Table 3-2 Existing Sub-Catchment Summary**

Sub Catchment	Area (Ha)	Impervious %	Vectored Slope %	Catchment Manning's 'n' Pervious	Catchment Manning's 'n' Impervious
A.1	1.776	35	6.47	0.05	0.015
A.2	0.866	70	3.90	0.05	0.015
A.3	1.709	70	4.72	0.05	0.015
A.4	0.675	70	3.77	0.05	0.015
A.5	2.678	0	2.44	0.05	0.015
A.6	3.86	0	1.85	0.05	0.015
B.1	0.375	70	2.07	0.05	0.015

**Table 3-3 Proposed Sub-Catchment Summary**

Sub Catchment	Area (Ha)	Impervious %	Vectored Slope %	Catchment Manning's 'n' Pervious	Catchment Manning's 'n' Impervious
A.1	1.776	35	6.47	0.05	0.015
A.2	0.866	70	3.90	0.05	0.015
A.3	1.709	70	4.72	0.05	0.015
A.4	0.675	70	3.77	0.05	0.015
C.1	1.134	40	1.08	0.05	0.015
C.2	1.25	40	4.55	0.05	0.015
C.3	1.048	40	4.27	0.05	0.015
C.4	1.97	40	2.75	0.05	0.015
C.5	0.624	40	2.40	0.05	0.015
B.1	0.375	70	2.07	0.05	0.015

### 3.4 Results of Hydrological Modelling

Numerous durations were modelled ranging from 10min to 4.5hrs for the 1% AEP event.

Based on ARR16 procedures the median storm from each sub catchment was selected and hydrograph exported into the TUFLOW Model. The results are summaries in Table 3-4 below.

The critical storm duration during the 1% AEP and PMF events were 10 minutes and 30 minutes, respectively.

**Table 3-4 Existing Peak Flow Summary**

SUB Catchment	XP RAFTS Peak 1% AEP Flowrate (m <sup>3</sup> /s)	XP RAFTS Peak 1% AEP Climate Flowrate (m <sup>3</sup> /s)	XP RAFTS Peak PMF Flowrate (m <sup>3</sup> /s)
A.1	1.061	1.306	3.855
A.2	0.467	0.638	2.084
A.3	1.186	1.259	3.931
A.4	0.364	0.497	1.641
A.5	1.435	1.965	4.269
A.6	2.386	2.832	5.862
B.1	0.233	0.276	0.875

**Table 3-5 Proposed Peak Flow Summary**

SUB Catchment	XP RAFTS Peak 1% AEP Flowrate (m <sup>3</sup> /s)	XP RAFTS Peak 1% AEP Climate Flowrate (m <sup>3</sup> /s)	XP RAFTS Peak PMF Flowrate (m <sup>3</sup> /s)
A.1	1.061	1.306	3.855
A.2	0.467	0.638	2.084
A.3	1.186	1.259	3.931
A.4	0.364	0.497	1.641
A.5	1.435	1.965	4.269
A.6	2.386	2.832	5.862
B.1	0.233	0.276	0.875
C.1	0.610	0.919	2.304
C.2	0.670	0.797	3.020
C.3	0.563	0.771	2.472
C.4	1.069	1.449	4.440
C.5	0.335	0.459	1.488

## 4 HYDRAULIC MODELLING

### 4.1 Modelling Technique

Siteplus, has adopted a 2D hydrodynamic numerical model as they are currently the most accurate, cost effective and efficient tools to predict flood behaviour.

For this Study TUFLOW was chosen for the modelling for the following reasons:

- Accurately representation of the overland flow paths.
- Produces high quality map outs.
- Is widely accepted by councils as the preferred 2D model.
- Utilised by the Wollondilly Shire Flood Study by Advison in 2021.

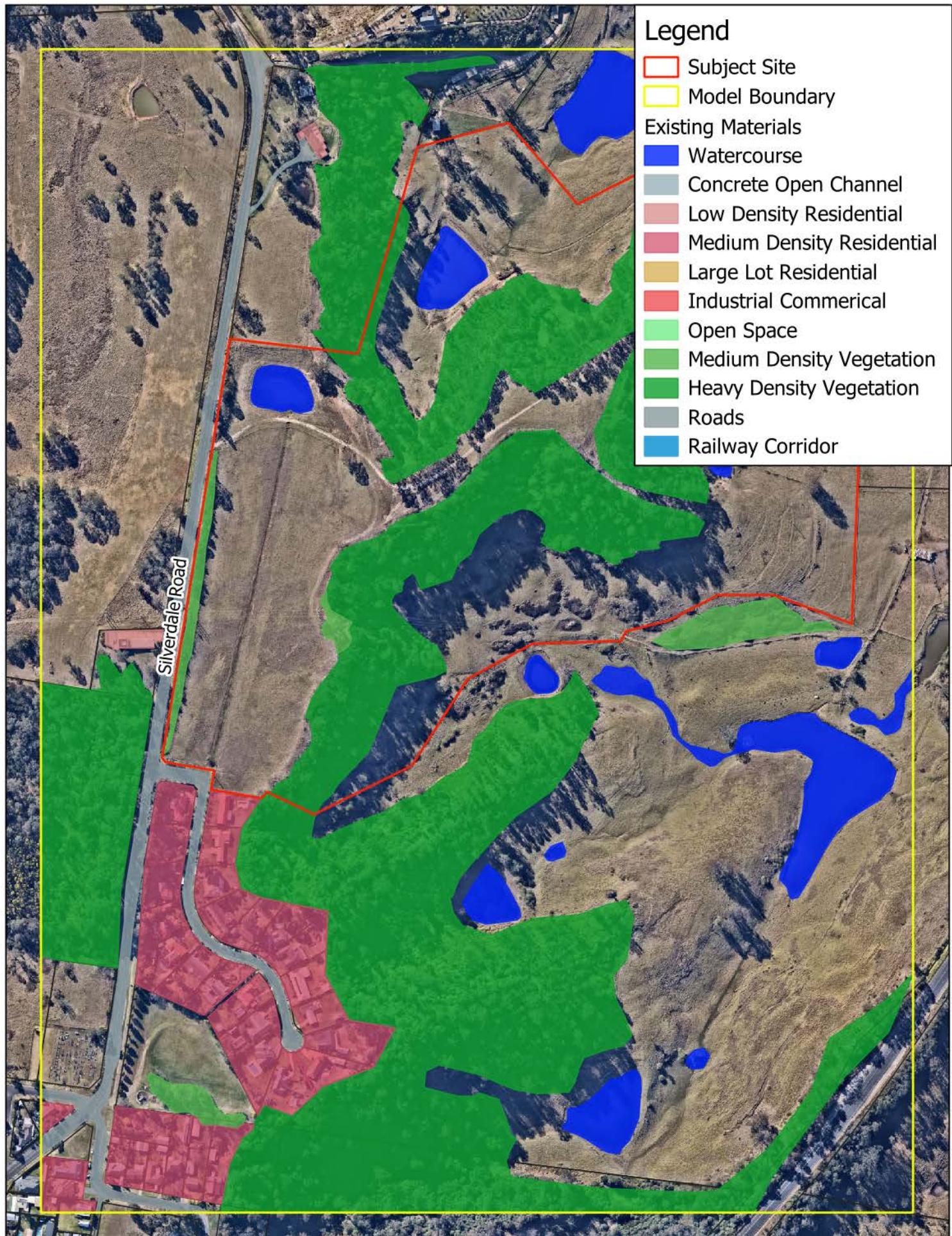
### 4.2 Hydraulic Roughness

Roughness coefficients represent the resistance to flood flows in channels and floodplains. The land use delineation for the model is based on aerial photography and a detailed site survey. The land use delineation used in the TUFLOW model is presented in Figures 4-1 and 4-2.

The adopted depth varied Manning's 'n' roughness coefficients for the land uses within the 2D hydraulic model extent are listed in Table 4-1.

**Table 4-1 Land Use Table**

Material	Depth 'y1'	Manning's 'n1'	Depth 'y2'	Manning's 'n2'
Watercourses	0.5	0.1	1.0	0.04
Medium Density Residential	0.15	0.2	0.3	0.1
Medium Density Vegetation	0.15	0.16	0.3	0.08
Road Corridor	0.1	0.16	0.2	0.08
Open Space	0.1	0.06	0.2	0.04
Rock Lined Channel	-	0.06	-	-
Unshaded areas of Figure 4-1 are modelled as Open Space.				



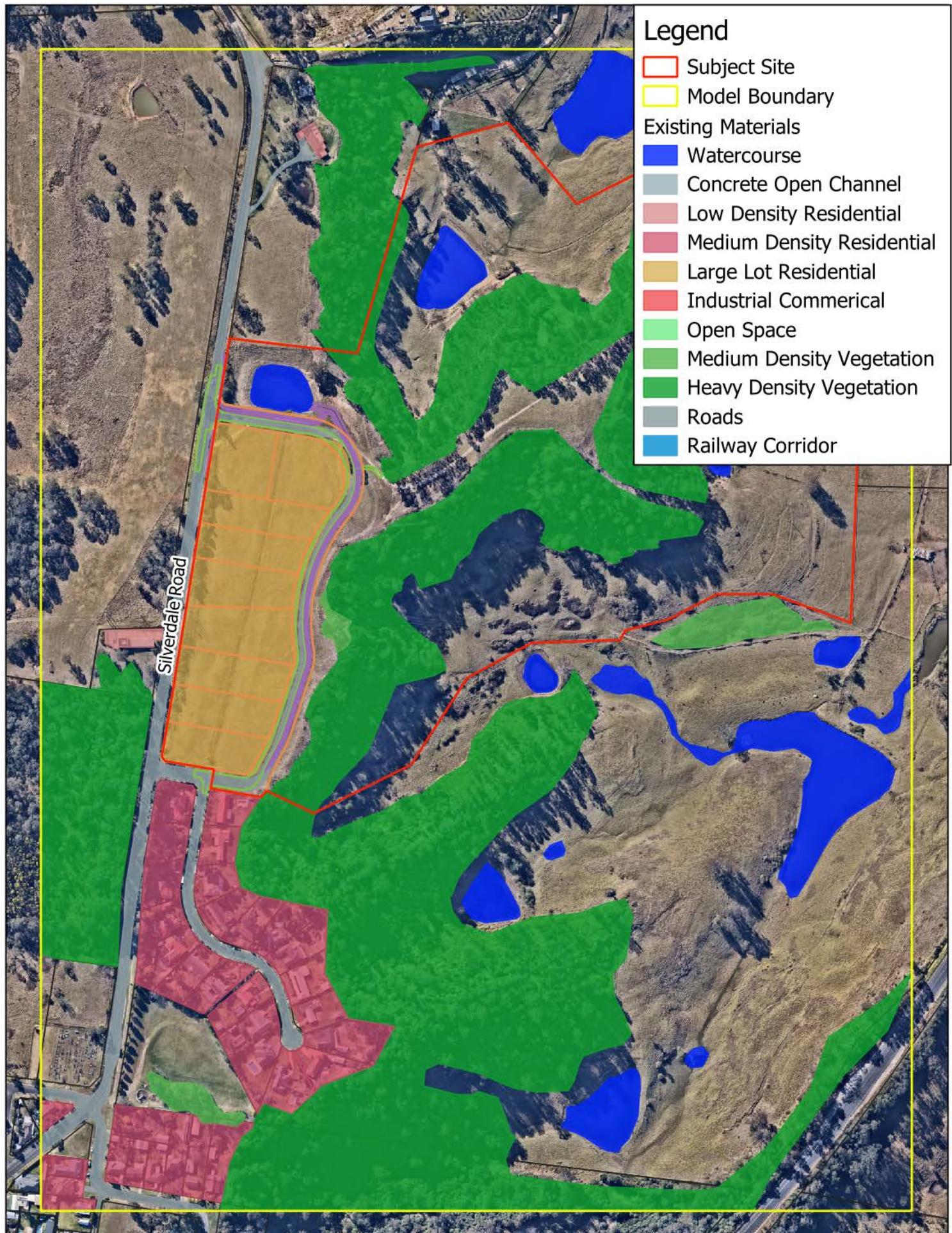
Title:  
**Existing Land Use Delineation**

Figure: **4.1** Rev: **B**



0 50 100 150 200 250 m

**siteplus**



Title:  
**Proposed Land Use Delineation**

Figure: **4.2** Rev: **B**



0 50 100 150 200 250 m

**siteplus**

### **4.3 Boundary Conditions**

Inflow and outflow boundary conditions are required for the TUFLOW model.

The TUFLOW model created for the subject site includes three (3) boundary conditions, including:

1. Inflow hydrographs; and
2. Downstream slope boundary downstream of the site.

#### **4.3.1 Inflow Boundary Condition**

To increase the stability of the model and reduce unnecessary run times the upstream catchments were modelled in XP RAFTS and applied as an inflow hydrograph at the appropriate location as shown in Figure 4-4.

The model covers the entire upstream catchment which is approximately 400m south of subject site. The upstream inflow locations allow for the best representation of overland flow impacting the site from the upstream sub catchments.

#### **4.3.2 2D Downstream Boundary Condition**

A 2D downstream boundary condition has been applied to the model. The purpose of this boundary is to allow water to flow out of the model, replicating flows in a flood event. The location of the downstream boundary is 500m downslope of the proposed subdivision which ensures any affectation by the development is fully modelled and the downstream boundary has no impact on flooding within the site.

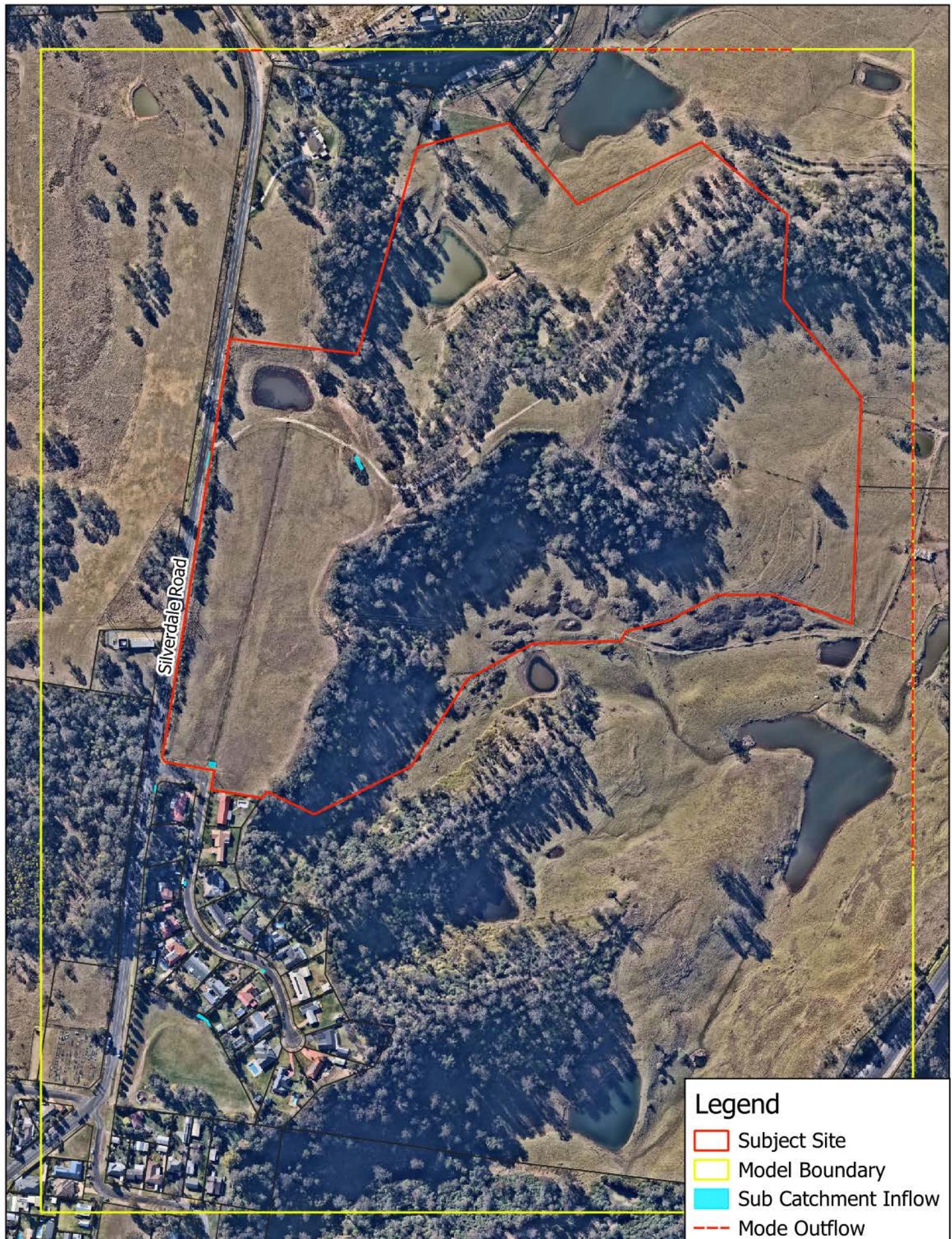
The location of the downstream boundaries are shown within Figure 4-4.

A slope boundary condition was used on Werombi Road to replicate flow leaving the model west to Wattle Creek the boundary condition has an effective slope of 1%.

### **4.4 Hydraulic Structures**

Existing pit and pipe network was modelled within the subject model. Road drainage was modelled as 1d pipe networks with 2d links at the headwalls. Blockage factors were applied in the pipe network.

All pipes within the model have been modelled in both blocked and unblocked scenarios. The blocked scenario blocked all pipes within the model by 60%. With the maximum results from each scenario adopted throughout the model.



**Legend**

- Subject Site (Red Box)
- Model Boundary (Yellow Dashed Line)
- Sub Catchment Inflow (Cyan Arrows)
- Mode Outflow (Dashed Red Line)

Title:  
**Existing Model Boundary Conditions**

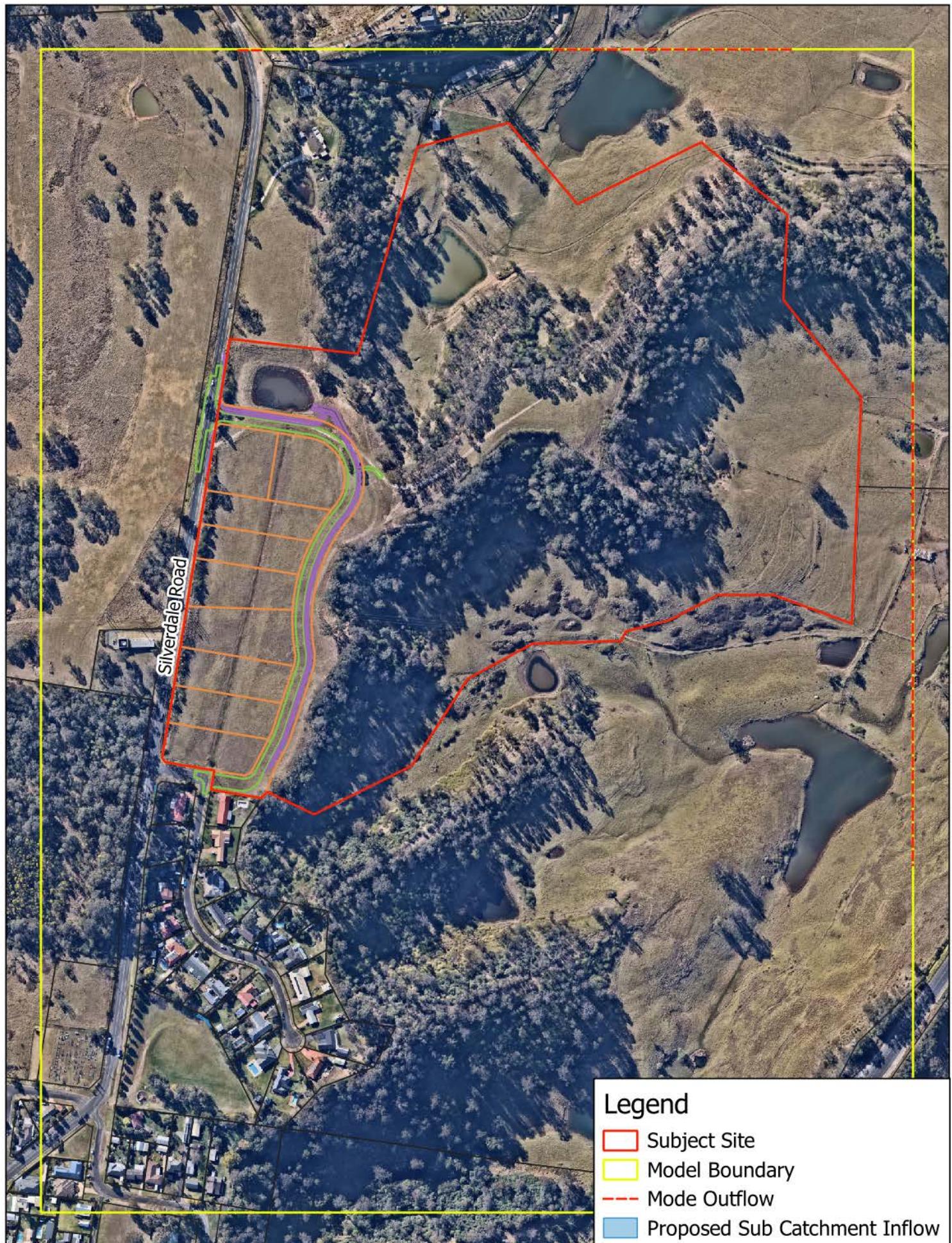
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Title:

### Proposed Model Boundary Conditions

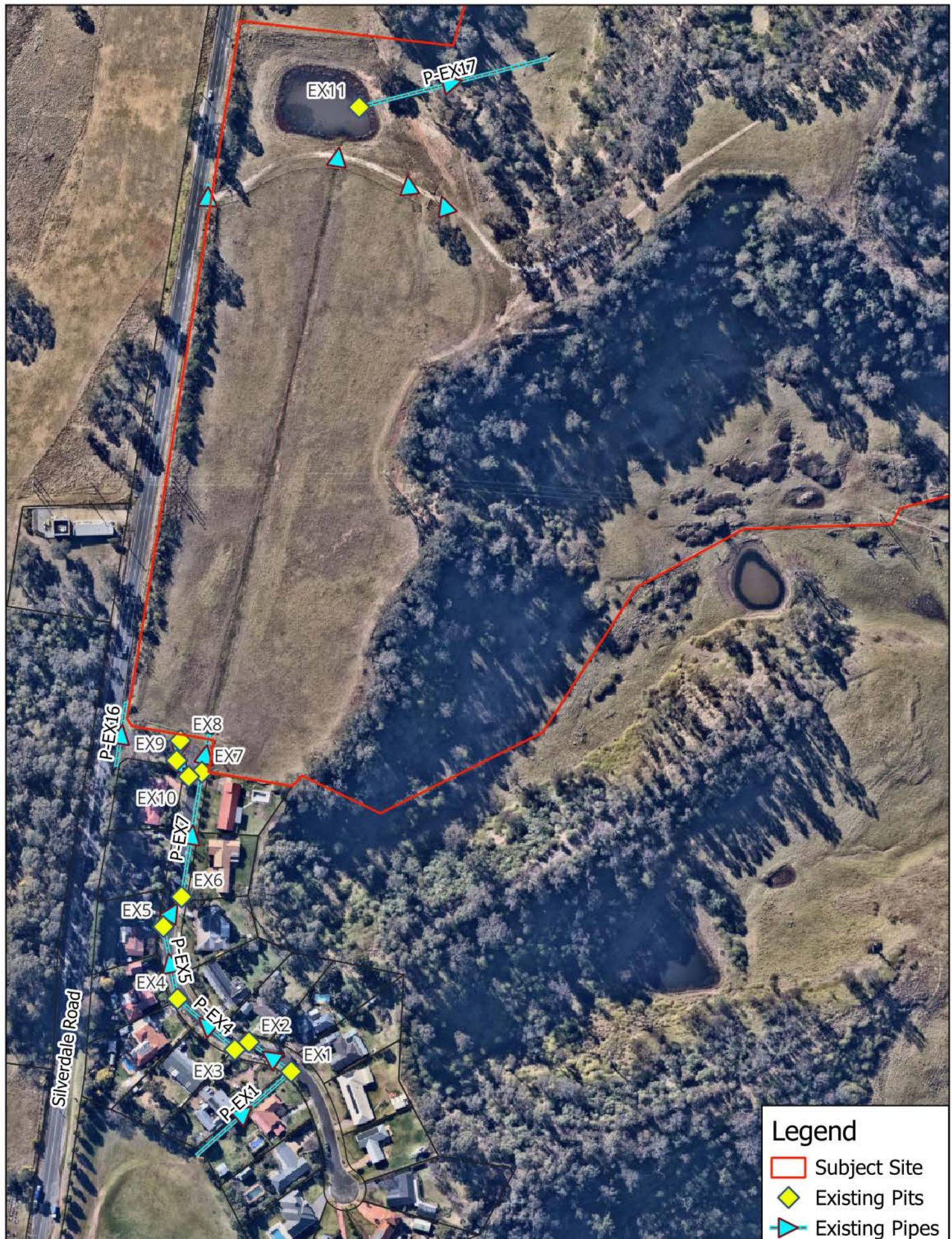
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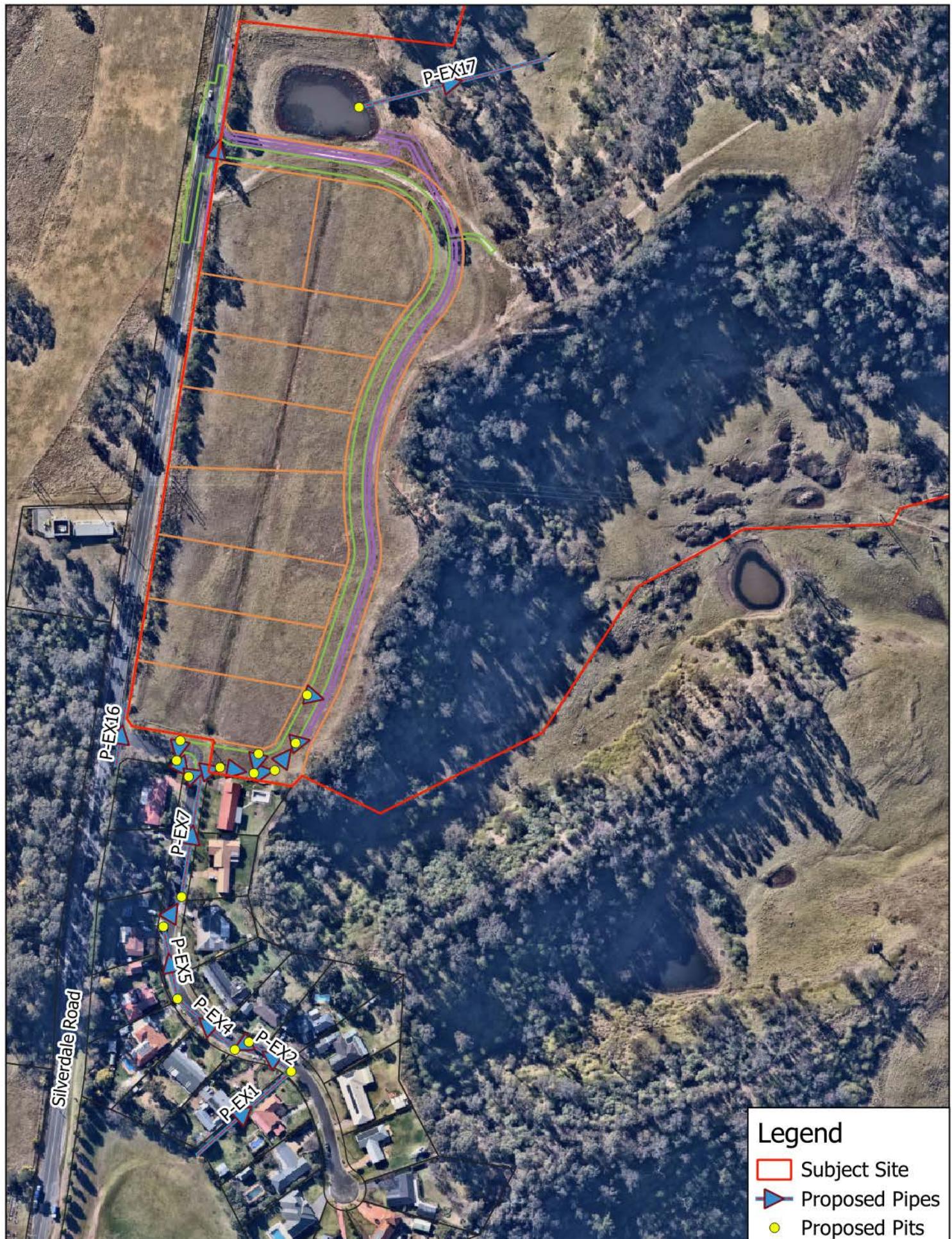
Title:  
**Existing Hydraulic Structures**

Figure: **4.5** Rev: **B**



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**siteplus**



Title:  
**Proposed Hydraulic Structures**

Figure: **4.6** Rev: **B**



0 50 100 150 200 250 m

**siteplus**

## 5 MODEL RESULTS

Flood mapping is shown in Appendix C.

### 5.1 Existing Model Results

Flooding of the subject site is bisected by a single overland flow path from Browns Road north to the existing dam and detention basin.

Flows overtop the existing road reserve from Browns Road in both a north and east direction. The existing grass lined channel contains the 1% AEP flows to the existing dam at the northern end of the proposed subdivision.

Two smaller table drains with the development extent convey minor flows to the existing dam. However, due to the table drains capacity sheet flow overtops the drain and falls east down the steep embankment to the existing drains.

### 5.2 Proposed Model Results

The proposed road intersection with Browns Road. Directs overland flow from Browns Road east to a new roadside swale on the eastern extends of the development area. The roadside swale has been designed to cater for the 1%AEP flow and directs all of the upstream catchment into the existing dam and detention storage system at the northern end of the development extents.

## 6 FLOOD PLANNING – WOLLONDILLY COUNCIL DCP

Using Wollondilly Shire Councils Development Control Plan 2016 Volume 1 – General, Part 8 – Flooding. The following section addresses each of the flood planning controls within the DCP.

### 6.1 Flood Risk Precinct Definition

Based on the Siteplus Flood Study results, the proposed site is located within the Flood Planning Area (1% AEP plus 0.5m) and subject site contains both low and medium hydraulic hazard flood waters. Therefore, the site is to be considered within a Medium Flood Risk Precinct.

### 6.2 Floor Levels

Only lots 101 and 109 are flood control lots as they are affected by PMF flood waters. Floor levels are proposed 500mm above the 1% AEP level as shown in Table 6-1.

**Table 6-1 Floor Level Summary**

Proposed Lot	1% AEP Level (m AHD)	Flood Planning Level (m AHD)	PMF flood level (m AHD)
101	281.37	281.87	281.50
109	278.09	278.59	278.12

### 6.3 Flood Compatible Materials

Flood compatible materials will be provided up and including the flood planning level. All structures will need to be constructed of either reinforced concrete or masonry. This only applies to lots 101 and 109 as the lots are impacted by the PMF flood extents. The remaining dwellings are greater than 0.75m above the flood planning level and PMF flood level.

### 6.4 Flood Forces

The dwelling proposed on lot 101 and 109, will need to be conducted by registered structural engineer to analyse the forces of floodwaters, debris and buoyancy.

### 6.5 Evacuation

During the 1% AEP and PMF flood events results illustrate that access to Browns Road and Silverdale Road is achievable from the proposed development. Only in the PMF do occupants need to travel through safe H1 floodwaters. Therefore, all the proposed lots can be evacuated safely during all storm events.

## 6.6 Flood Affectation

Appendix C and D illustrates that the proposed development results in no changes in flood behaviour or increases in levels will result from the development.

## 6.7 Filling of Land Below the Flood Planning Level

Based on the results illustrated in Appendix C and D the following conclusions can be made:

- i. Accumulative impacts are negligible as the proposed lots are outside the 1%AEP flood extents.
- ii. Flood storage has been maintained as the dams are to be maintain onsite.
- iii. No surrounding properties are impacts by either an increased hazard or flood level.
- iv. No increased flood liability occurs surrounding the site.

## 7 FLOOD PLANNING – WOLLONDILLY LEP

Referring to the Wollondilly Local Environment Plan 2011, clause 5.21 Flood planning, the following section addresses each of the flood planning requirements.

### (2)(a) Flood Function and Behaviour Compatibility

All of the proposed dwellings are located out of the extents of the 1%AEP. The PMF flooding isn't obstructed the flood behaviour on the land is maintained post development.

### (2)(b) Potential Flood Affectation of Other Developments or Properties

All of the proposed dwellings are located out of the extents of the 1%AEP extents. Therefore, no change to the hazard zones occurs with no increase in hazard category over the study area.

### (2)(c) Safe Occupation and Efficient Evacuation

Safe access for all the proposed lots can be achieved through safe flood waters 0.1m deep during the PMF flood event on Brown Road. Flood free access has been provided to Silverdale Road. Egress to Silverdale Road during a PMF event is safe and allows occupants from all lots to exit the site safely during the PMF event.

Appendix C illustrates the area identified has no vulnerability constraints and is safe for wading.

### (2)(d) & (3)(c) Risk Management Measures

The flood planning controls outlined in the Wollondilly Shire Council's DCP have been strictly followed to ensure the appropriate flood risk mitigation measure have been implemented.

### (2)(e) Environmental Affect

The proposed development will not increase the amount of erosion, siltation, destruction to riparian vegetation or reduction in the stability of riverbanks or watercourses, in comparison to the existing development.

## 8 ONSITE DETENTION

### 8.1 Onsite Detention Requirements

Wollondilly Council requires the peak flow rate of stormwater runoff in the post-developed state to be no more than the pre-developed state. This condition is to be met with the use of onsite detention storage.

### 8.2 Onsite Detention System

To reduce the peak flows leaving the site to pre-development levels, an existing dam at the northern end of the site will be utilised and act as onsite detention.

### 8.3 Proposed Stormwater Design

The existing contours of the site showed a number of natural sub-catchments within the development site. An existing swale bisects the site draining to an existing dam.

For the proposed development, the existing swale is to be removed, and water from the proposed subdivision is to be conveyed via a roadside swale which drains the existing dam. All lots within the proposed development are graded such that all stormwater runoff will discharge to the roadside swale via pipe outlets with scour protection.

The invert of the existing dam is required to be lowered to RL. 272.967m AHD to allow 1% fall for the upstream swale. An existing pit with a Ø375mm outlet pipe is to be maintained within the existing dam and is utilised to discharge water from the dam.

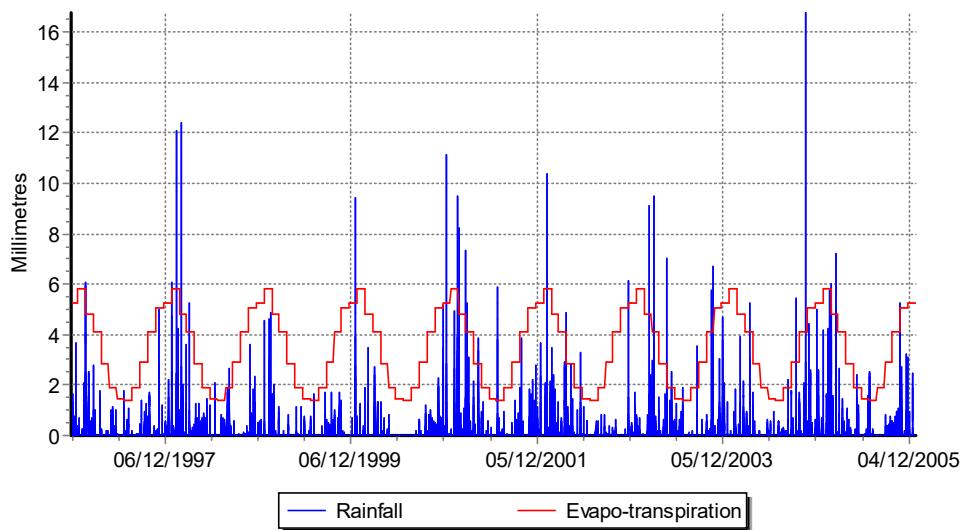
Post development flows were input into the TUFLOW model with increased impervious areas. The flood impact mapping indicates that post development flows were attenuated to pre-development levels and shows no adverse impacts downstream of the subject site.

Refer to impact mapping in Appendix C for details. The Civil Engineering Plans are included in Appendix D illustrates the above features.

## 9 WATER QUALITY

### 9.1 Meteorological Template

MUSIC requires historical rainfall data to determine the mean annual pollutant loadings leaving the site. The subject site is closest to Penrith rainfall gauge where the appropriate corresponding data has been used from 1997 to 2005.



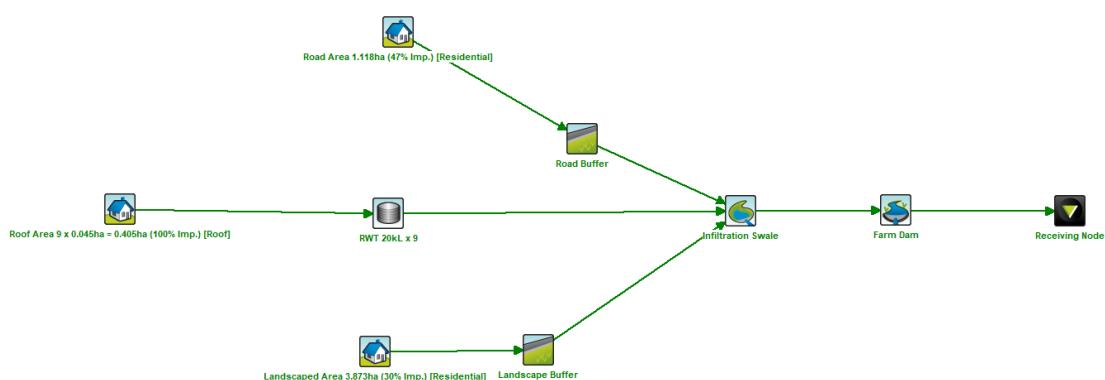
### 9.2 Source Nodes

#### 9.2.1 Existing Site

The existing site has been assumed to produce similar pollutants as residential development with the corresponding impervious areas. The residential parameters have been used from the Draft Western Sydney MUSIC modelling guidelines.

### 9.2.2 Urban Node

The existing and proposed site has been modelled within MUSIC as an urban node with the required residential parameters. Due to the current use of the site it has been assumed that the site will produce similar gross pollutants, suspended solids, nitrogen and phosphorus as roof and paved surfaces as per the modelling guidelines. The MUSIC model is shown below.



### 9.3 Proposed Development Sources

#### 9.3.1 Urban Nodes

The site has been divided into three residential catchments that all drain to the proposed infiltration trench. The three catchments represent the main catchment areas within the site namely roof, road reserve and landscaped areas. The catchment areas have been divided up based on the input parameters required for the MUSIC modelling Guidelines with the zoning areas of the catchments forming the model as shown in Figure 3.

Each urban node has a calculated impervious percentage based on the impervious surface areas within each catchment. The roof, road reserve and landscape catchments have been modelled as 100%, 47%, 30% impervious respectively.

## 9.4 Treatment Nodes

### 9.4.1 Infiltration Trench

Infiltration trenches are used to slow down flow, allow sediment to drop out and allow low flows to infiltrate.

The proposed road contains a 6.5m wide swale with a 0.7m deep infiltration trench at the base. All stormwater runoff from the proposed developments discharges to these infiltration trenches and is conveyed to the existing dam.

### 9.4.2 Rainwater Tanks

Rainwater tanks are used to collect roof runoff for reuse, reduce stormwater runoff volumes and also remove pollutants.

The sizing of the tanks was based on the table outlined in Wollondilly Council's WSUD document. The assumed roof size of each lot was estimated to be 450m<sup>2</sup>. From Council's table, a minimum average daily demand was calculated to be 2,700 L/day.

The minimum size of the rainwater tanks for each lot is to be 18,000 L. 20,000 L tanks have been proposed for each lot.

#### 9.4.3 Sediment Basin

For this development application the dam will be acting as a single sediment basin. The treatment train prior to discharging to the basin ensures that water entering the permanent water body is of very good quality. The swales with infiltration trenches are to be planted out to landscape architects' requirements.

#### 9.4.4 MUSIC Results

	Sources	Residual Load	% Reduction
Flow (ML/yr)	39.6	13.4	66.2
Total Suspended Solids (kg/yr)	5440	399	92.7
Total Phosphorus (kg/yr)	10.2	1.79	82.4
Total Nitrogen (kg/yr)	81.9	21.7	73.5
Gross Pollutants (kg/yr)	907	0	100

The results confirm that the proposed swales, rainwater tanks, and dam have an impact on the water quality discharging from the site. Improvements are achieved for all pollutants.

The above table demonstrates that the results in fact improve the quality of stormwater runoff over the existing situation. There are benefits across the full suite of pollutants modelled.

#### 9.5 Monitoring and Maintenance Procedures

Monitoring and maintenance of water sensitive urban design control is critical to ensure their performance is retained throughout its life cycle. Unmaintained stormwater quality controls can fail leading to an increase of pollutant loads on receiving waters. The following section provides a guide into the monitoring and maintenance of both the rainwater tanks and swale proposed within the development.

### 9.5.1 Swale areas

Predictive and regular inspections should be carried out on a regular basis for each swale system. The predictive inspection is based on a storm event that enables sediment transport roughly 35mm.

The performance of the swale system can be based on the following performance indicators:

- Pounding Time, a maximum of 12 hours.
- Even flow distribution across the filter area. No concentrated flow paths should be present.

During the vegetation establishment period the systems should be inspected every 3 months or after a major rainfall event. During the establishment period the following should be monitored:

- Pounding, clogging or blockage of filter media. Untreated water should not be pooling on the surface of the system for extended periods of time.
- Vegetation and density of plants should be at the desired level. No bare patches or sand filter media should be visible on the surface of the system.
- Outlet should be free of debris and free flowing.
- Structures such as pits and weirs should be clear of debris and functioning correctly.
- Any litter should be removed from the filter area.
- Remove all weeds from both the batter slope and filter area. This should be carried out by hand or with targeted herbicide.
- All sedges and native grasses should be maintained or trimmed at an approximately 200mm high to ensure that both fuel load requirements and water treatment is constant.

(Upper Parramatta River Trust, 2004)

After plants are established correct monitoring and maintenance of the systems can be reduced to a 6 monthly interval. During these inspections the following activities should be recorded and documented:

- Maintain free flow through the system.

- Maintain the surface vegetation as vigorous plant growth is important for treatment. This includes scheduled watering in dry periods.
- Prevent undesired growth of weeds and vegetation.
- Removal of debris and sediment.
- Any litter should be removed from the filter area.
- Remove all weeds from both the batter slope and filter area. This should be carried out by hand or with targeted herbicide.
- Remove excess or dead plant material which will increase the nutrient load on the system.

(Upper Parramatta River Trust, 2004)

## 9.6 Treatment Device Life Cycle Costings

### 9.6.1 Swale systems

The following preliminary costings are based on the standard rates applied by MUSIC with a 25yr renewal period and a total life cycle length of 50yrs.

The initial cost includes complete commissioning of the system, however it does not allow for rock excavation. The cost of each swale is detailed in the table below.

Structure	Area (m <sup>2</sup> )	Life Cycle Cost	Initial cost	Maintenance Cost (yr)
Swale	258	\$245,938	\$72,000	\$8,425

## 10 CONCLUSION

Mr and Mrs Nocera C/- Proficient Constructions (Aust) is seeking a rezoning approval for a proposed rural residential subdivision at No.80 Silverdale Road, The Oaks. The site contains an existing overland flow path and is therefore subject to the Wollondilly Shire Council flood planning controls.

The following conclusions can be made regarding the water cycle management study:

- All of the proposed lots are located outside the of 1%AEP flood extents.
- Proposed habitable floor levels are to be a minimum of 0.5m above the 1% AEP flood level.
- During the PMF occupants from the proposed lots can safely access Silverdale Road which is floor free.
- The existing Dam attenuates flow from the development in its current state and leads to no increases in flood levels or hazard downstream of the development.
- The existing dam (OSD) adequately attenuates the post-development flows to pre-development levels.
- The proposed stormwater treatment measures effectively remove pollutants to Council requirements.

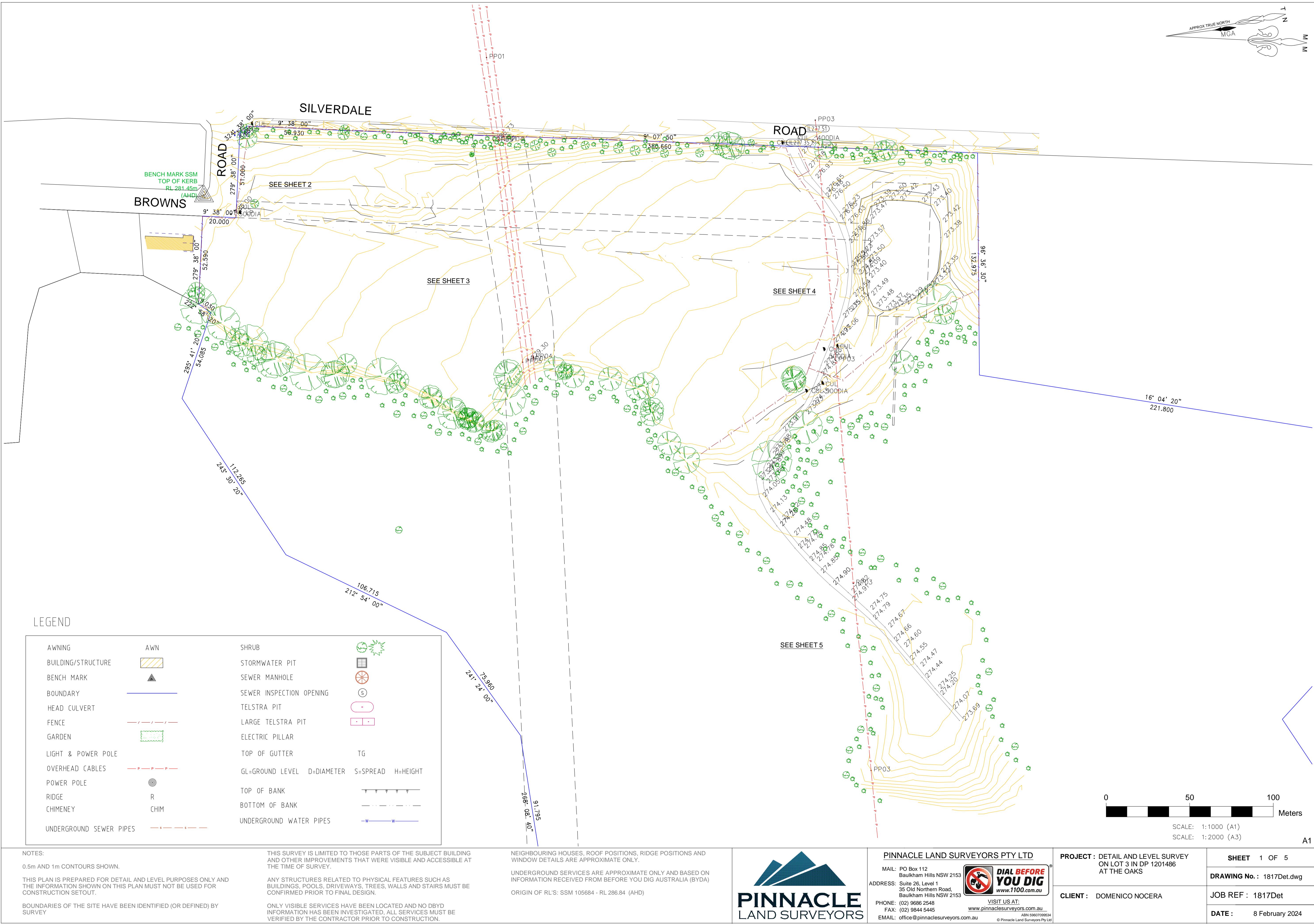
The flood extents are graphically illustrated in Appendix C.

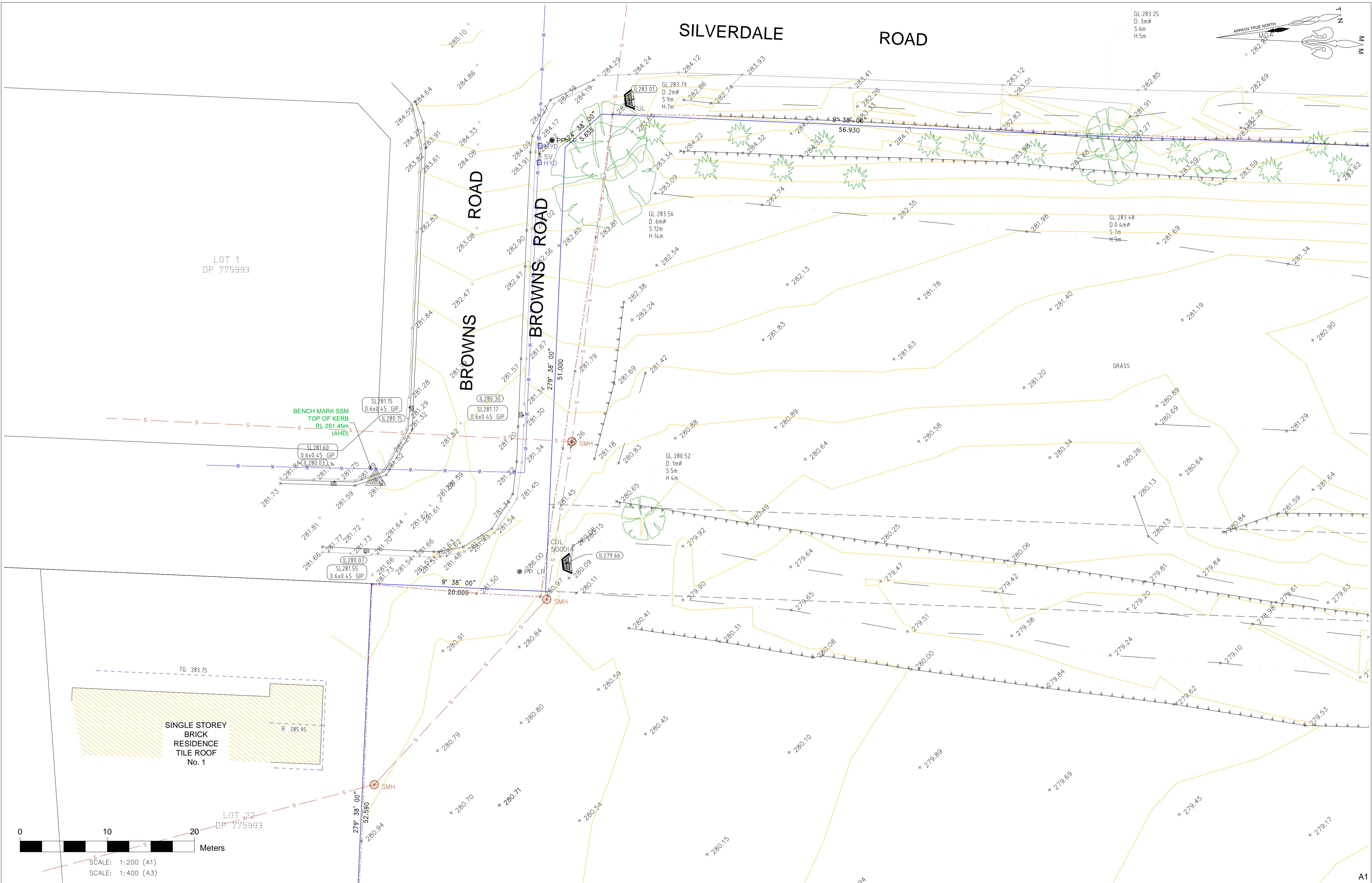
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## **APPENDIX A**

### **Site Survey**

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NOTES:

THIS PLAN IS PREPARED FOR DETAIL AND LEVEL PURPOSES ONLY AND THE INFORMATION SHOWN ON THIS PLAN MUST NOT BE USED FOR CONSTRUCTION SETOUT.

BOUNDARIES OF THE SITE HAVE BEEN IDENTIFIED (OR DEFINED) BY SURVEY

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UNDERGROUND SERVICES ARE APPROXIMATE ONLY AND BASED ON

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ORIGIN OF RL'S: SSM 105684 - RL 286.84 (AHD)



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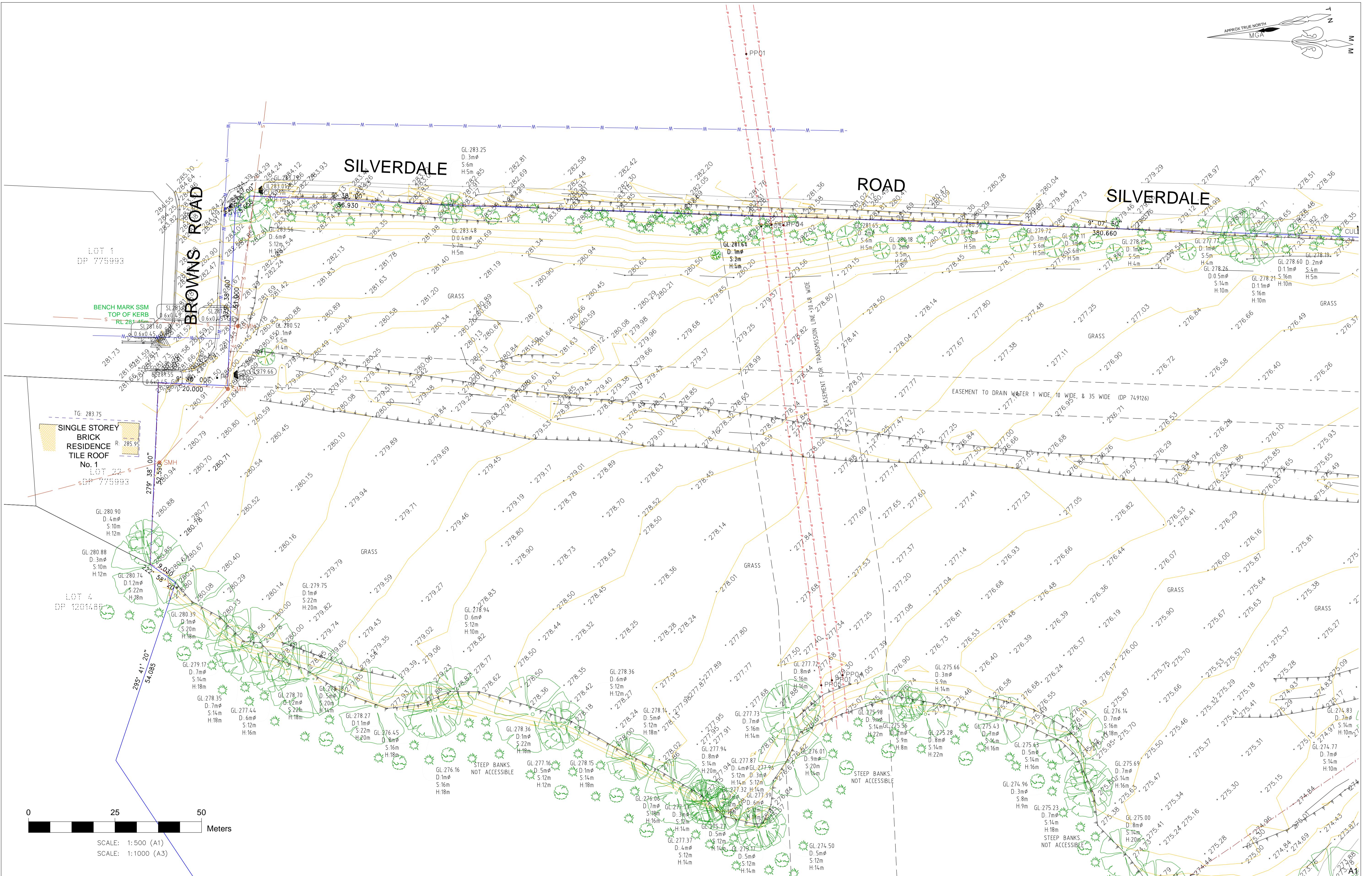
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ABN 59607099534

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**ECT : DETAIL AND LEVEL SURVEY  
ON LOT 3 IN DP 1201486  
AT THE OAKS**

DRAWING NO.: 1817Det.dwg	
NAME : MR & MRS NOCERA	JOB REF : 1817Det
	DATE : 8 February 2024



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ORIGIN OF RL'S: SSM 105684 - RL 286.84 (AHD)



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**PROJECT : DETAIL AND LEVEL SURVEY  
ON LOT 3 IN DP 1201486  
AT THE OAKS**

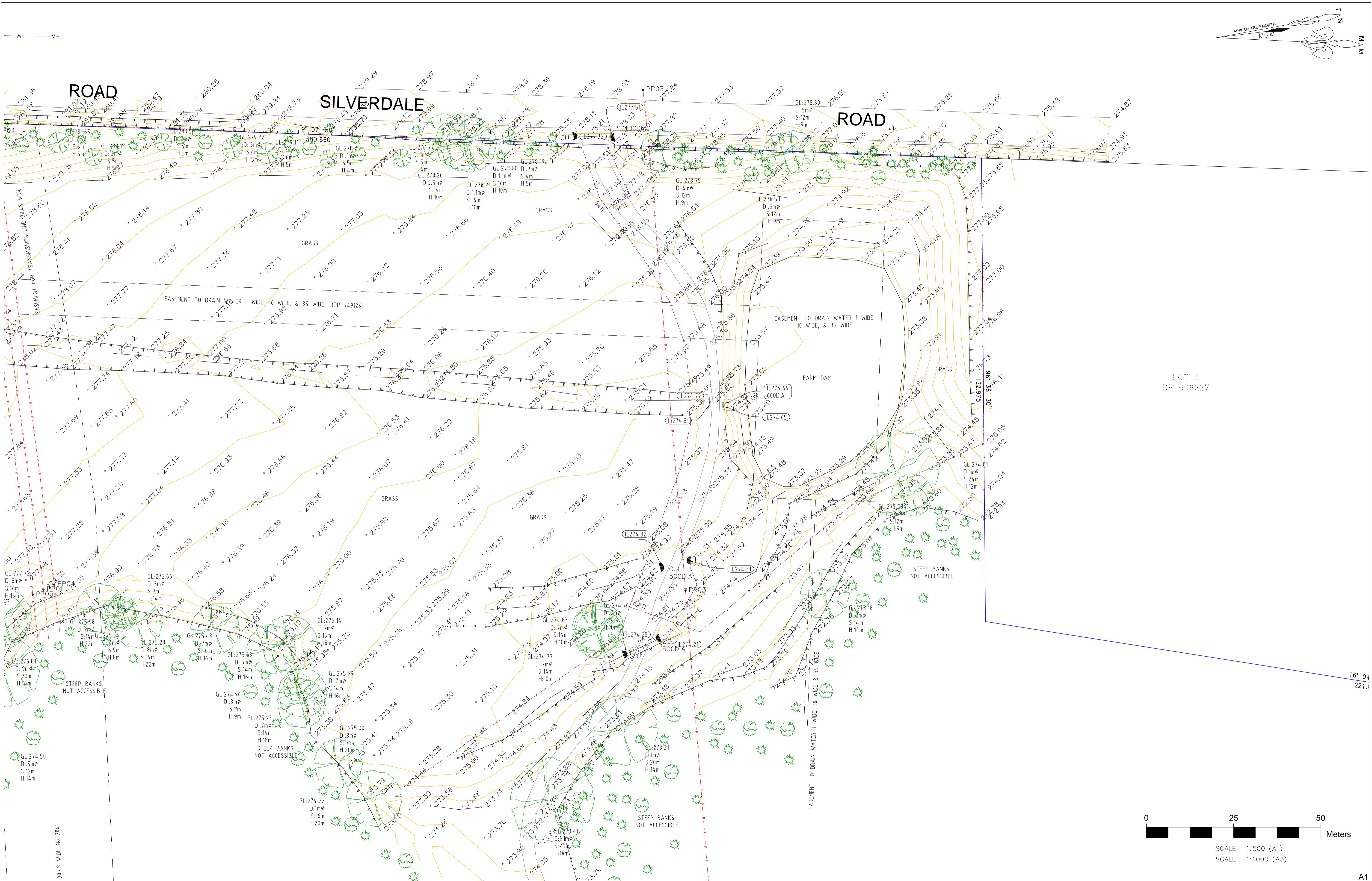
SHEET

DRAWING No. : 1817Det.dwg

CLIENT : MR & MRS NOCERA

SCB REF : 1877 Dec

DATE : 8 February 2024



## NOTES:

0.5m AND 1m CONTOURS SHOWN.

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**PROJECT : DETAIL AND LEVEL SURVEY  
ON LOT 3 IN DP 1201486  
AT THE OAKS**

---

CLIENT : MR & MRS NOCERA

LIBERTY - MR & MRS NOZERA

1

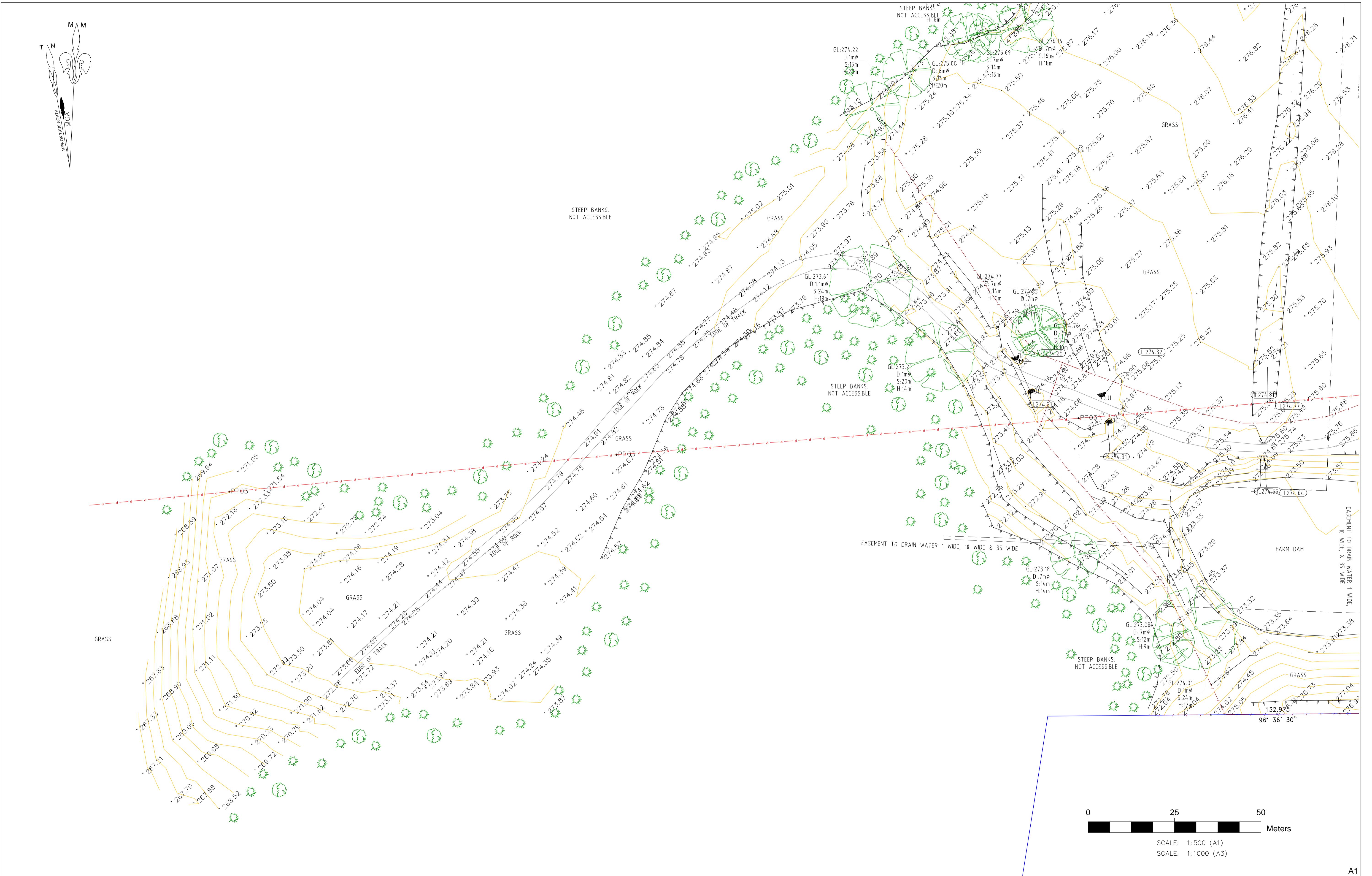
**STREET** 11-01-0

DRAWING No. : 1817Det.dwg

JOB REF : 1817Det

CD KEY: 101102

**DATE :** 8 February 2024



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## **APPENDIX B**

### **Flood Mapping**

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Title:

**80 Silverdale Road, The Oaks  
Existing Development - Peak Flood Depth  
1% AEP Event**

Fig: 23130.F01

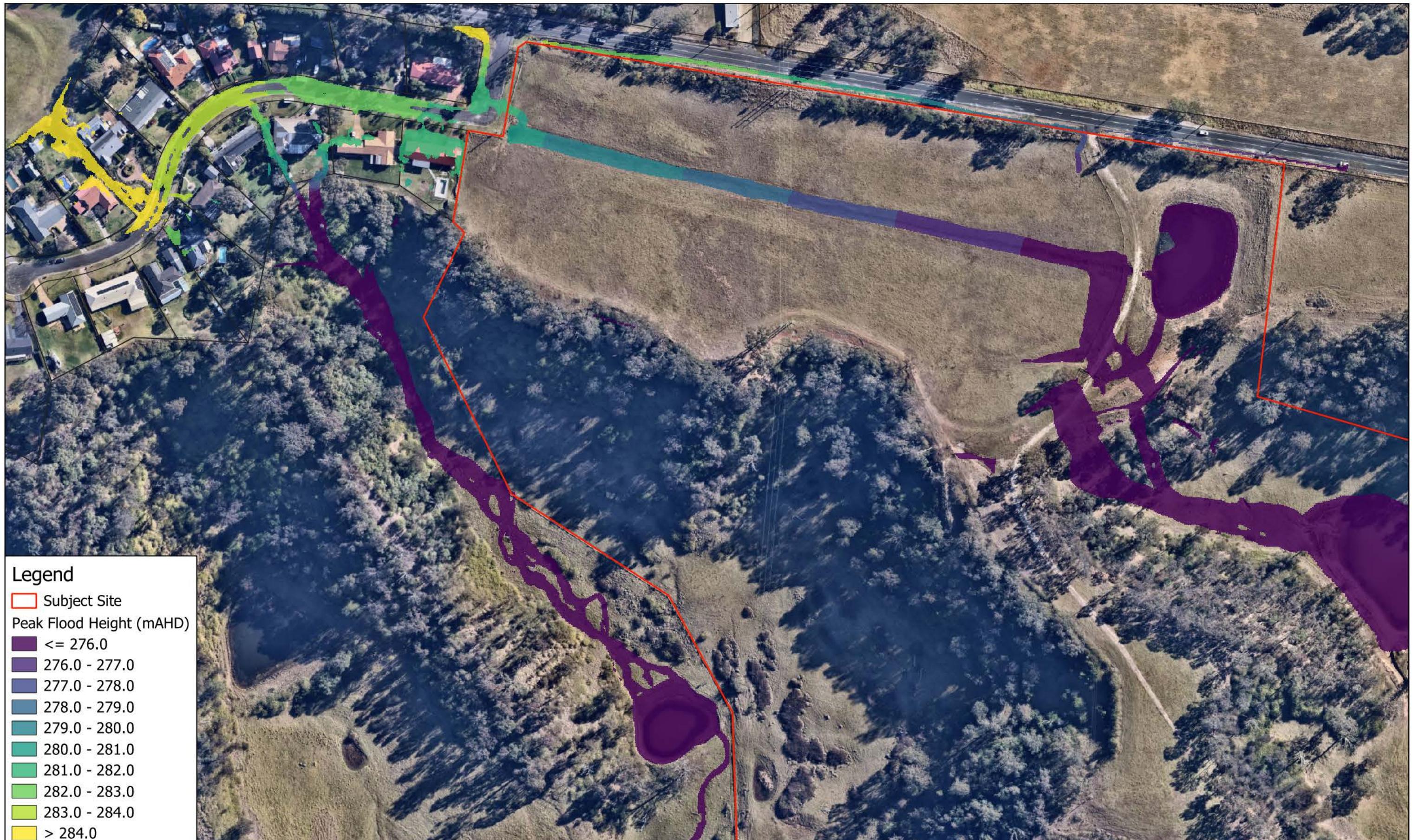
Rev: B

Date: 13.03.24

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Title:

**80 Silverdale Road, The Oaks  
Existing Development - Peak Flood Height  
1% AEP Event**

Fig: 23130.F02

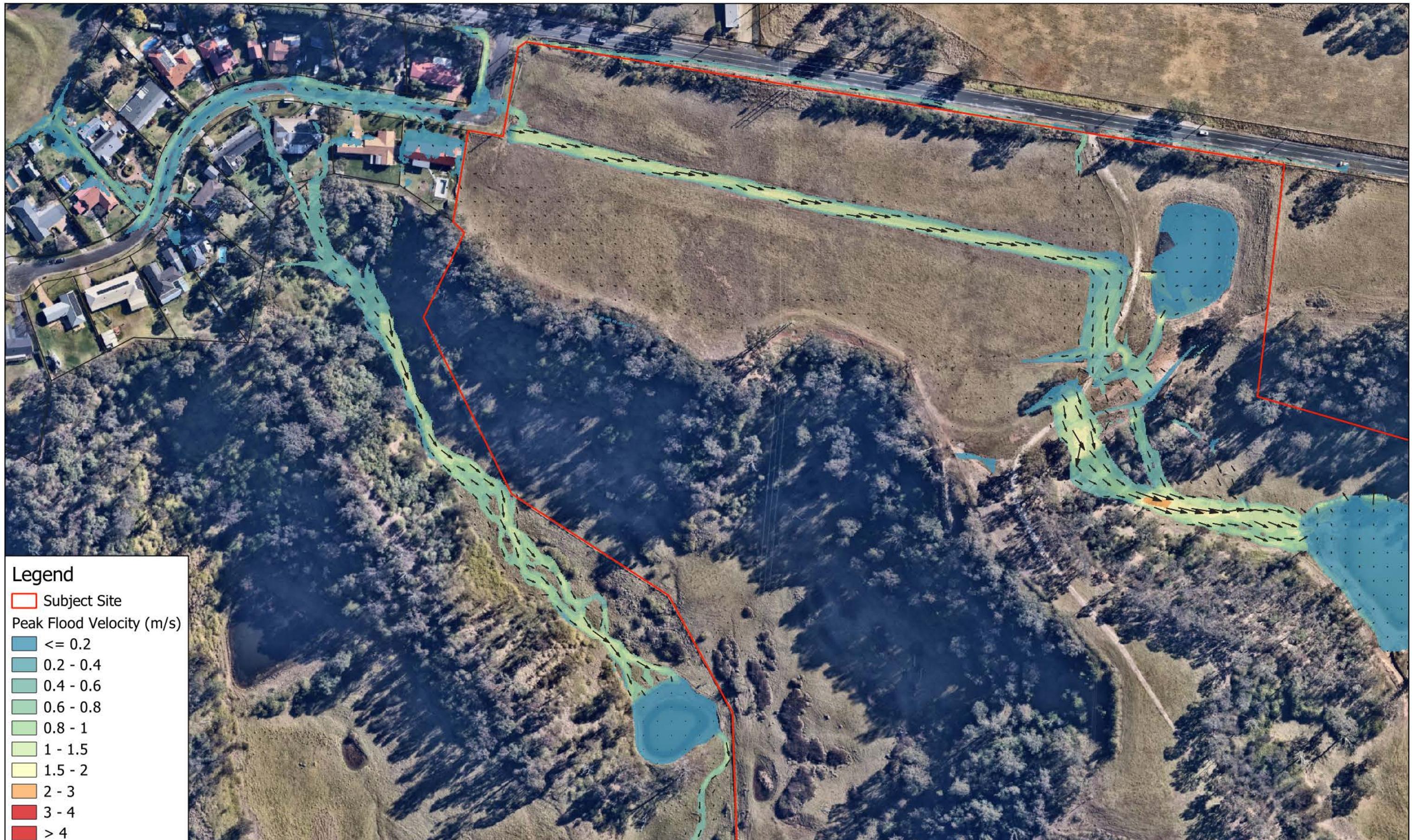
Rev: B

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Title:

**80 Silverdale Road, The Oaks**  
**Existing Development - Peak Flood Velocity**  
**1% AEP Event**

Fig: 23130.F03

Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks**  
**Existing Development - Peak Flood Hazard**  
**1% AEP Event**

Fig: 23130.F04

Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Depth  
1% AEP Event**

Fig: 23130.F05

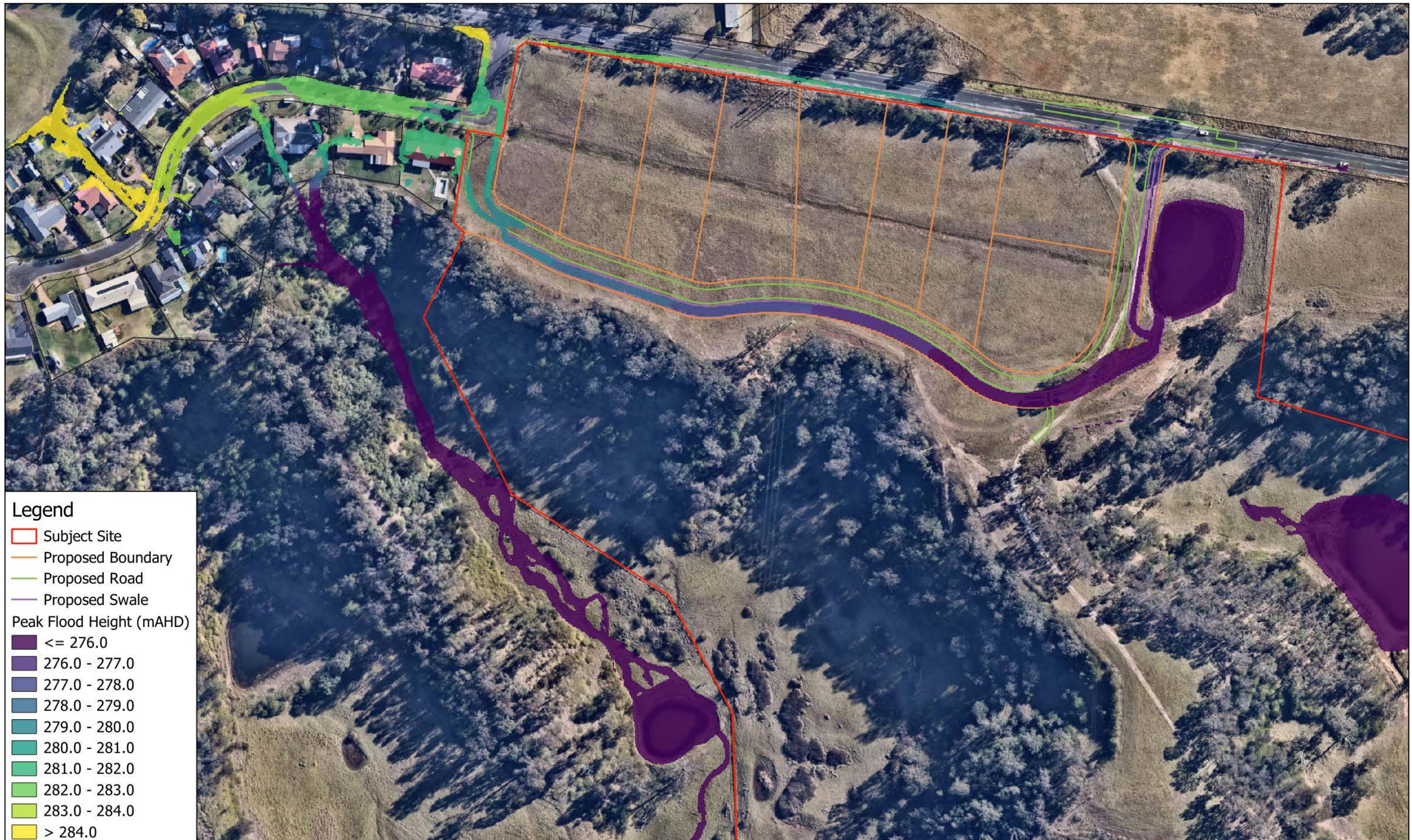
Rev: B

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Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Height  
1% AEP Event**

Fig: 23130.F06

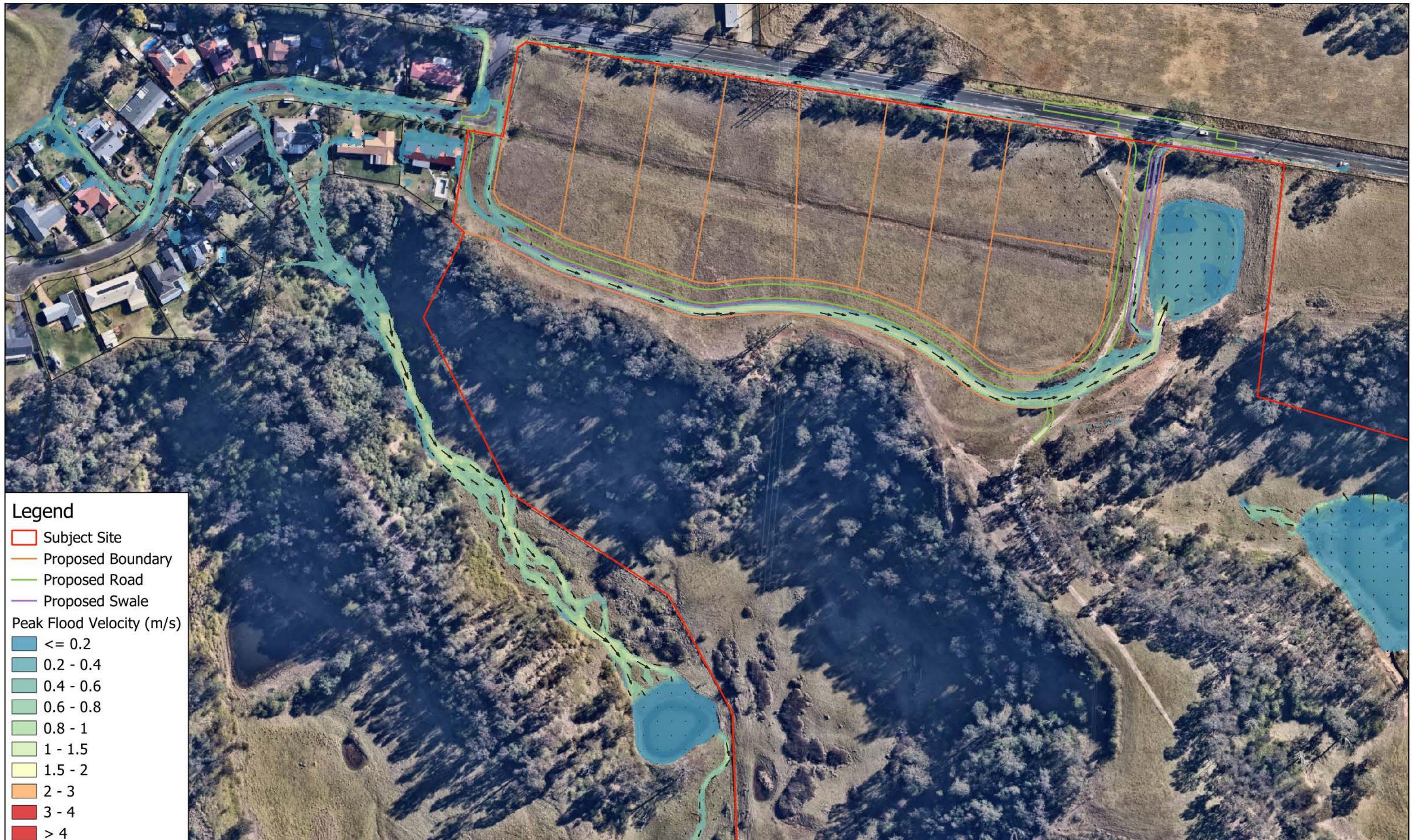
Rev: B

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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Velocity  
1% AEP Event**

Fig: 23130.F07

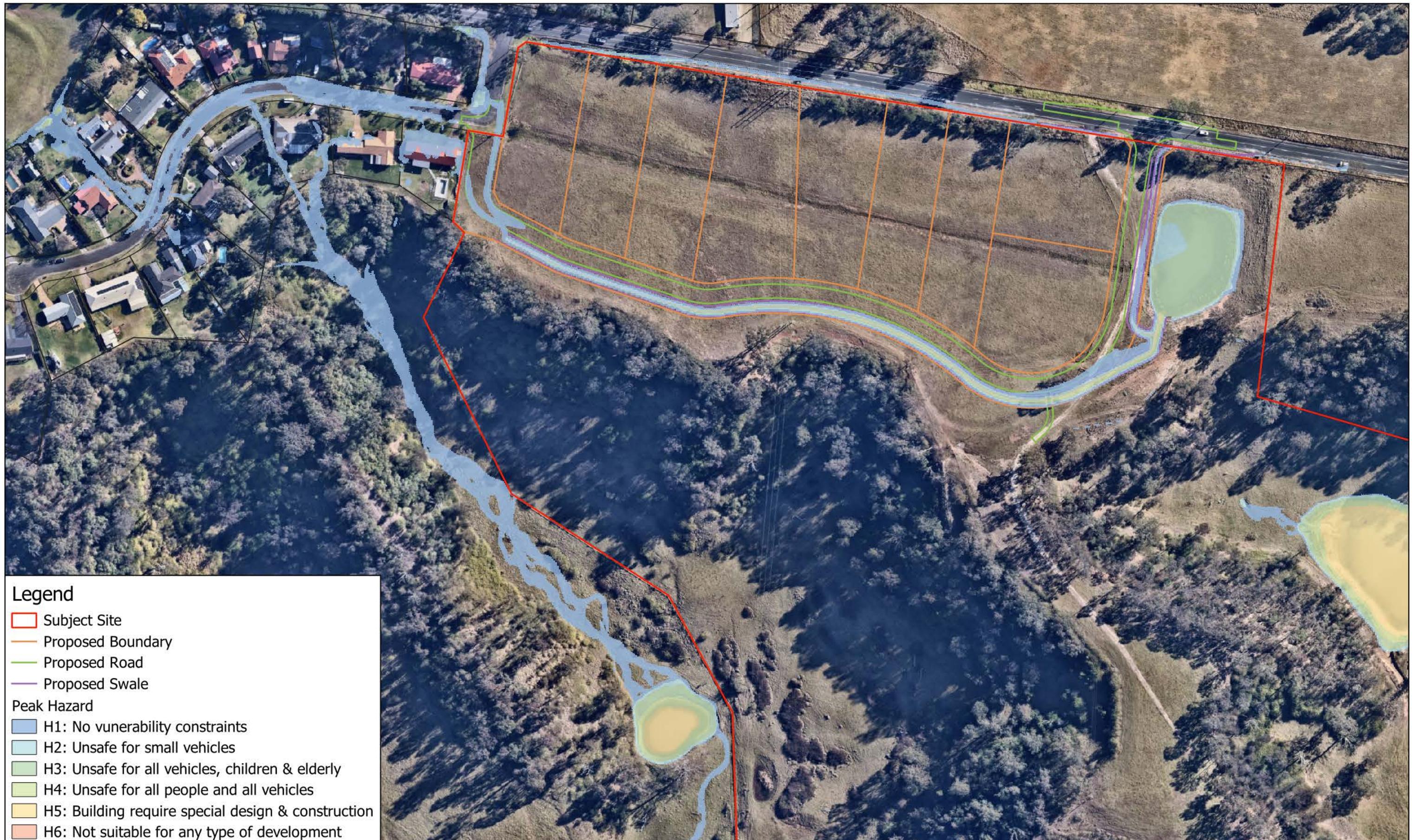
Rev: B

Date: 13.03.24

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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Hazard  
1% AEP Event**

Fig: **23130.F08**

Rev: **B**

Date: **13.03.24**

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Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks  
Existing Development - Peak Flood Depth  
PMF Event**

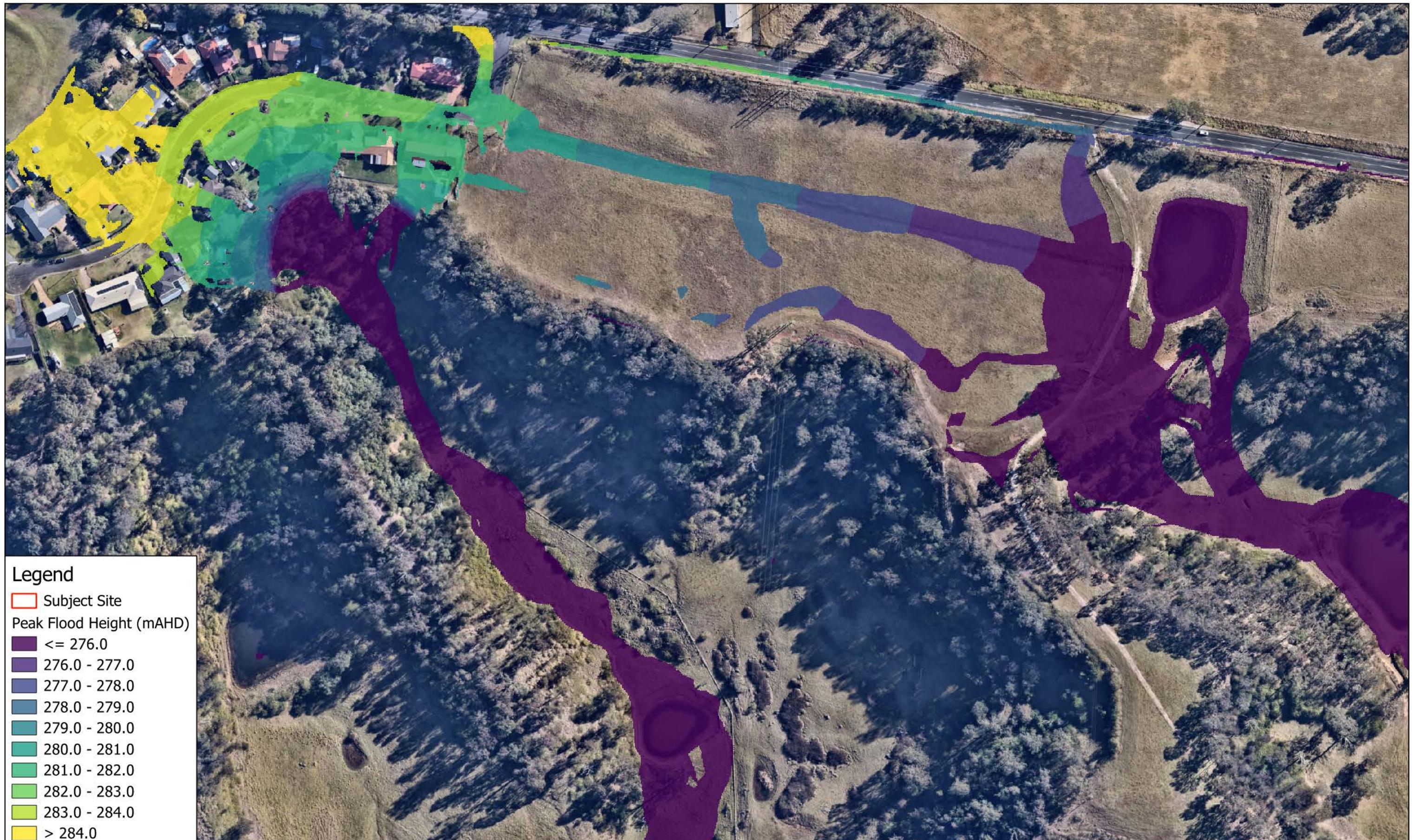
Fig: **23130.F09**

Rev: **B**

Date: **13.03.24**

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Scale: 1:2,000 @ A3

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Legend

- Subject Site
- Peak Flood Height (mAHD)
  - <= 276.0
  - 276.0 - 277.0
  - 277.0 - 278.0
  - 278.0 - 279.0
  - 279.0 - 280.0
  - 280.0 - 281.0
  - 281.0 - 282.0
  - 282.0 - 283.0
  - 283.0 - 284.0
  - > 284.0

Title:

**80 Silverdale Road, The Oaks**  
**Existing Development - Peak Flood Height**  
**PMF Event**

Fig: 23130.F10

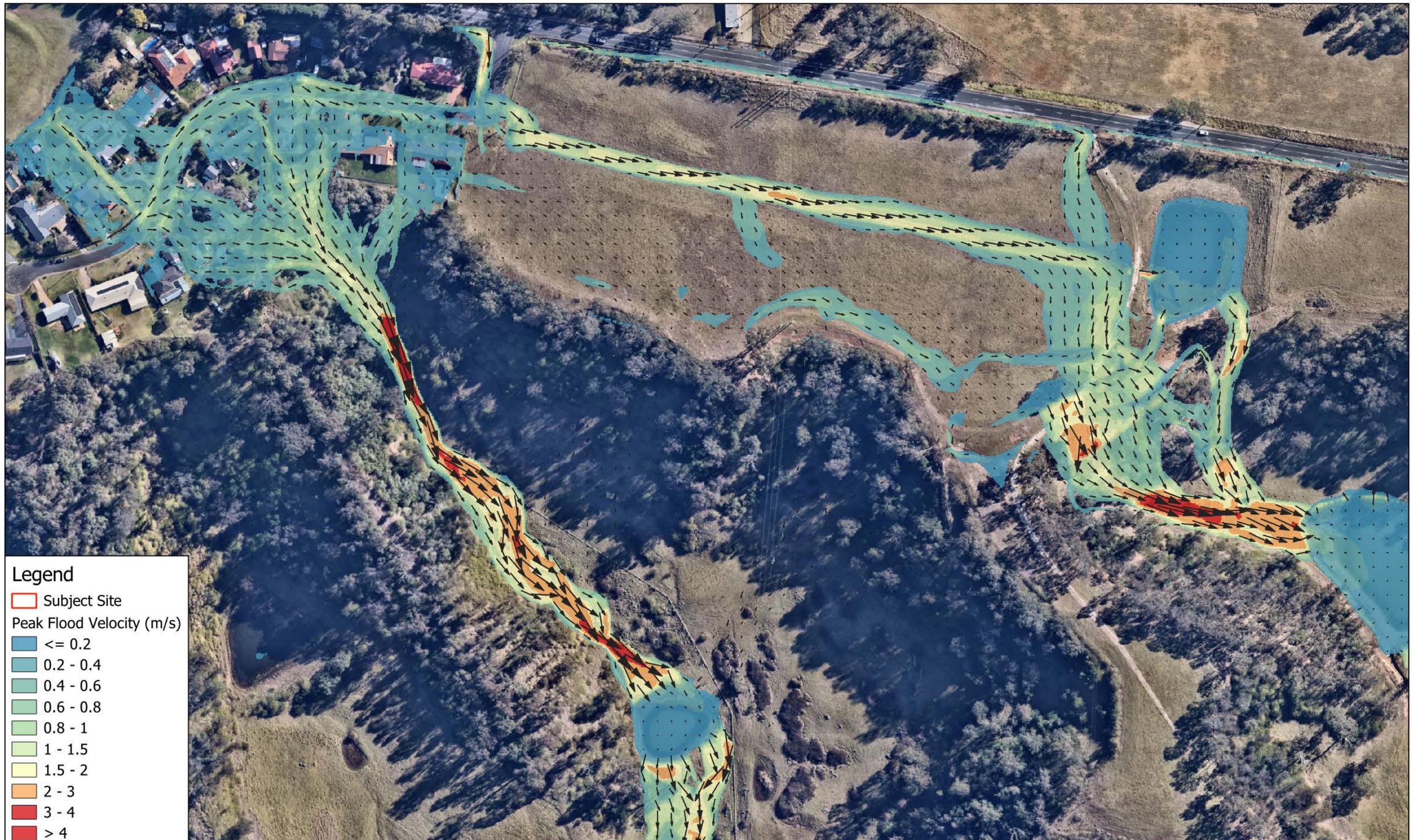
Rev: B

Date: 13.03.24

0 25 50 75 100 m  
Scale: 1:2,000 @ A3



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Legend

Subject Site

Peak Flood Velocity (m/s)

<= 0.2

0.2 - 0.4

0.4 - 0.6

0.6 - 0.8

0.8 - 1

1 - 1.5

1.5 - 2

2 - 3

3 - 4

> 4

Title:

**80 Silverdale Road, The Oaks  
Existing Development - Peak Flood Velocity  
PMF Event**

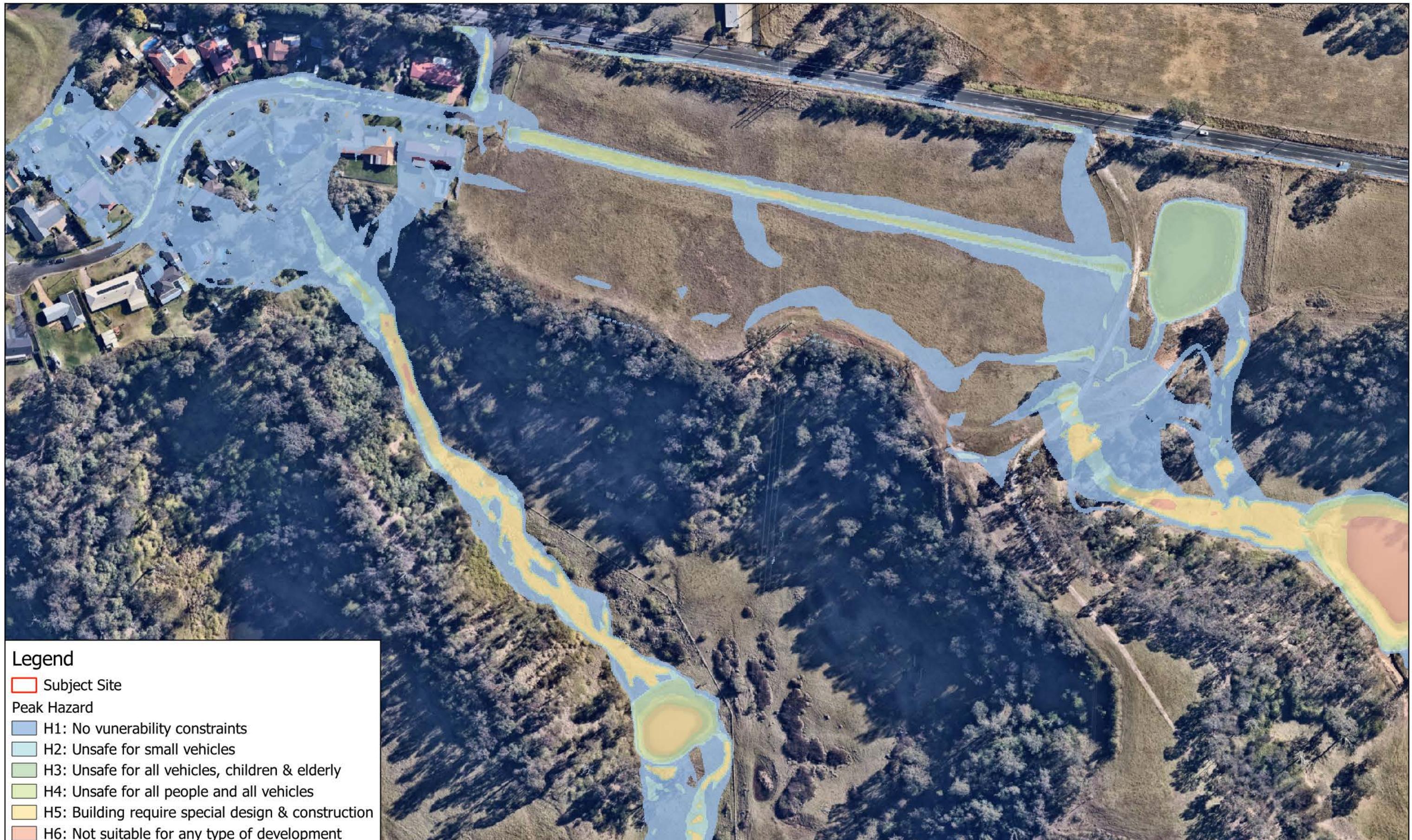
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Fig: 23130.F11

Rev: B

Date: 13.03.24

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Title:

**80 Silverdale Road, The Oaks  
Existing Development - Peak Flood Hazard  
PMF Event**

Fig: 23130.F12

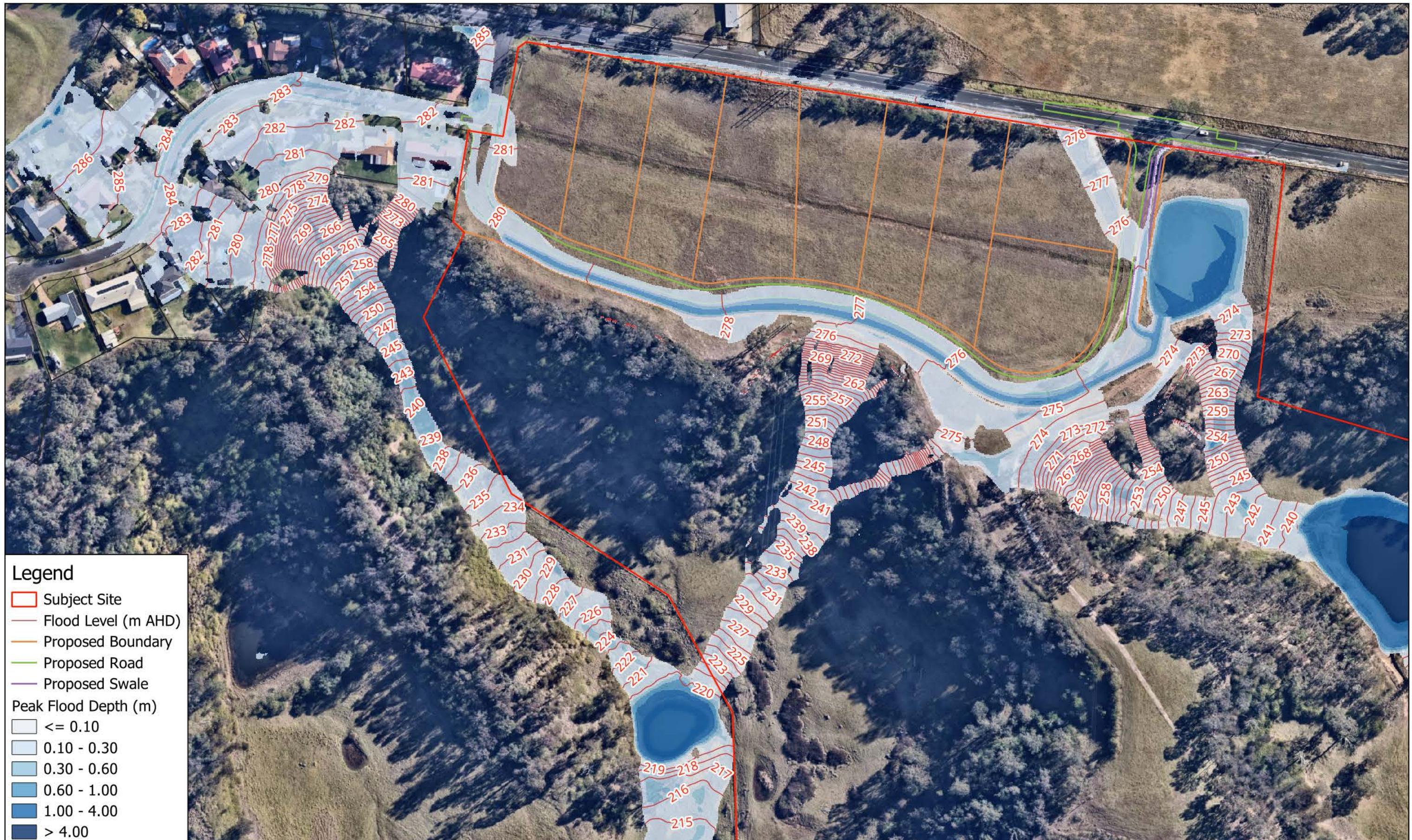
Rev: B

Date: 13.03.24

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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Depth  
PMF Event**

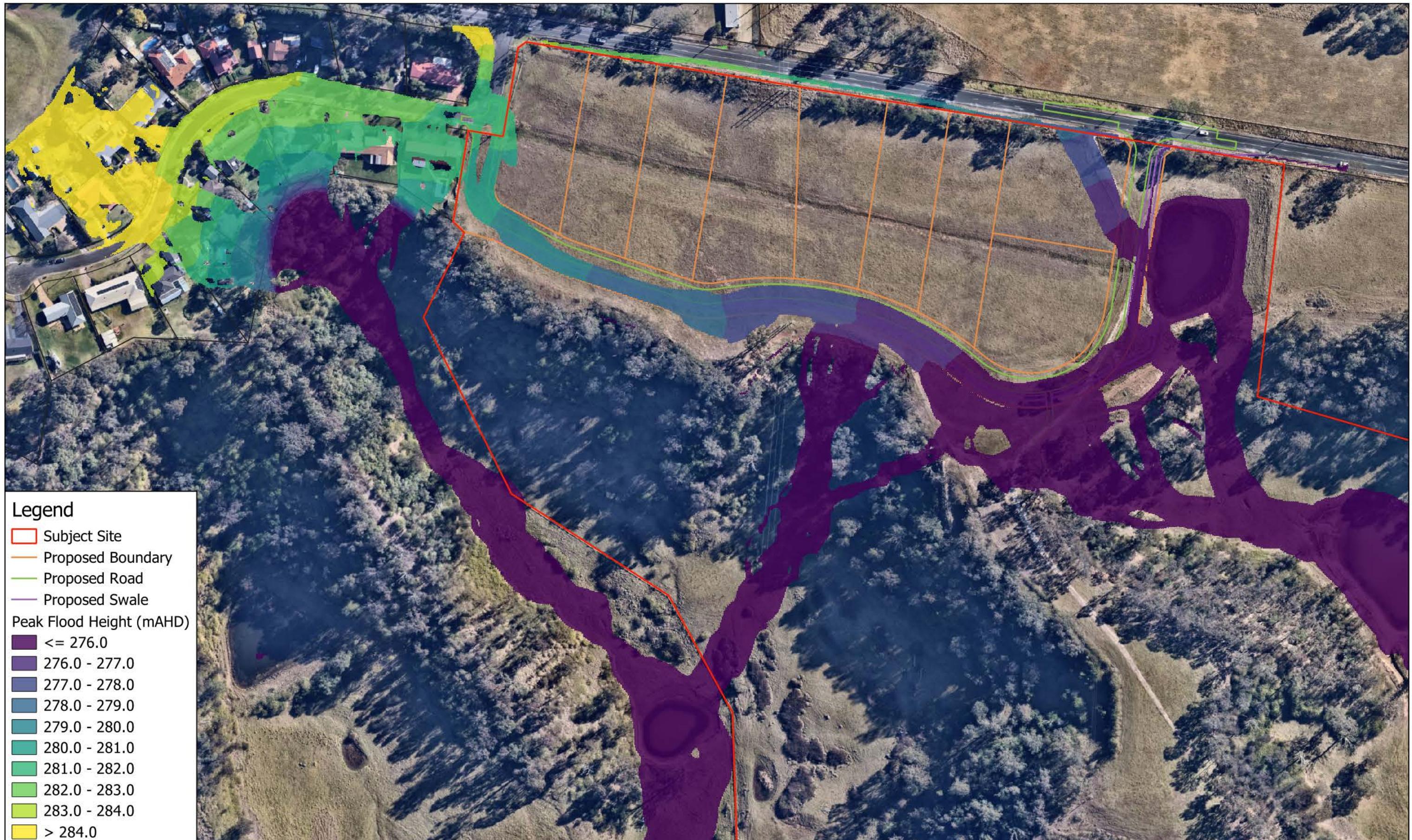
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Rev: **B**

Date: **13.03.24**

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Scale: 1:2,000 @ A3

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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Height  
PMF Event**

Fig: 23130.F14

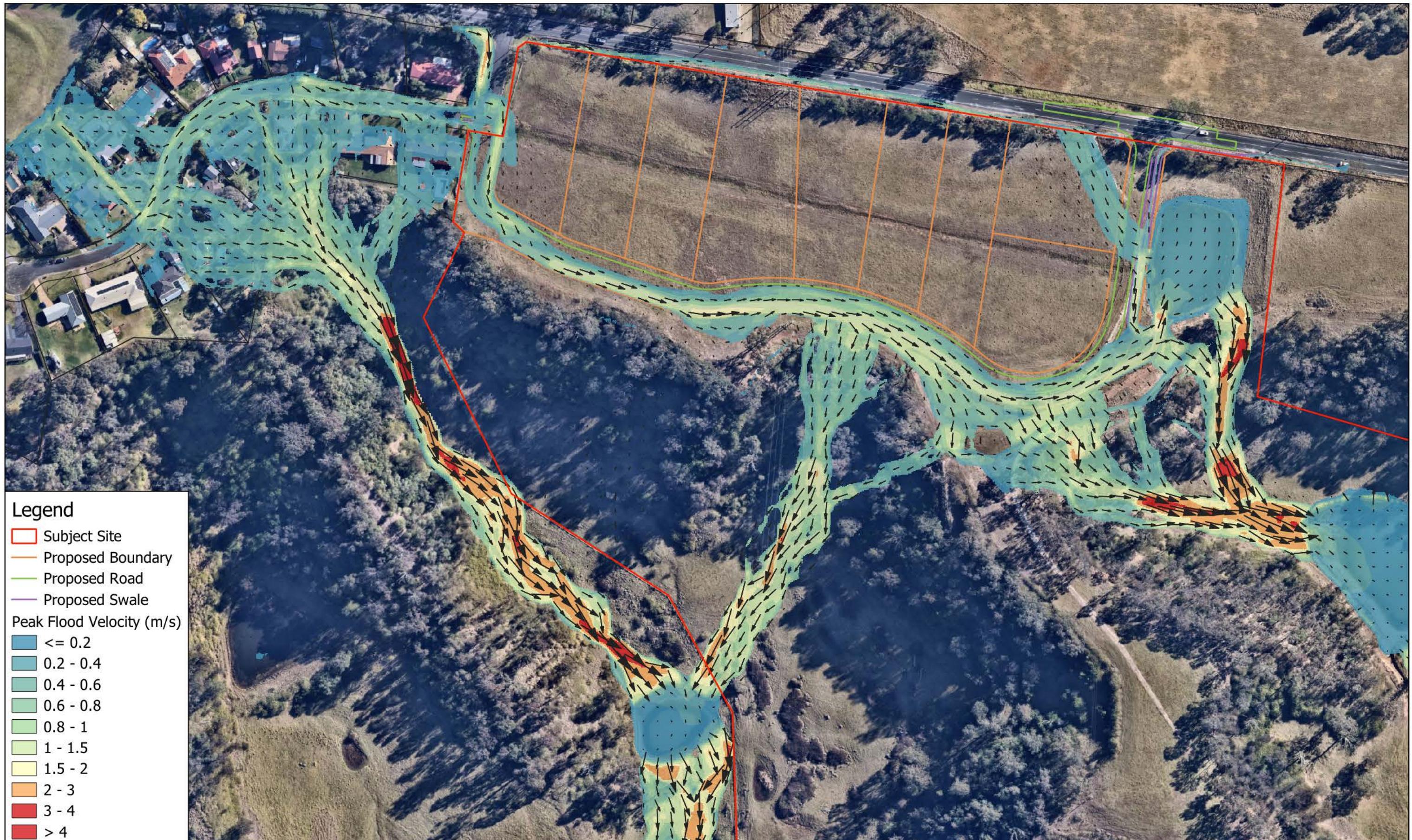
Rev: B

Date: 13.03.24

0 25 50 75 100 m  
Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Velocity  
PMF Event**

Fig: 23130.F15

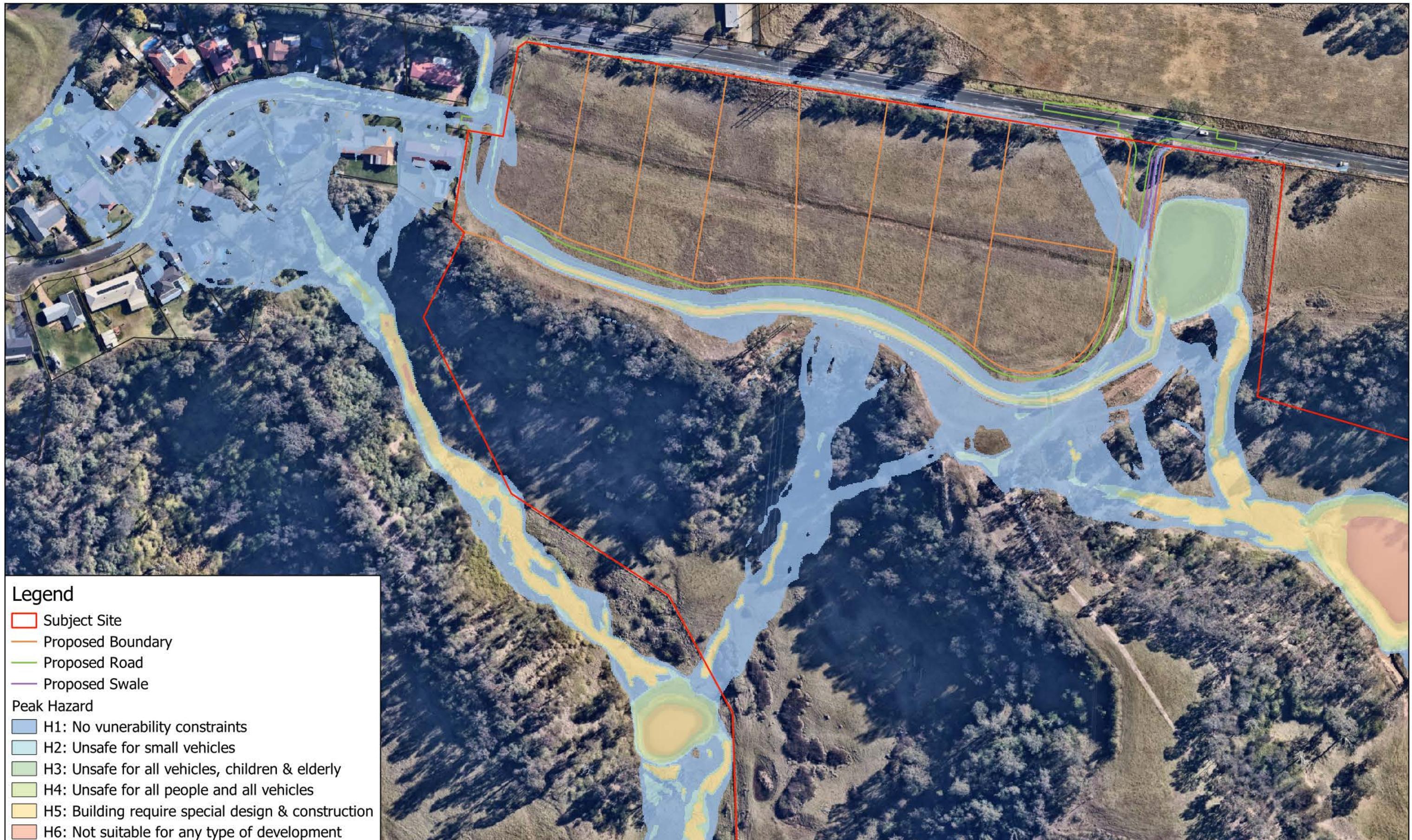
Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



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Title:

## 80 Silverdale Road, The Oaks Proposed Development - Peak Flood Hazard PMF Event

Fig: 23130.F16

Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



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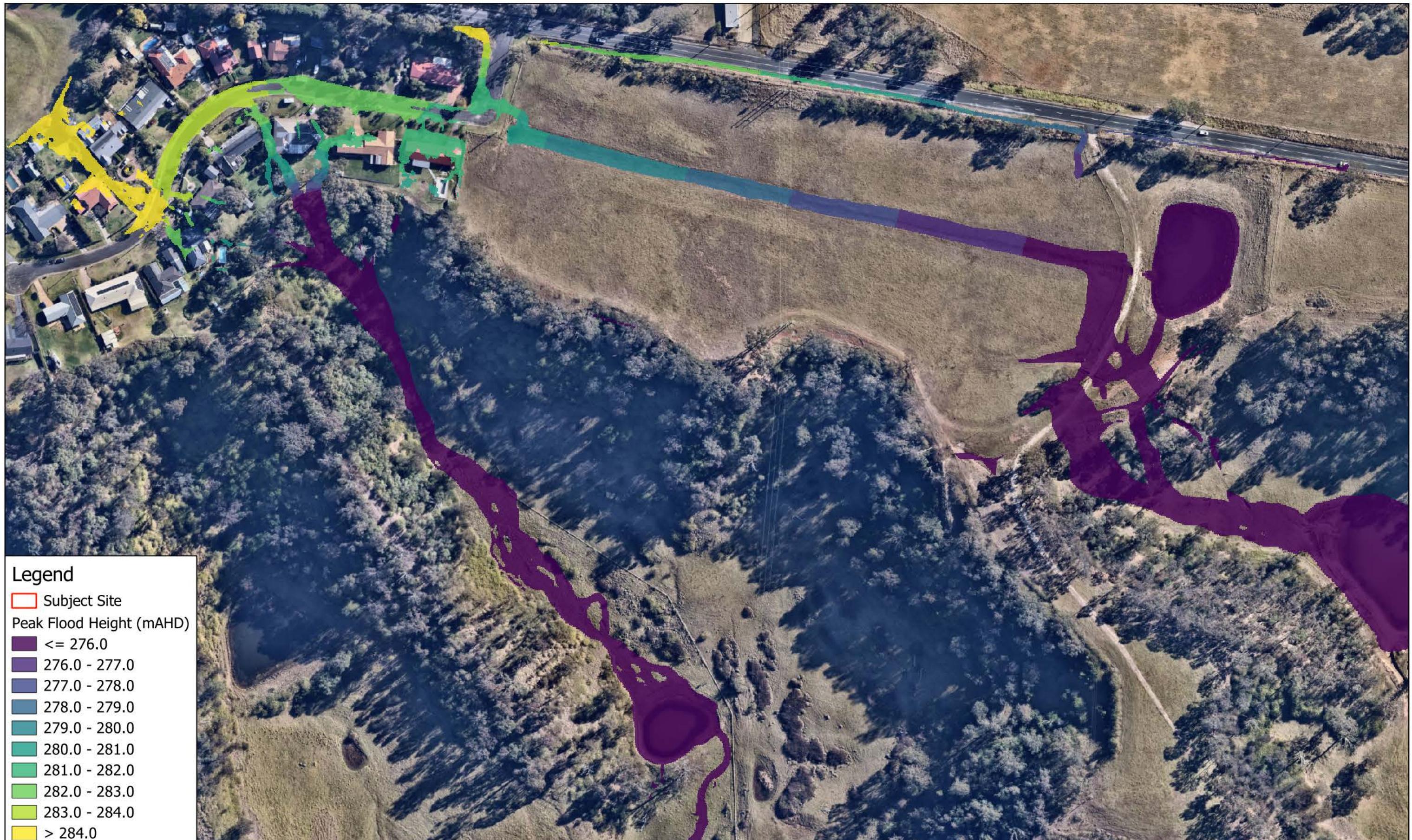
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Fig: 23130.F17

Rev: B

Date: 13.03.24

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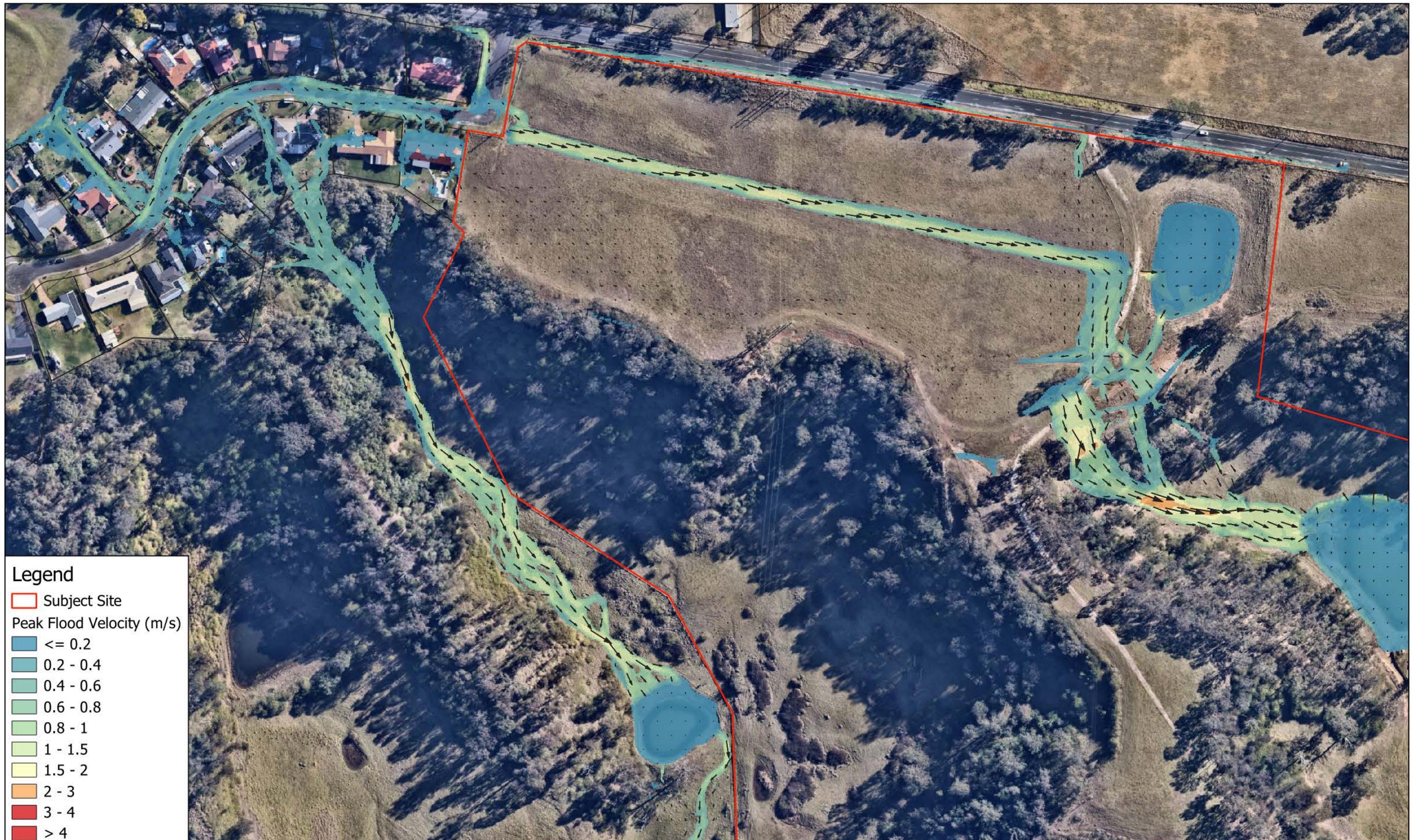
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Scale: 1:2,000 @ A3

Fig: 23130.F18

Rev: B

Date: 13.03.24

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Title:

**80 Silverdale Road, The Oaks  
Existing Development - Peak Flood Velocity  
1%AEP Climate Change Event**

Fig: 23130.F19

Rev: B

Date: 13.03.24

0 25 50 75 100 m  
Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks**  
**Existing Development - Peak Flood Hazard**  
**1%AEP Climate Change Event**

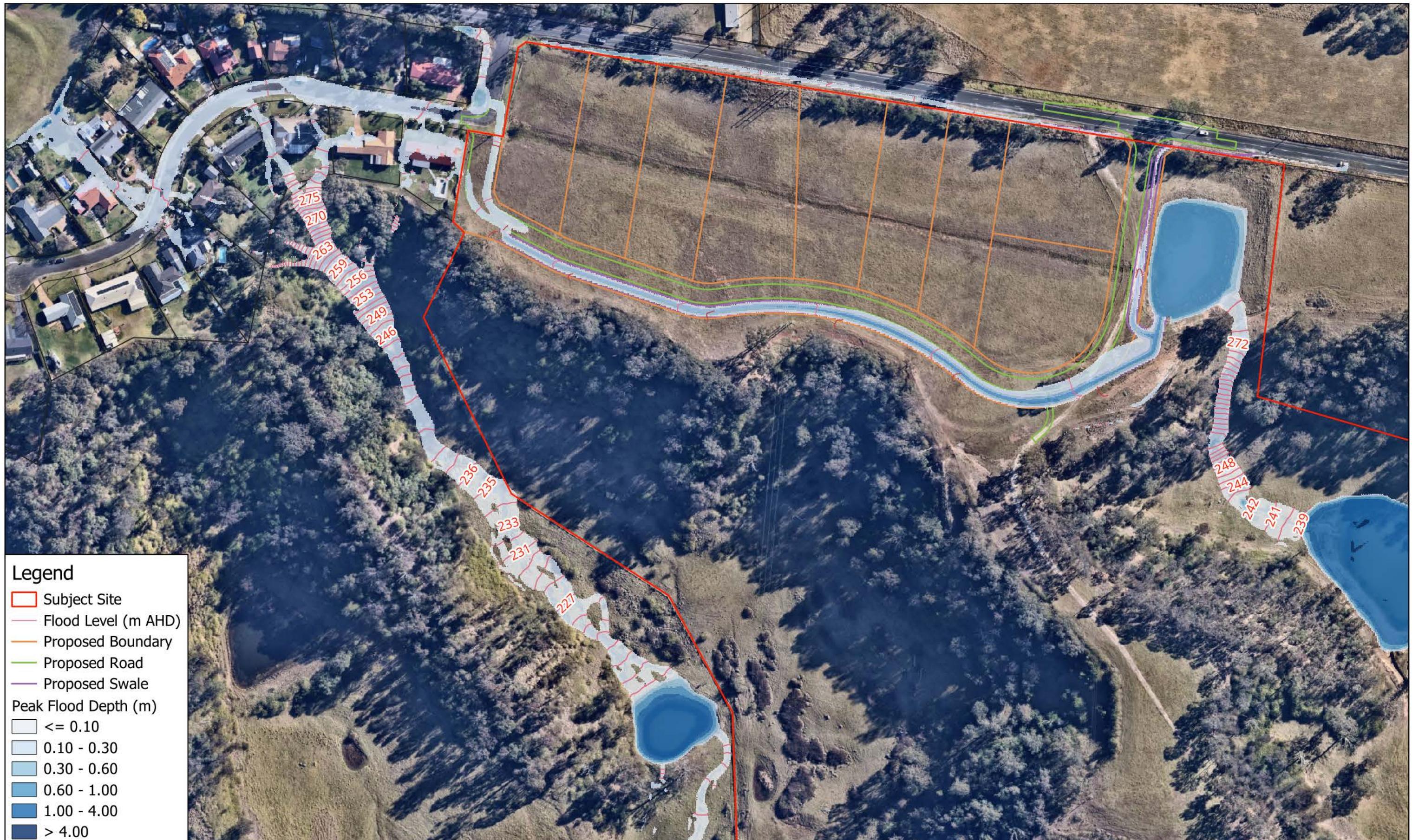
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Fig: 23130.F20

Date: 13.03.24

Rev: B

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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Depth  
1%AEP Climate Change Event**

Fig: 23130.F21

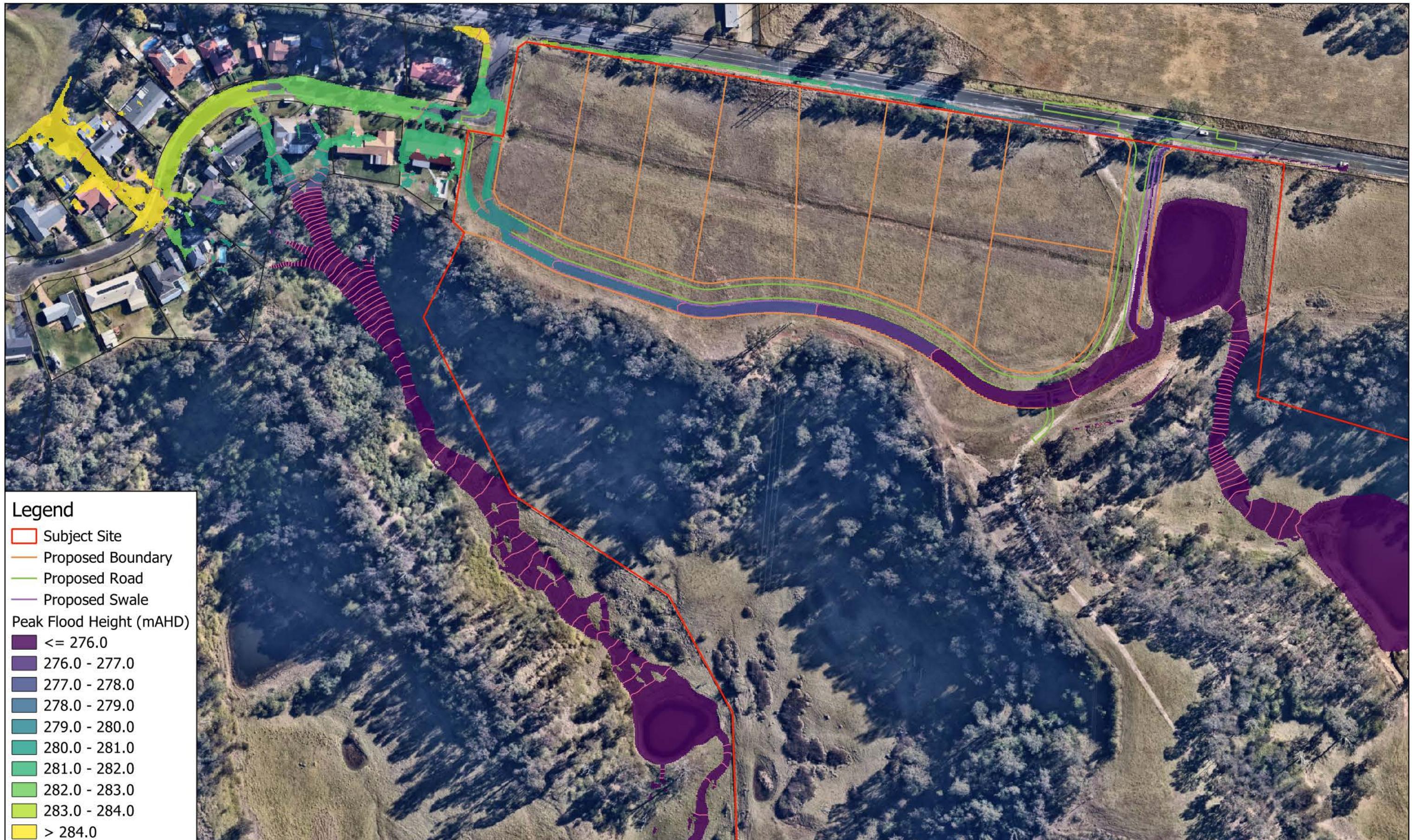
Rev: B

Date: 13.03.24

0 25 50 75 100 m  
Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Height  
1%AEP Climate Change Event**

Fig: 23130.F22

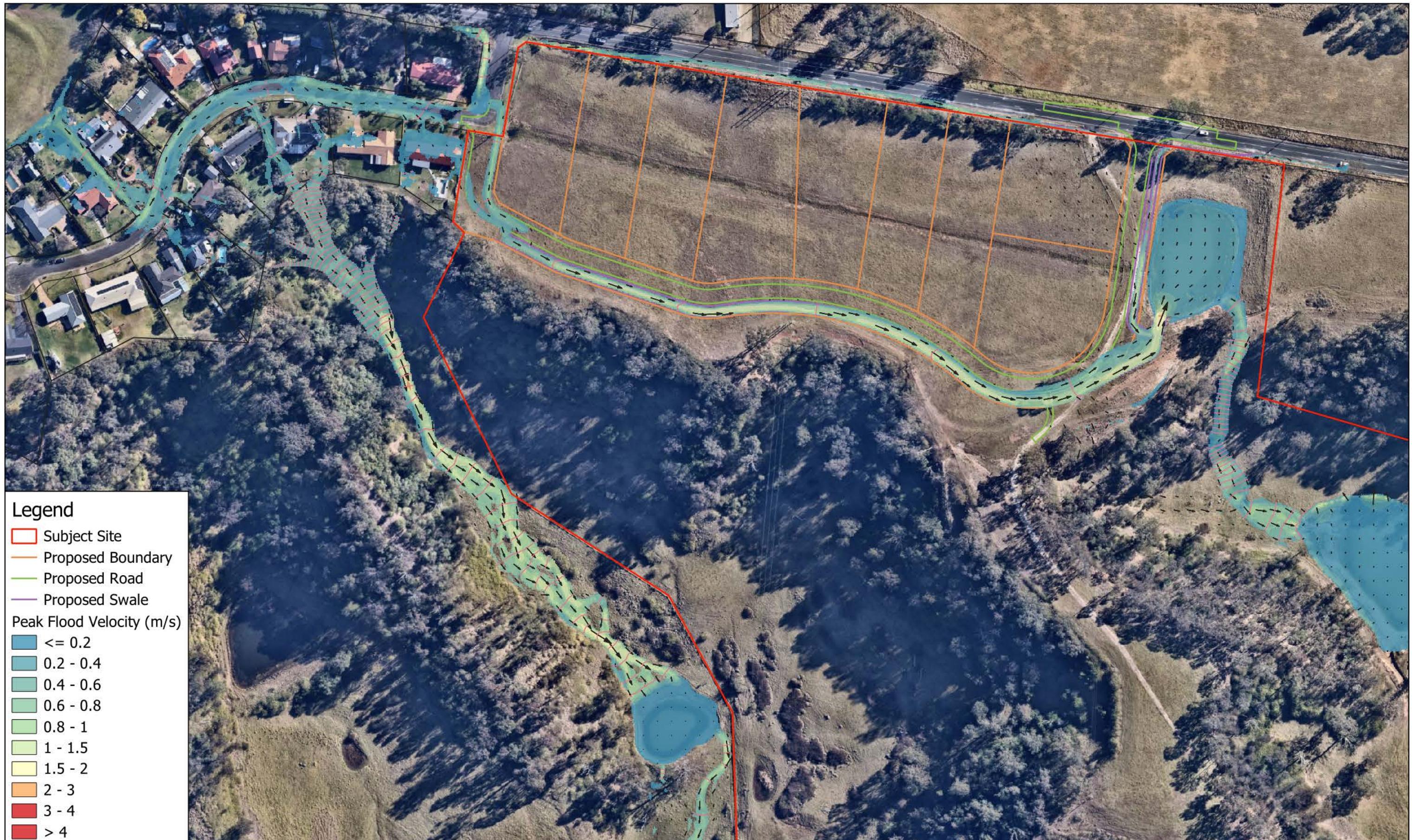
Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Velocity  
1%AEP Climate Change Event**

Fig: 23130.F23

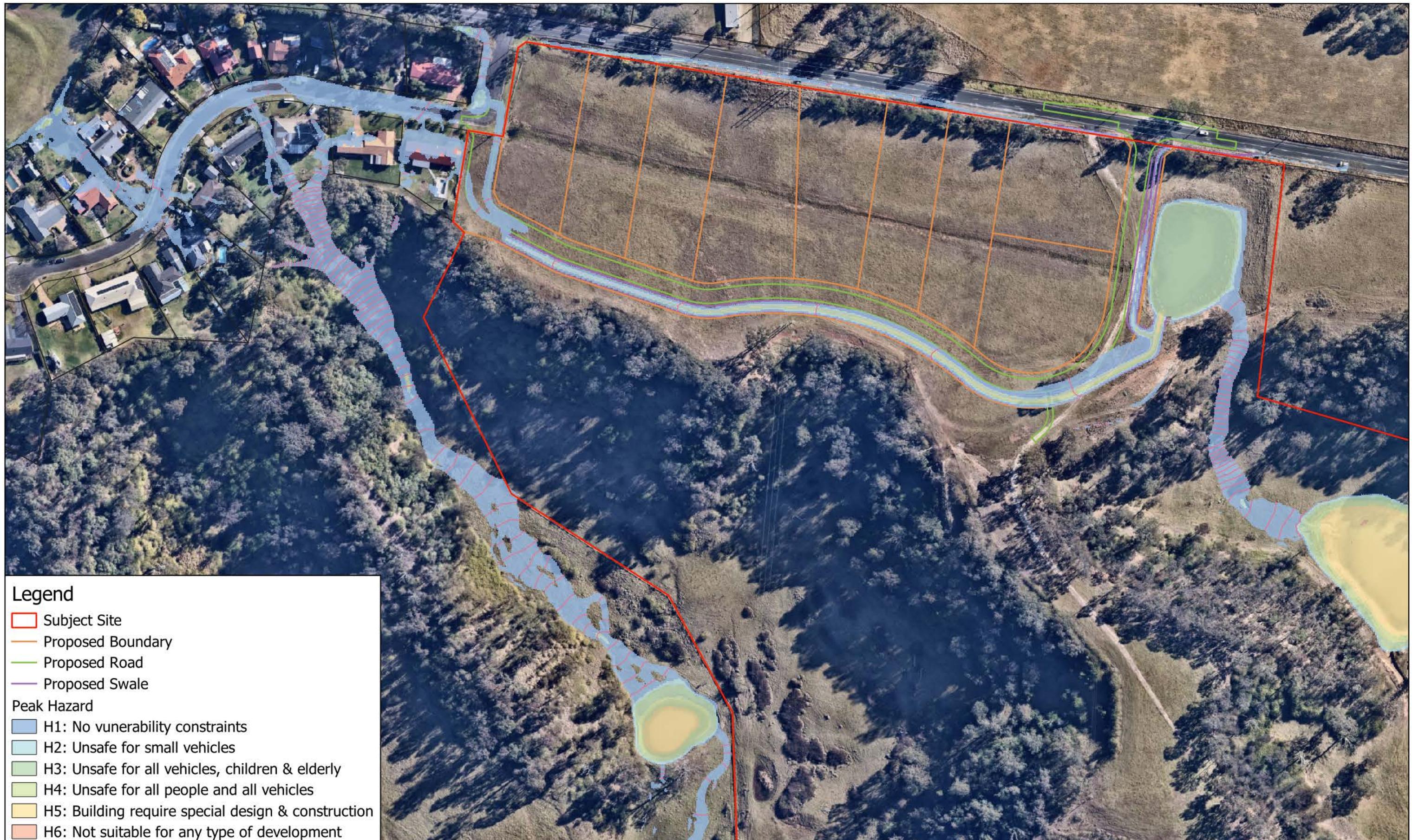
Rev: B

Date: 13.03.24

0 25 50 75 100 m  
Scale: 1:2,000 @ A3



**siteplus**



Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Hazard  
1%AEP Climate Change Event**

0 25 50 75 100 m  
Scale: 1:2,000 @ A3

Fig: 23130.F24

Rev: B

Date: 13.03.24

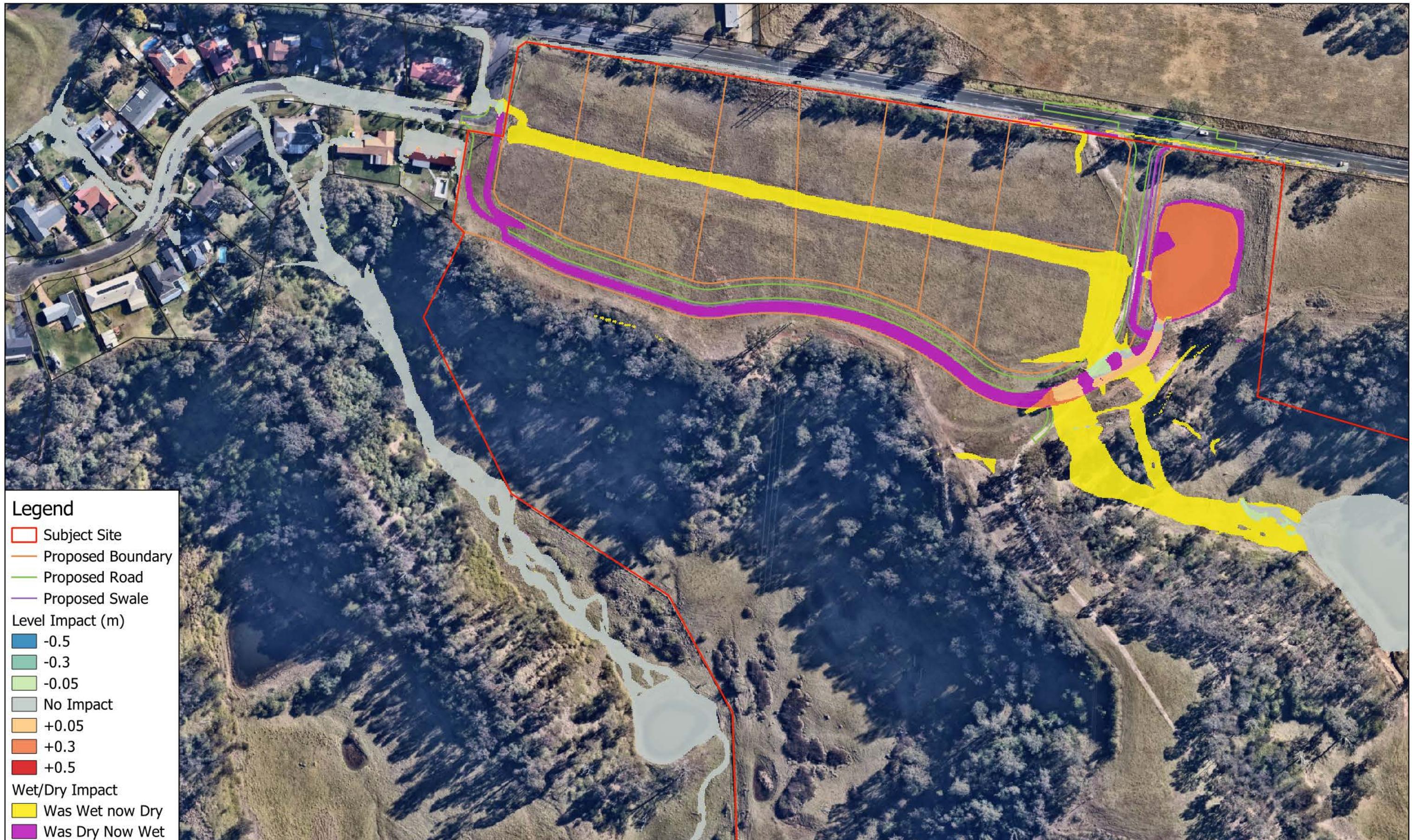
**siteplus**

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## **APPENDIX C**

### **Flood Impact Mapping**

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Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Hazard  
1%AEP Level Impacts**

Fig: 23130.F25

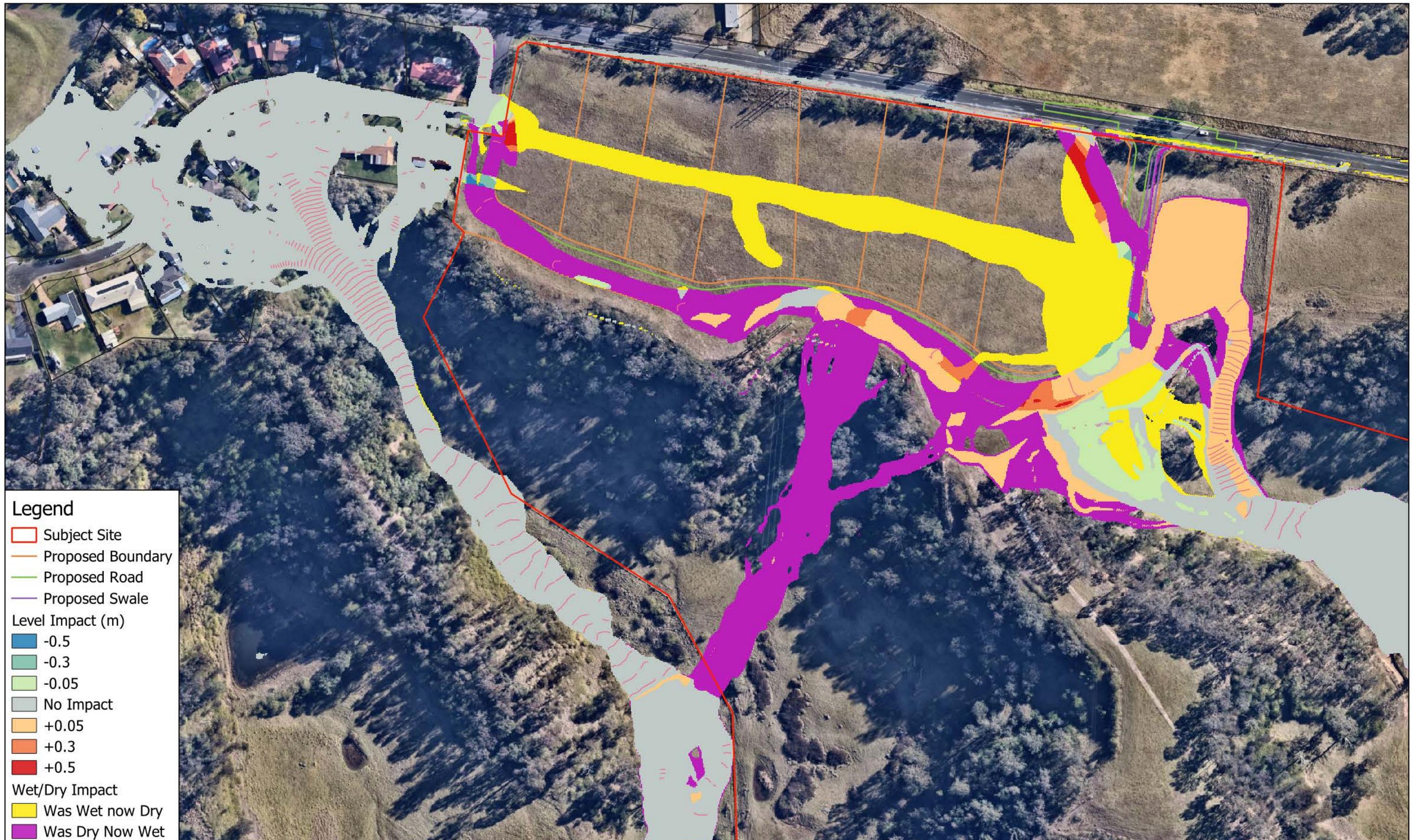
Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



**siteplus**



Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Hazard  
PMF Level Impacts**

Fig: 23130.F26

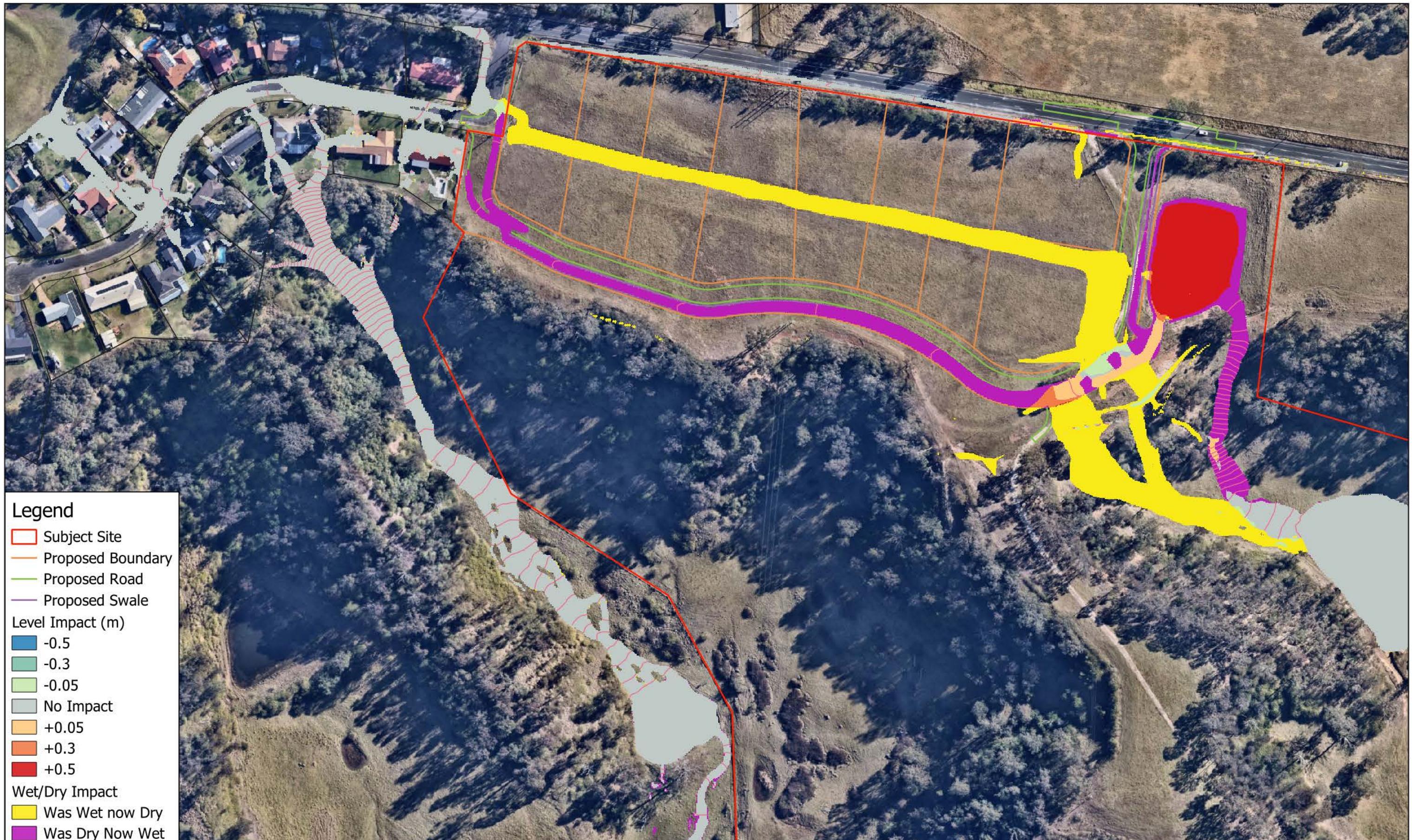
Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



**siteplus**



Title:

**80 Silverdale Road, The Oaks  
Proposed Development - Peak Flood Hazard  
1%AEP Climate Change Level Impacts**

Fig: 23130.F27

Rev: B

Date: 13.03.24

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Scale: 1:2,000 @ A3



**siteplus**

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## **APPENDIX D**

## **Civil Engineering Plans**

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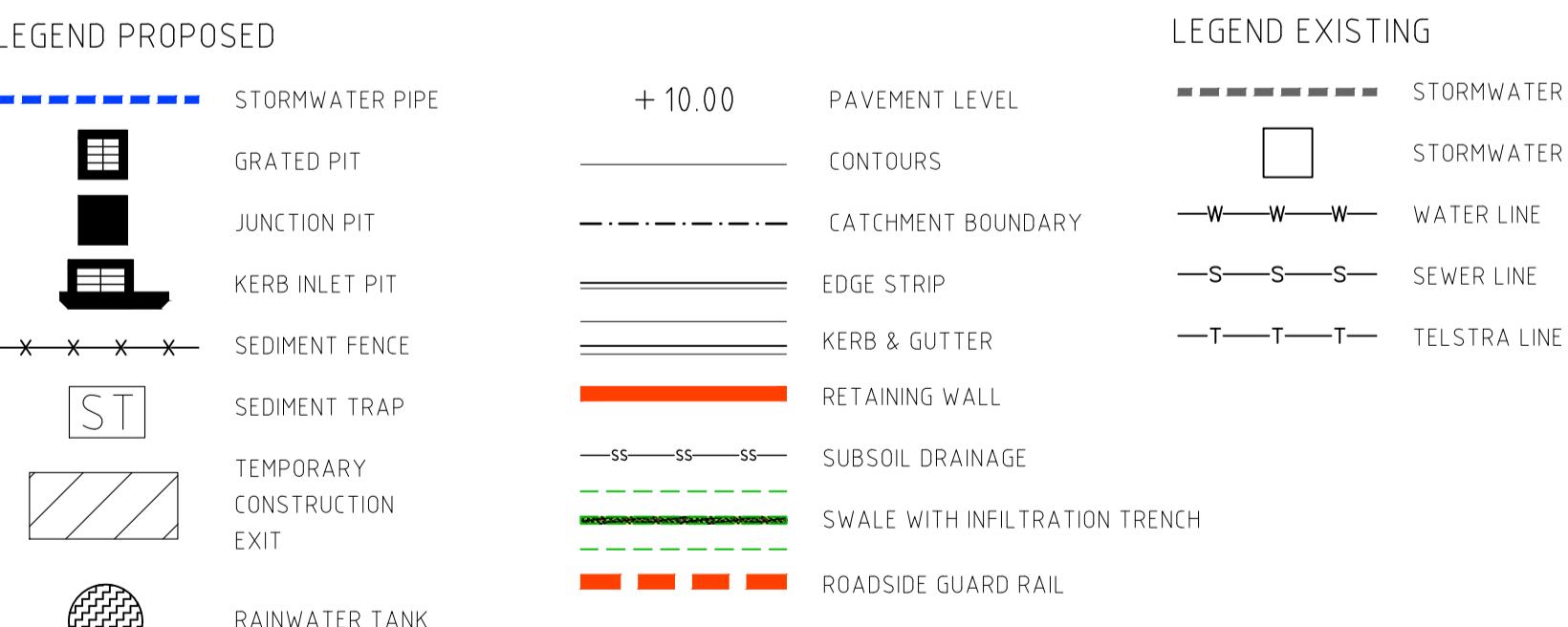
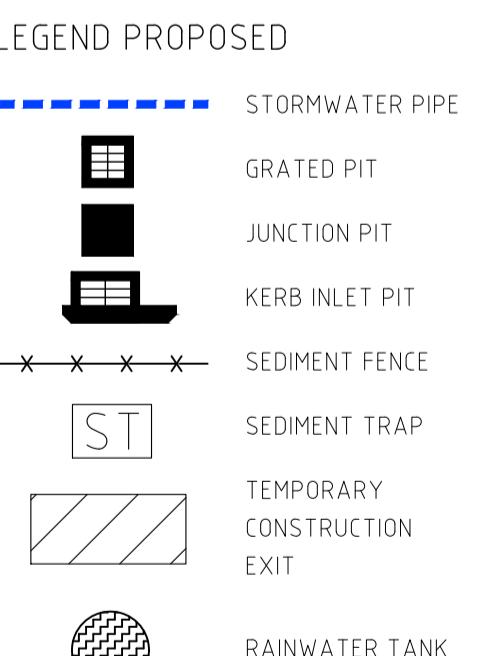
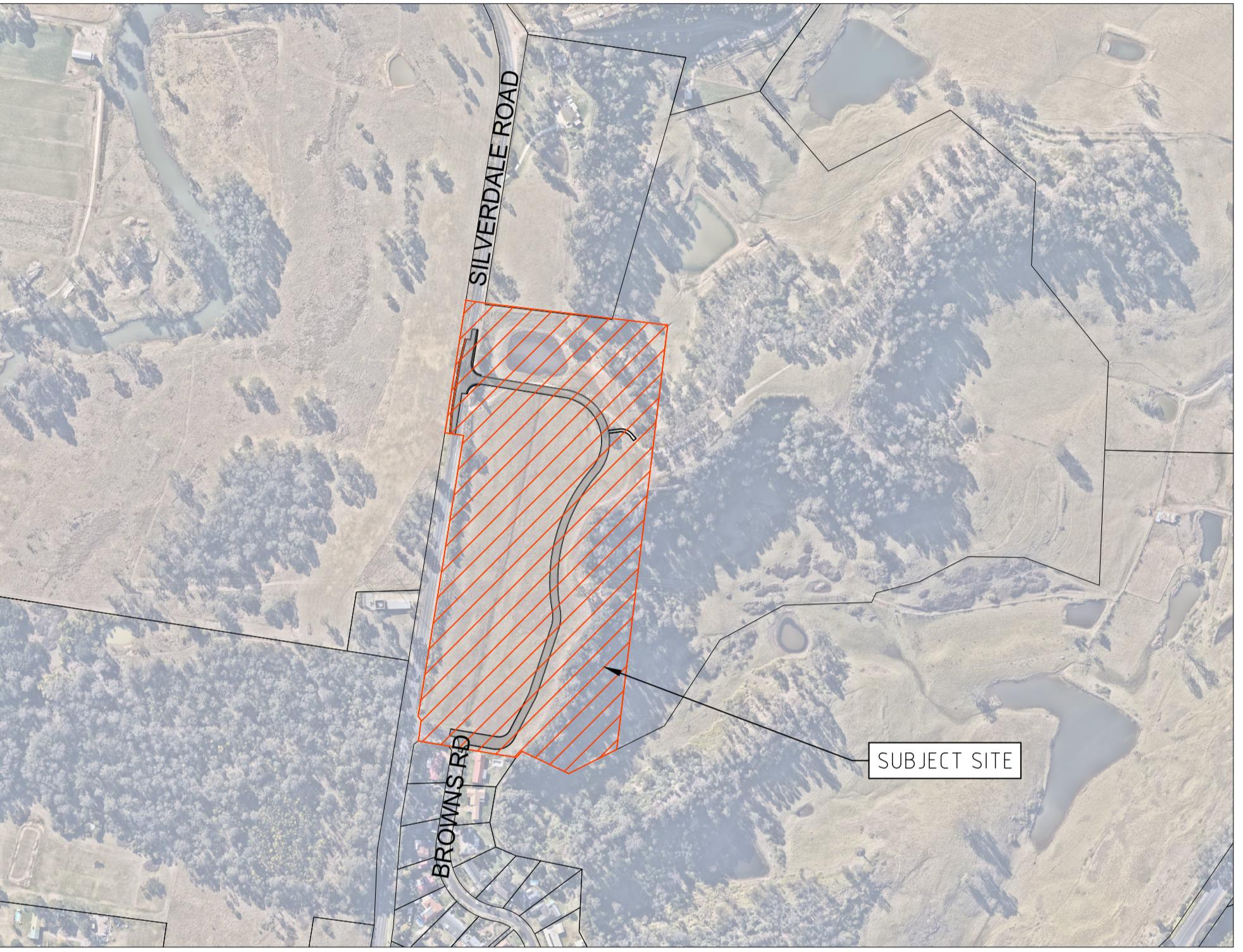
# PROPOSED RESIDENTIAL SUBDIVISION

## LOT 3 DP 1201486, 80 SILVERDALE ROAD, THE OAKS

### DEVELOPMENT APPLICATION CIVIL PLANS

#### MR & MRS NOCERA C/- PROFICIENT CONSTRUCTIONS (AUST) PTY LTD

Sheet List Table	
Sheet Number	Sheet Title
01	TITLE PAGE
02	CIVIL WORKS PLAN
03	BULK EARTHWORKS
04	ROAD LONG SECTIONS
05	INTERSECTION PLAN
06	ROAD TYPICAL SECTIONS
07	CATCHMENT PLAN
08	DRAINAGE CALCULATIONS
09	DRAINAGE LONG SECTIONS
10	MUSIC CATCHMENT PLAN
11	INTERSECTION SIGHT DISTANCE
12	INTERSECTION SWEEP PATHS
13	SOIL & WATER MANAGEMENT PLAN
14	SOIL & WATER MANAGEMENT DETAILS



SERVICES ARE SHOWN INDICATIVE ONLY. CONTRACTOR TO CONFIRM ALL SERVICE LOCATIONS PRIOR TO CONSTRUCTION

DIMENSIONS SHALL NOT BE OBTAINED BY SCALING FROM THIS SET OF PLANS

No.	DESCRIPTION	DRN	APP	DATE
A	PRELIMINARY CLIENT ISSUE	I.B.	A.C.	14.03.24
B	REVISED EARTHWORKS	I.B.	A.C.	05.04.24
C	REVISED TO COMMENTS	I.B.	A.C.	23.04.24
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Height Datum	A.H.D	Client Title	MR & MRS NOCERA C/- PROFICIENT CONSTRUCTIONS (AUST)	Dwg Title
Drawn	I.B.			PROPOSED SUBDIVISION
Designed	A.C.			80 SILVERDALE ROAD, THE OAKS
Checked	A.C.			AS NOTED @ A1
Approved	A.C.	Dwg Status	DA	Local Authority
				WOLLONDILLY

#### GENERAL NOTES

- G1. ALL WORK TO BE CARRIED OUT IN ACCORDANCE WITH WOLLONDILLY SHIRE COUNCIL DEVELOPMENT CODE AND TO THE REQUIREMENTS OF COUNCIL'S AUTHORISED OFFICER.
- G2. INSPECTIONS BY THE AUTHORISED OFFICER SHALL BE CARRIED OUT AT THE FOLLOWING STAGES:
  - (a) PRIOR TO INSTALLATION OF EROSION AND SEDIMENT CONTROL STRUCTURES
  - (b) PRIOR TO BACKFILLING PIPELINES, SUBSOIL DRAINS, TRENCH BEDDING AND DAMS
  - (c) PRIOR TO CASTING OF PITS AND OTHER CONCRETE STRUCTURES, INCLUDING KERB AND GUTTER
  - (d) PROOF ROLLER TEST OF SUBGRADE AND SUB-BASE
  - (e) ROLLER TEST OF COMPLETED PAVEMENT PRIOR TO PLACEMENT OF WEARING COURSE
  - (f) FORMWORKS PRIOR TO POURING CONCRETE IN PARKING AREA FOR FOOTPATH CROSSING AND OTHER ASSOCIATED WORK
  - (g) PRIOR TO BACKFILLING PUBLIC UTILITY CROSSINGS IN ROAD RESERVES
  - (h) PRIOR TO PLACEMENT OF ASPHALTIC CONCRETE
  - (i) FINAL INSPECTION AFTER ALL WORKS ARE COMPLETED AND 'WORKS AS EXECUTED' PLANS HAVE BEEN SUBMITTED TO COUNCIL
- G3. NO TREES TO BE REMOVED UNLESS APPROVAL IS GRANTED BY COUNCIL.
- G4. MAKE SMOOTH JUNCTIONS WITH EXISTING WORKS.
- G5. NO WORK TO BE CARRIED OUT ON COUNCIL PROPERTY OR ADJOINING PROPERTIES WITHOUT THE WRITTEN PERMISSION FROM THE OWNER.
- G6. VEHICULAR ACCESS AND ALL SERVICES TO BE MAINTAINED AT ALL TIMES TO ADJOINING PROPERTIES AFFECTED BY CONSTRUCTION.
- G7. ALL RUBBISH, BUILDINGS, SHEDS AND FENCES TO BE REMOVED TO SATISFACTION OF COUNCIL'S ENGINEER AT COMPLETION OF WORKS.
- G8. A TRAFFIC CONTROL PLAN IS TO BE SUBMITTED TO COUNCIL WITH A SECTION 138 APPLICATION PRIOR TO COMMENCEMENT OF WORKS.
- G9. ALL FILL AREAS ARE TO BE INSPECTED BY A GEOTECHNICAL ENGINEER PRIOR TO STRIPPING AND ANY RECOMMENDATIONS REGARDING TREATMENT OF SALINE AFFECTATION ARE TO BE IMPLEMENTED.
- G10. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE VERIFICATION OF THE LOCATION OF ANY EXISTING SERVICES AFFECTING THE WORKS AREA, ANY DAMAGED SERVICES SHALL BE REPAIRED AT THE CONTRACTOR'S COST.

#### EARTHWORKS NOTES

- E1. EARTHWORKS TO BE CARRIED OUT TO THE SATISFACTION OF THE PCA AND GEOTECHNICAL ENGINEER. UNSOUND MATERIALS ARE TO BE REMOVED FROM ROADS AND LOTS PRIOR TO FILLING. THE CONTRACTOR IS TO ARRANGE AND MAKE AVAILABLE COMPACTION CERTIFICATES WHERE REQUIRED.
- E2. WHERE THE SLOPE OF THE NATURAL SURFACE EXCEEDS ONE IN FOUR (1:4), BENCHES ARE TO BE CUT TO PREVENT SLIPPING OF THE PLACED FILL MATERIAL AS REQUIRED BY THE PCA AND GEOTECHNICAL ENGINEER.
- E3. ALL BATTERS ARE TO BE SCARIFIED TO ASSIST WITH ADHESION OF TOP SOIL TO BATTER FACE.
- E4. PROVIDE MINIMUM 150mm AND MAXIMUM 300mm TOPSOIL WITH GRASS SEEDING ON FOOTPATHS, FILLED AREAS AND ALL OTHER AREAS DISTURBED DURING CONSTRUCTION.
- E5. THE CONTROL TESTING OF EARTHWORKS SHALL BE IN ACCORDANCE WITH THE GUIDELINES IN AUSTRALIAN STANDARD 3798 - 2007, WHERE IT IS PROPOSED TO USE TEST METHOD AS1289 E8.1 OR AS1289 E8.2 TO DETERMINE THE FIELD DENSITY, A SAND REPLACEMENT METHOD SHALL BE USED TO CONFIRM THE RESULTS AS DIRECTED BY COUNCIL. THE GEOTECHNICAL TESTING AUTHORITY SHALL HAVE A LEVEL 1 RESPONSIBILITY FOR ALL FILLING AS DEFINED IN APPENDIX B AS 3798-2007, AND AT THE END OF THE WORKS SHALL CONFIRM THE EARTHWORKS COMPLY WITH THE REQUIREMENTS OF THE SPECIFICATION AND DRAWINGS.
- E6. THE CONTRACTOR SHALL CONTROL SEDIMENTATION, EROSION AND POLLUTION DURING CONSTRUCTION IN ACCORDANCE WITH MANAGING URBAN STORMWATER: SOILS AND CONSTRUCTION VOLUME 1 (LANDCOM 2004) AND MANAGING URBAN STORMWATER: SOILS AND CONSTRUCTION VOLUME 2 (DEPARTMENT OF ENVIRONMENT AND CLIMATE CHANGE 2007).

#### ROADWORKS NOTES

- R1. SUBGRADE, SUB-BASE, AND BASE TO BE COMPAKTED IN ACCORDANCE WITH WOLLONDILLY SHIRE COUNCIL'S DEVELOPMENT CODE.
- R2. SUBSOIL DRAINS TO BE PROVIDED ON BOTH SIDES OF ROADS (EXCEPT WHERE THERE IS STORM WATER DRAINAGE).
- R3. 150 X 50 H.D. KERB OUTLETS TO BE PLACED IN LAYBACK KERB AND 90mm DIA. GALVANISED STEEL PIPE SECTION TO BE PLACED IN UPRIGHT KERB ON LOW SIDE OF LOTS. PROVIDE SUITABLE ADAPTOR TO ALLOW CONNECTION OF 90mm DIA. STORM WATER PIPE.
- R4. PERAMBULATOR CROSSINGS TO BE PROVIDED IN ALL KERB RETURNS OR WHERE REQUIRED BY COUNCIL.
- R5. SERVICE CONDUITS TO BE PLACED AS DIRECTED BY ENDEAVOUR ENERGY, TELECOMMUNICATIONS AND AS REQUIRED BY THE SYDNEY WATER.
- R6. PROPOSED SERVICES CROSSING EXISTING ROADS SHALL BE THRUST BORED UNDER THE ROAD SO AS NOT TO DAMAGE EXISTING SURFACE.
- R7. SIGNPOSTING AND LINEMARKING TO CONFORM WITH AS1742.2 RAISED RETRO-REFLECTIVE PAVEMENT MARKERS TO CONFORM WITH AS1906.
- R8. STREET SIGNS TO COMPLY WITH COUNCIL'S SPECIFICATION FOR STREET NAME SIGNS AND MUST BE INSTALLED BY THE DEVELOPER.
- R9. ALL LEVELS ARE TO BE SET OUT FROM ESTABLISHED STATE SURVEY MARKS.

#### STORMWATER NOTES

- S1. ALL PIPES TO BE SPIGOT AND SOCKET, RUBBER RING JOINTED. ALL PIPES IN ROAD RESERVES (OTHER THAN ROOF WATER AND SUBSOIL) ARE TO BE STEEL REINFORCED CONCRETE PIPES.
- S2. ALL LONGITUDINAL PIPELINES IN ROADS MUST BE LOCATED UNDER KERB AND GUTTER AND BE BACKFILLED WITH 7mm AGGREGATE WHERE 10-15% OF FINES IS ALLOWABLE UNLESS OTHERWISE INDICATED ON PLANS AND APPROVED BY COUNCIL.
- S3. DRAINAGE LINES MUST BE BACKFILLED AS PER WOLLONDILLY SHIRE COUNCIL'S DEVELOPMENT CODE. THREE (3) METRES OF AGLINE WRAPPED IN GEOTECH STOCKING MUST BE PROVIDED TO ALL DOWNSTREAM PITS.
- S4. ALL GULLY PITS TO COUNCIL'S STANDARD AND LINTELS CENTRALLY PLACED AT SAG PITS.
- S5. ALL PITS MUST BE BENCHED AND STREAMLINED. PROVIDE SL72 REINFORCEMENT AND STEP IRONS IN ALL PITS OVER 1.2M DEEP.
- S6. CONCRETE TO HAVE MINIMUM COMPRESSIVE STRENGTH OF 25 MPa AT 28 DAYS UNLESS SPECIFIED OTHERWISE BY COUNCIL ENGINEER.
- S7. ALL INTER ALLOTMENT DRAINAGE MUST HAVE A MINIMUM COVER OF 300mm TO THE TOP OF PIPE UNLESS OTHERWISE APPROVED BY THE COUNCIL ENGINEER.
- S8. CATCH DRAINS MUST BE CONSTRUCTED AS PER SWMP.
- S9. ALL COMMON DRAINAGE LINES MUST BE LAID CENTRALLY WITHIN 1.2m-3.0m EASEMENTS. CLEANING EYES MUST BE PROVIDED IMMEDIATELY DOWNSTREAM OF ALL SLOPE JUNCTIONS.
- S10. ONE HUNDRED (100) YEAR OVERLAND FLOW PATHS MUST BE FORMED AND SHOWN ON WORK AS EXECUTED DRAWINGS.
- S11. ADEQUATE PROVISION TO BE MADE FOR SCOURING AND SEDIMENTATION TO ALL DRAINAGE WORKS IN ACCORDANCE WITH WOLLONDILLY SHIRE COUNCIL'S DEVELOPMENT CODE.
- S12. COMMON DRAINAGE LINES MUST BE INSTALLED AFTER SEWERAGE LINES HAVE BEEN INSTALLED WHERE SEWER IS PROPOSED ADJACENT TO INTER ALLOTMENT.

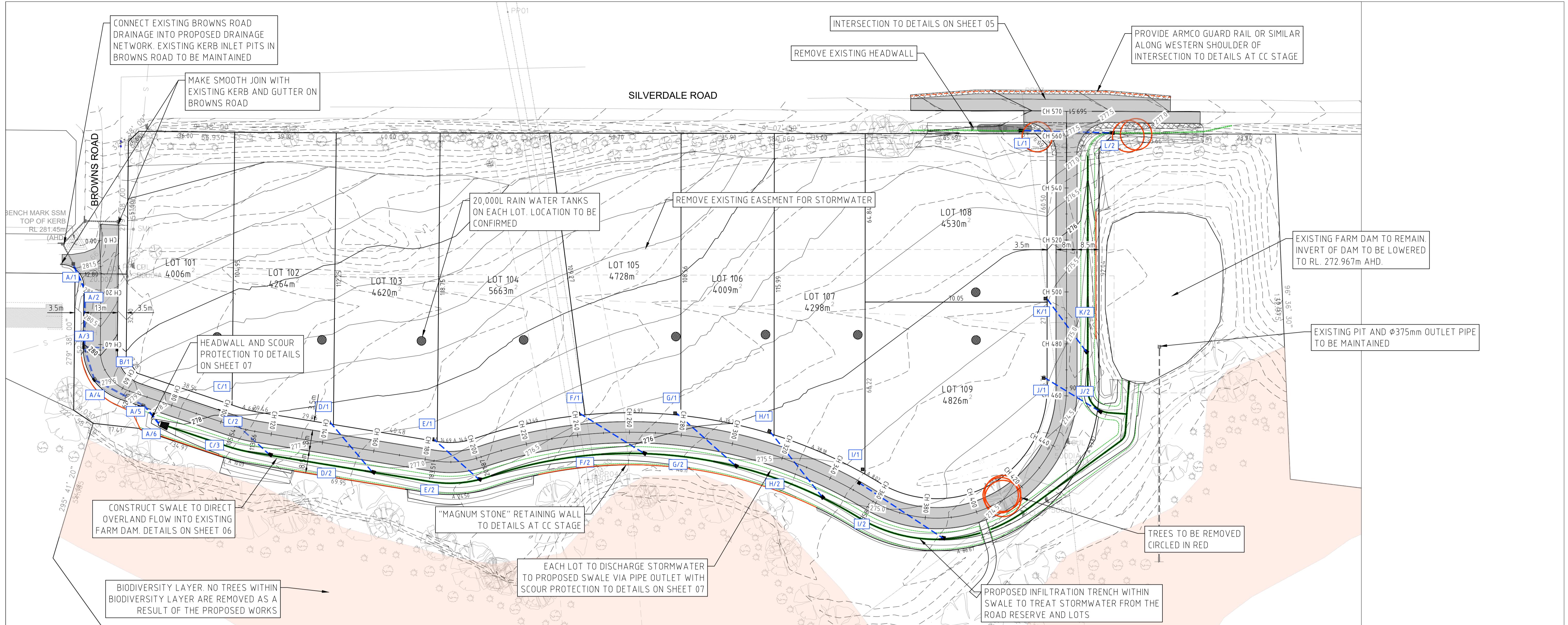
#### GEOTECHNICAL NOTES

- GT1. THE CONTRACTOR SHALL IMPLEMENT EROSION AND SEDIMENT CONTROL MEASURES AS NECESSARY, AND TO THE SATISFACTION OF COUNCIL PRIOR TO THE COMMENCEMENT OF CONSTRUCTION AND DURING CONSTRUCTION SEE SWMP.
- GT2. TESTS SHALL BE UNDERTAKEN ON ANY PROPOSED FILL MATERIALS TO ENSURE THAT THEY DO NOT HAVE A HIGH DISPERSION POTENTIAL AS DEFINED BY EMERSON CRUMB/DISPERSION TESTS (AS1289 C8-1980).
- GT3. ALL FILLING AND PAVEMENT CONSTRUCTION MUST BE UNDERTAKEN TO THE REQUIREMENTS OF AS3798-2007 THE FOLLOWING COMPACTION LEVELS ARE RECOMMENDED.
 

LOT FILLING	98% STANDARD
ROAD SUB-BASE	100% STANDARD
ROAD BASE	95% MODIFIED
ROAD BASE	98% MODIFIED
- GT4. ALL TESTING WORKS SHALL BE CONTROLLED AND CERTIFIED BY A N.A.T.A REGISTERED LABORATORY. A COLLATED COPY OF ALL TEST CERTIFICATES, ACCOMPANIED BY AN OVERALL SITE PLAN, CLEARLY INDICATING THE LOCATION OF EACH TEST AND FILL AREAS ETC. AND THE LABORATORY CERTIFICATE COVERING THE WHOLE OF THE AREA TESTED ARE TO BE FORWARDED TO COUNCIL UPON COMPLETION.
- GT5. FINAL PAVEMENT THICKNESS TO BE DETERMINED AFTER BOXING OUT BY JOINT INSPECTION BY N.A.T.A REGISTERED LABORATORY AND COUNCIL'S ENGINEER. PAVEMENT REPORT TO BE AVAILABLE TO COUNCIL A MINIMUM OF TWO CLEAR DAYS PRIOR TO INSPECTION.

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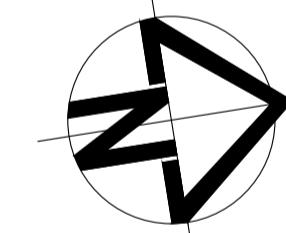
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Rev	C A1



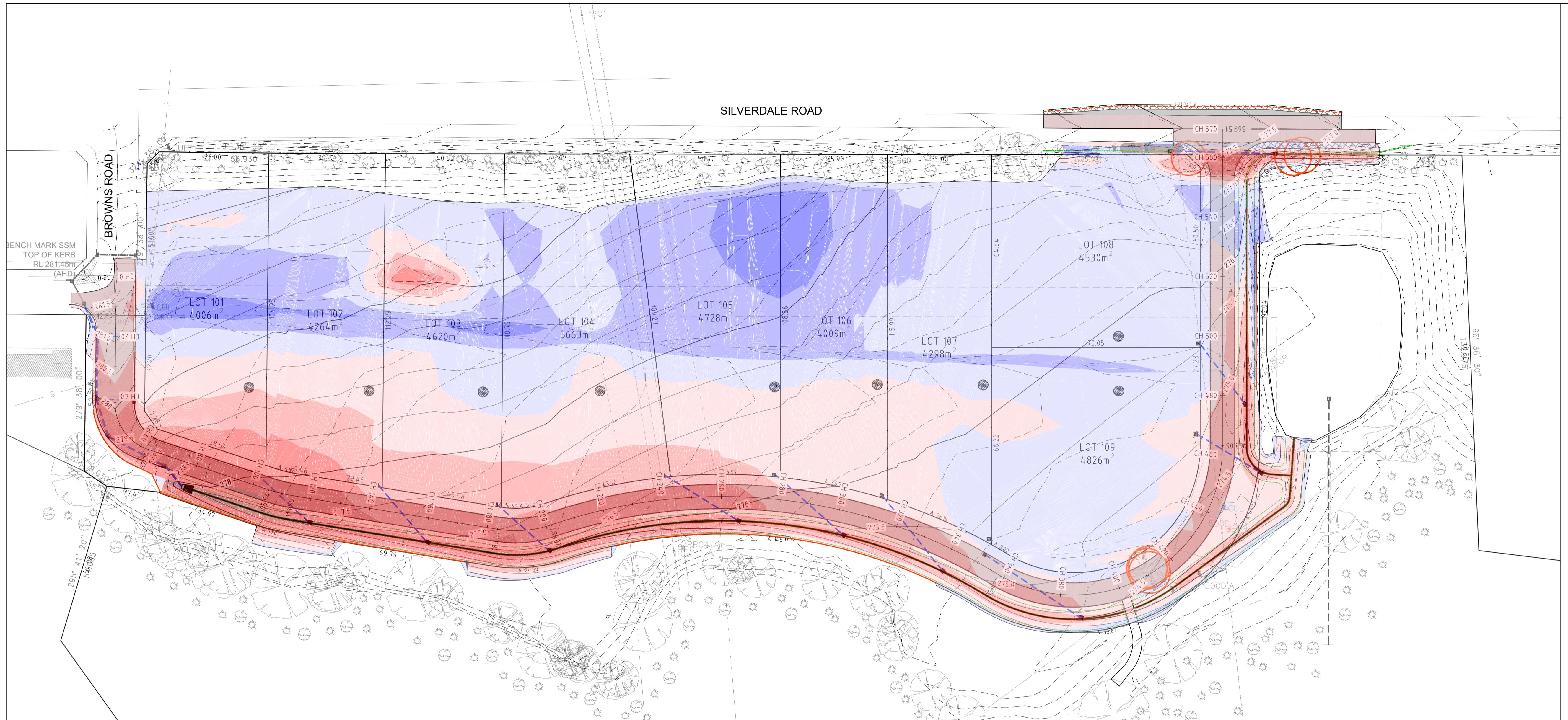
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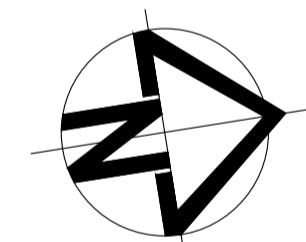
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### BULK EARTHWORKS PLAN

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SURFACE ELEVATION DATA			
NUMBER	MINIMUM ELEVATION	MAXIMUM ELEVATION	COLOR
1	-3.09	-2.50	
2	-2.50	-2.00	
3	-2.00	-1.50	
4	-1.50	-1.00	
5	-1.00	-0.50	
6	-0.50	0.00	
7	0.00	0.50	
8	0.50	1.00	
9	1.00	1.50	
10	1.50	1.80	

### CUT/FILL SUMMARY

- CUT/FILL SUMMARY ASSUMED 200mm TOP SOIL STRIPPING PRIOR TO EXCAVATION OF CUT OR PLACEMENT OF FILL.

- NO ALLOWANCE MADE FOR UNSUITABLE MATERIAL THAT MAY BE ENCOUNTERED ON SITE.

#### SUMMARY

CUT=	14,095	cu.m
FILL=	17,107	cu.m
EXCAVATION OF		
TRENCHES=	275	cu.m
EXCAVATION OF		
PAVEMENT=	1957	cu.m

TOTAL IMPORT OF MATERIAL		
TO SITE=	780	cu.m

A PRELIMINARY CLIENT ISSUE  
B REVISED EARTHWORKS  
C REVISED TO COMMENTS

DRN APP DATE

I.B. A.C. 14.03.24

I.B. A.C. 05.04.24

I.B. A.C. 23.04.24

**siteplus**  
Site Plus Pty Ltd ABN 73 104 315 095  
engineering landscape design flooding management

WOLLONGONG - HEAD OFFICE  
Shop 1, 18 Arrow Avenue  
Figtree NSW 2252  
P 612 4227 4130  
F 612 4227 4133  
E info@siteplus.com.au

Height Datum A.H.D

Drawn I.B.

Designed A.C.

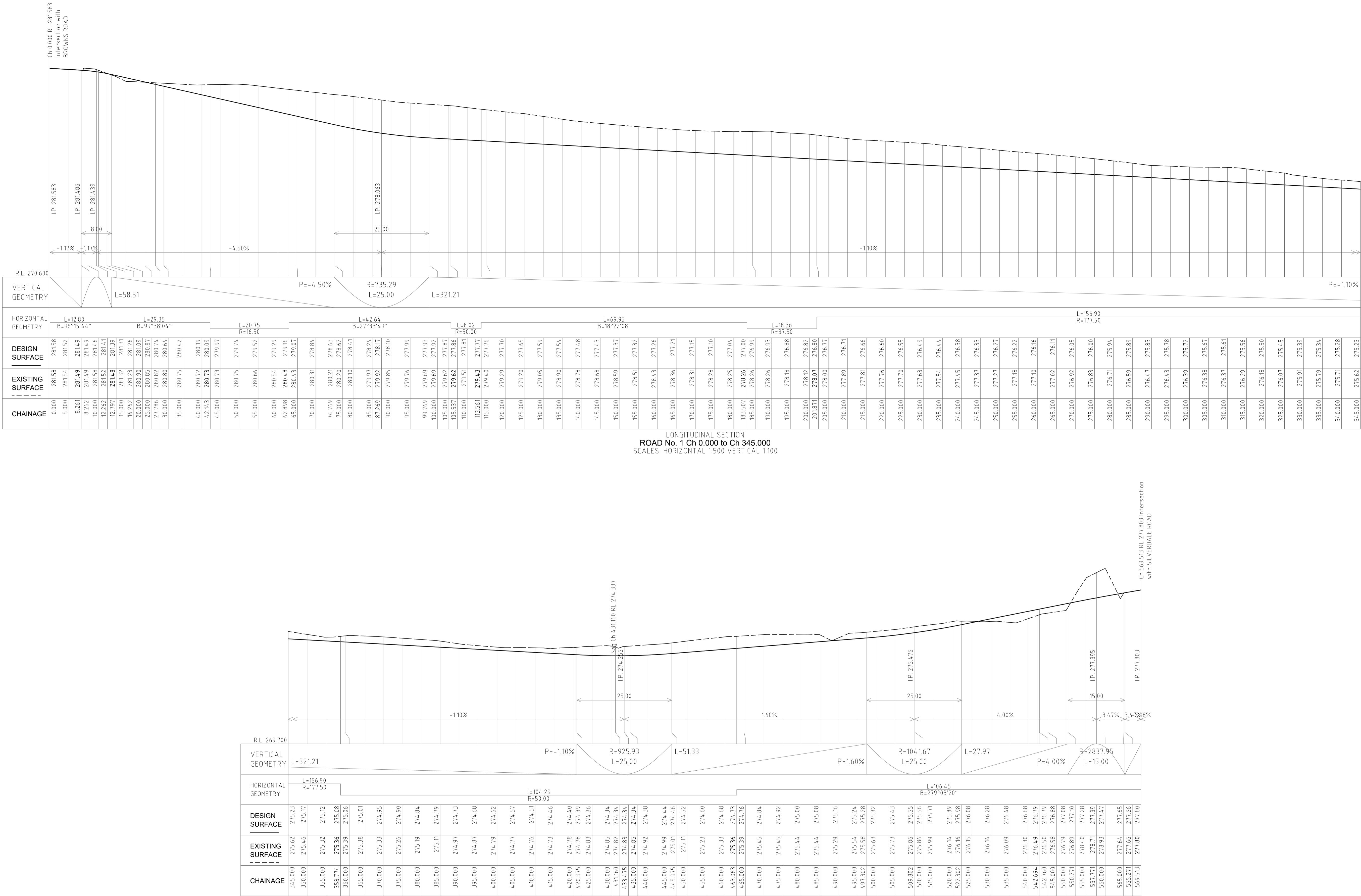
Checked A.C.

Approved A.C.

Client Title MR & MRS NOCERA C/-  
PROFICIENT CONSTRUCTIONS (AUST)  
Dwg Status DA Local Authority WOLLONDILLY

PROPOSED SUBDIVISION  
80 SILVERDALE ROAD, THE OAKS  
BULK EARTHWORKS

Ref & Dwg No  
23130.DA.C03  
Sheet No  
03 of 14  
Scale  
1:750 @ A1  
Date  
23.04.24 Rev  
C A1



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		B	REVISED EARTHWORKS
		C	REVISED TO COMMENTS
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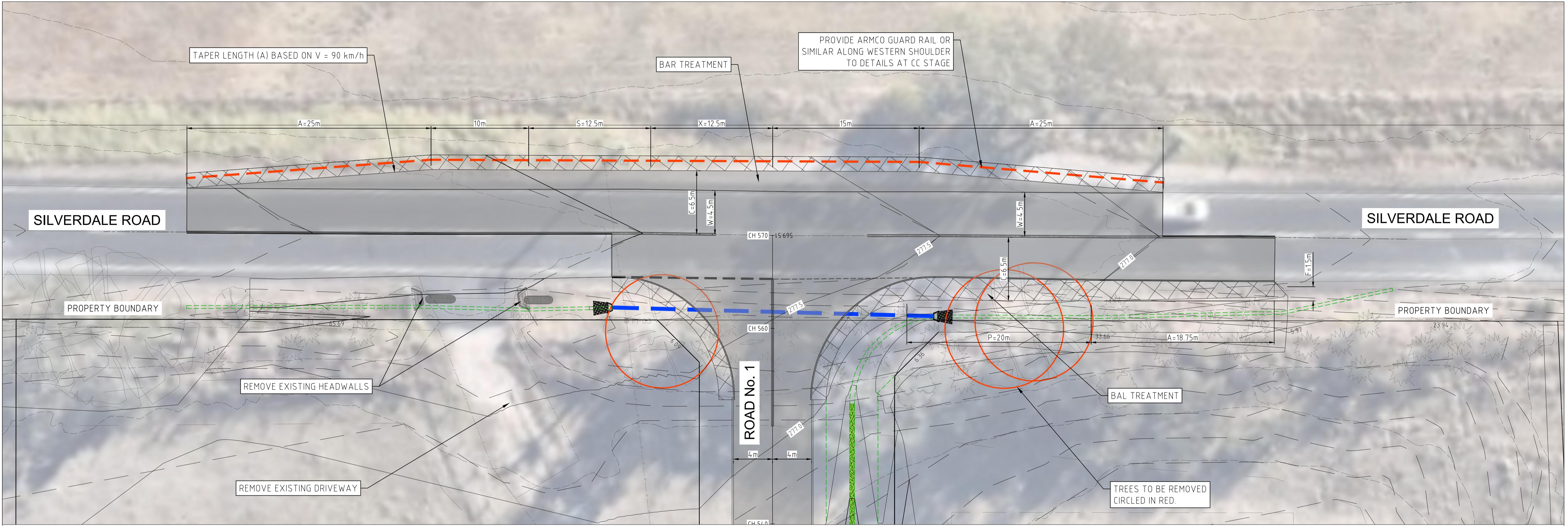
WOLLONGONG - HE  
Shop 1, 18 A  
Figtree

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	<b>PROFIC</b>
	Dwg Status

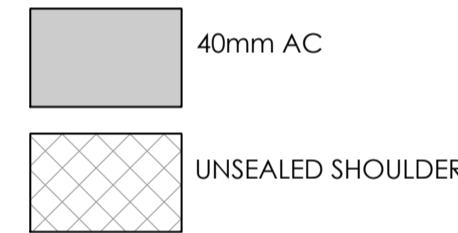
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	<b>MR &amp; MRS NOCERA C/- PROFICIENT CONSTRUCTIONS (AUST)</b>

**PROPOSED SUBDIVISION  
80 SILVERDALE ROAD, THE OAKS  
ROAD LONG SECTIONS**

Ref & Dwg No		
<b>23130.DA.C04</b>		
Sheet No		
Sheet	<b>04</b>	of <b>14</b>
Scale		
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Date	Rev	
<b>23.04.24</b>	<b>C</b>	<b>A1</b>



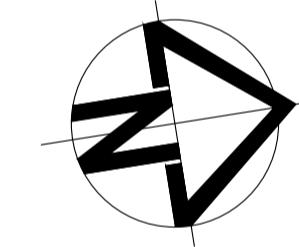
LEGEND



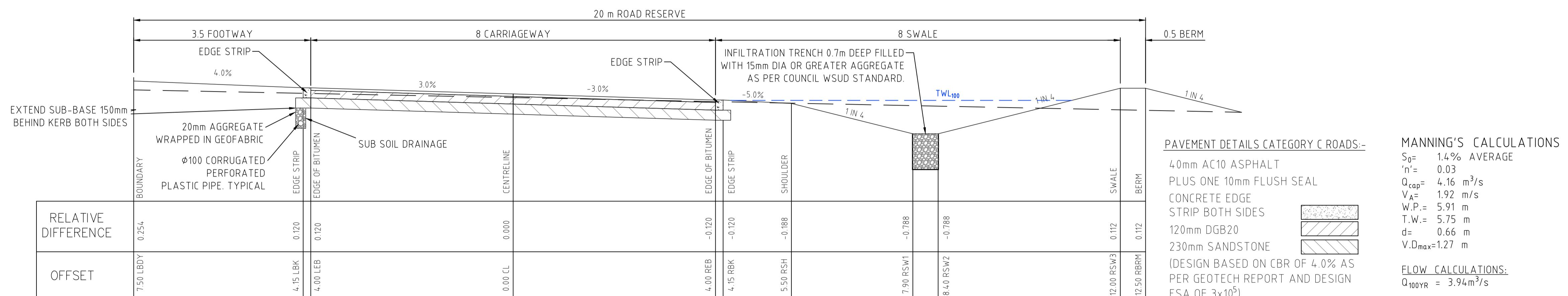
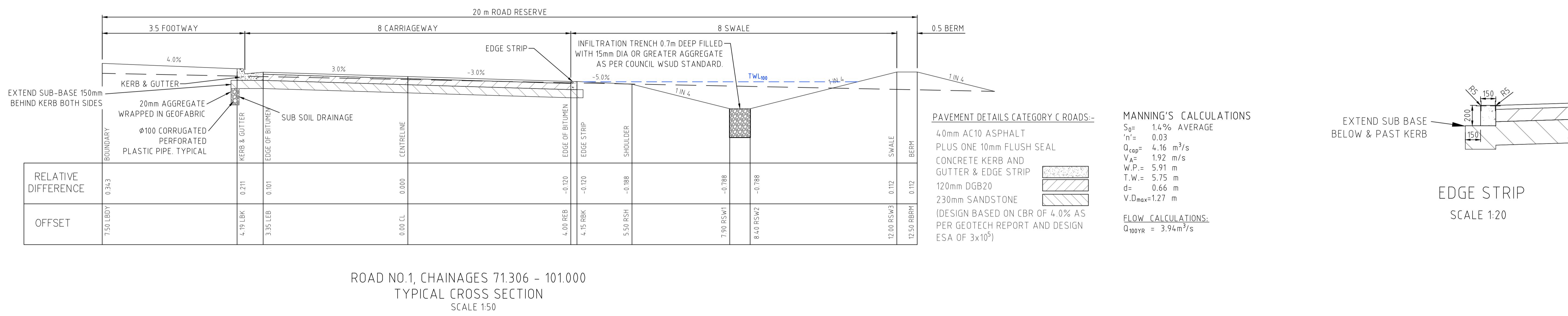
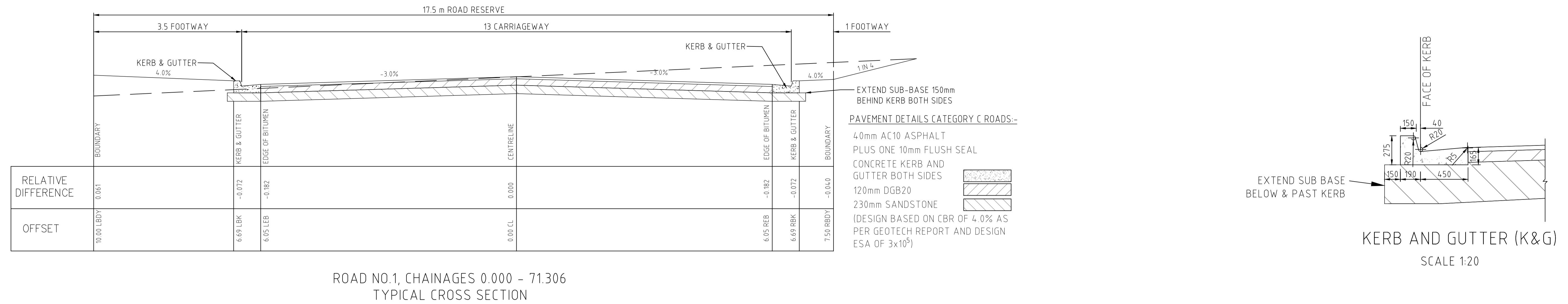
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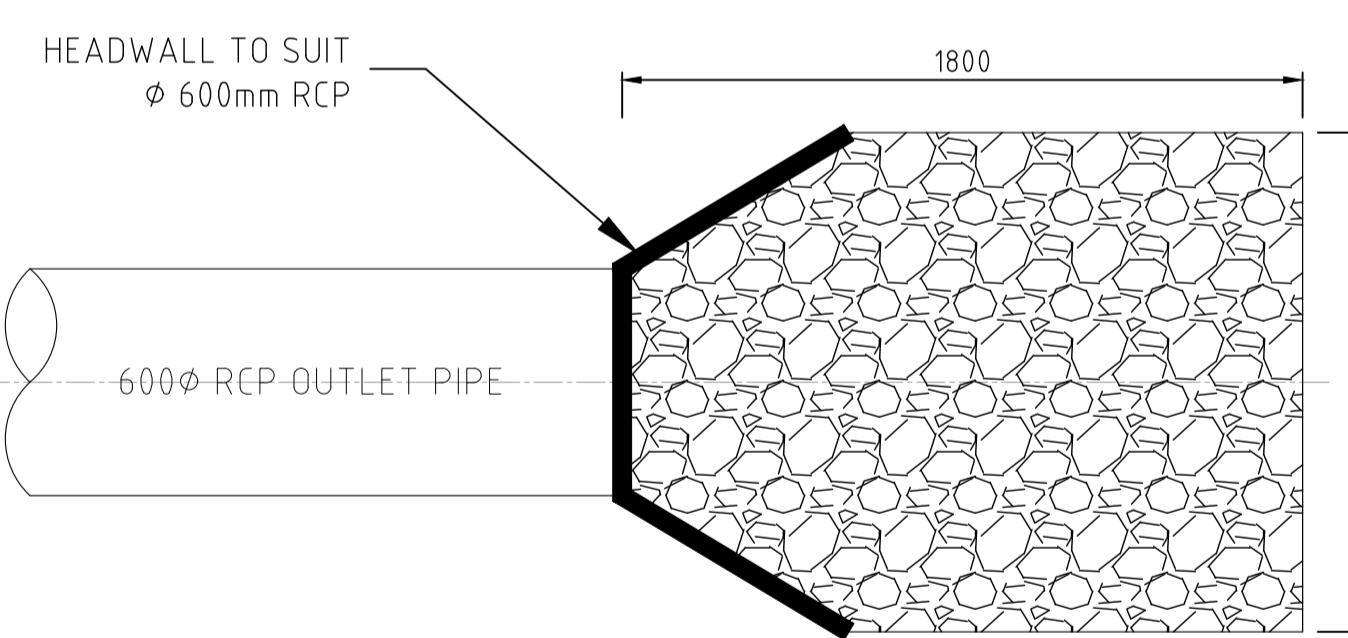
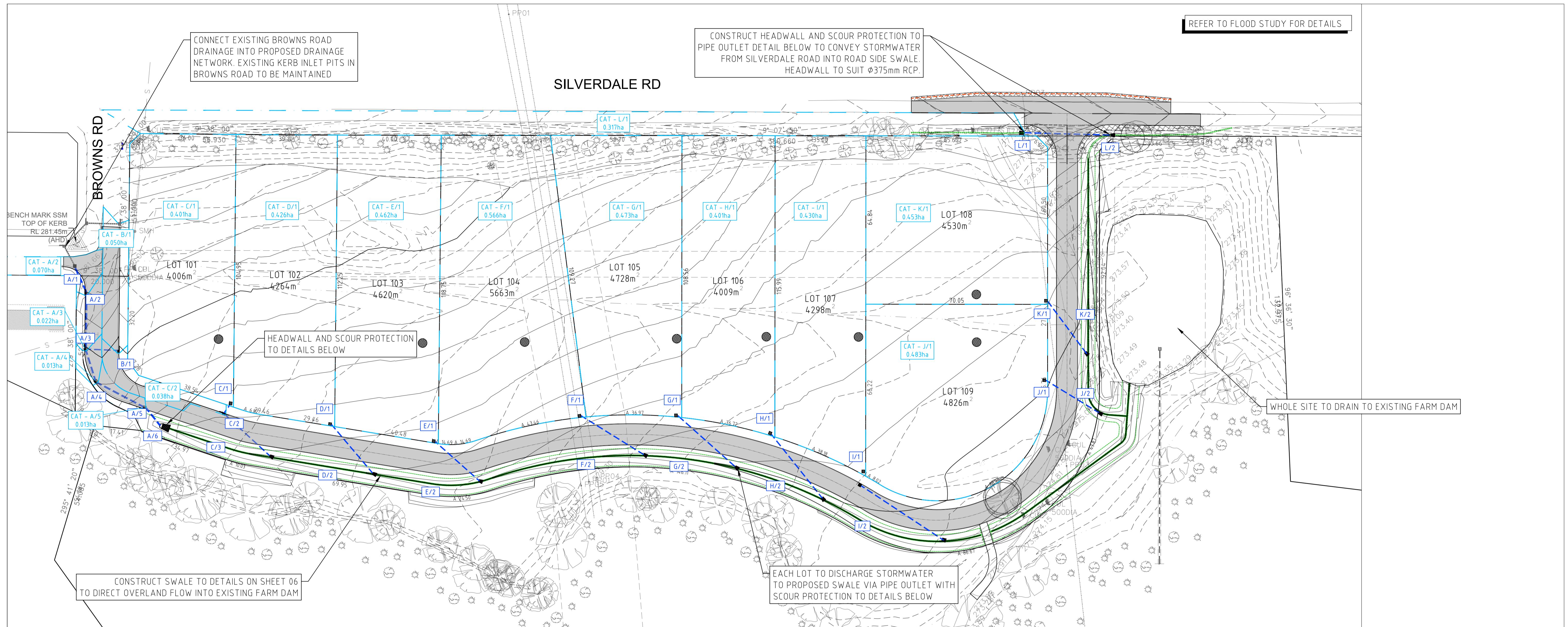
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1:400 @ A3  
METRES

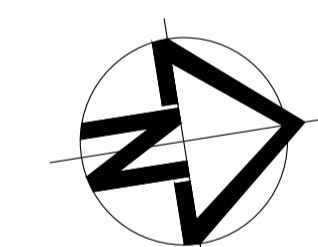


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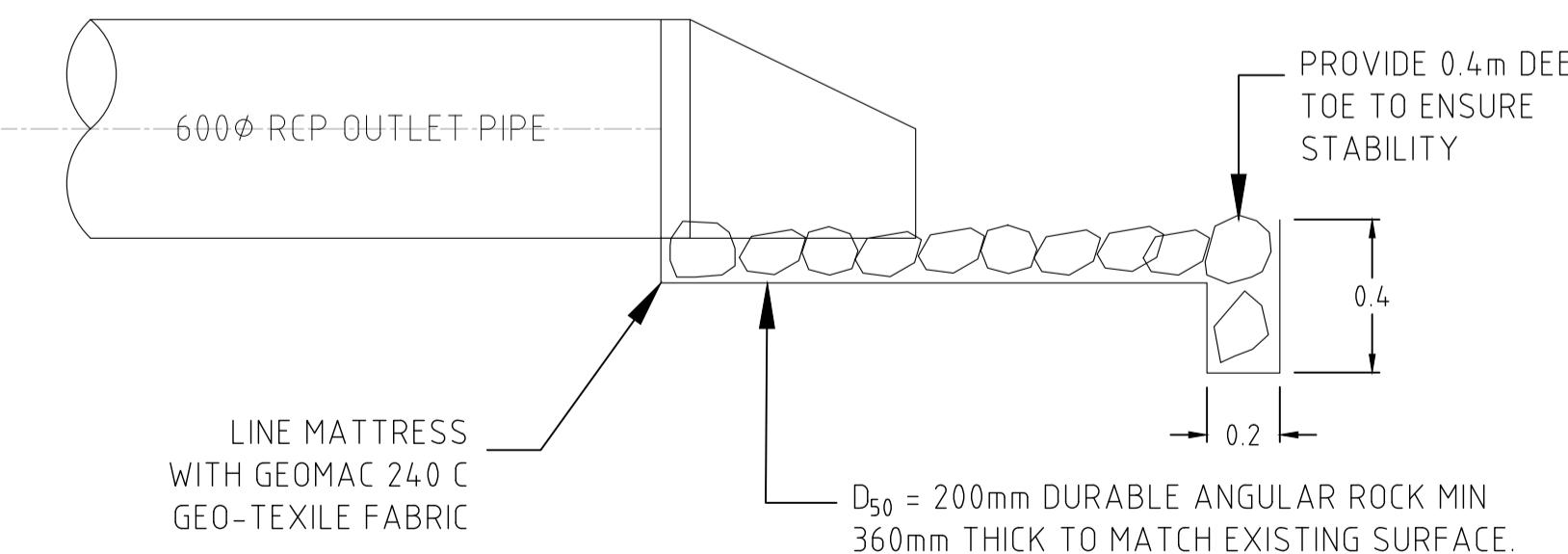
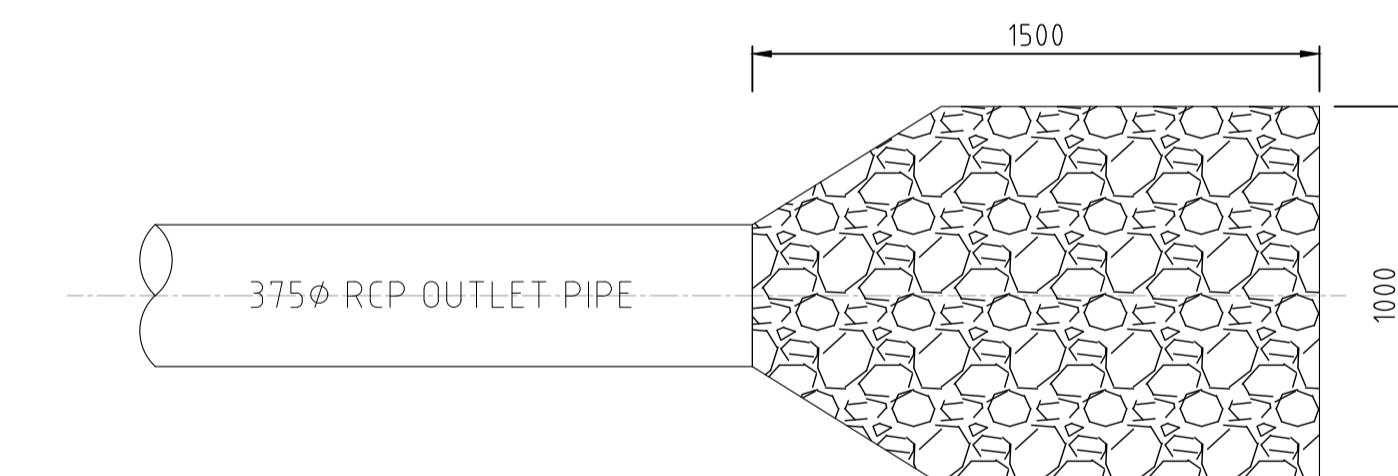




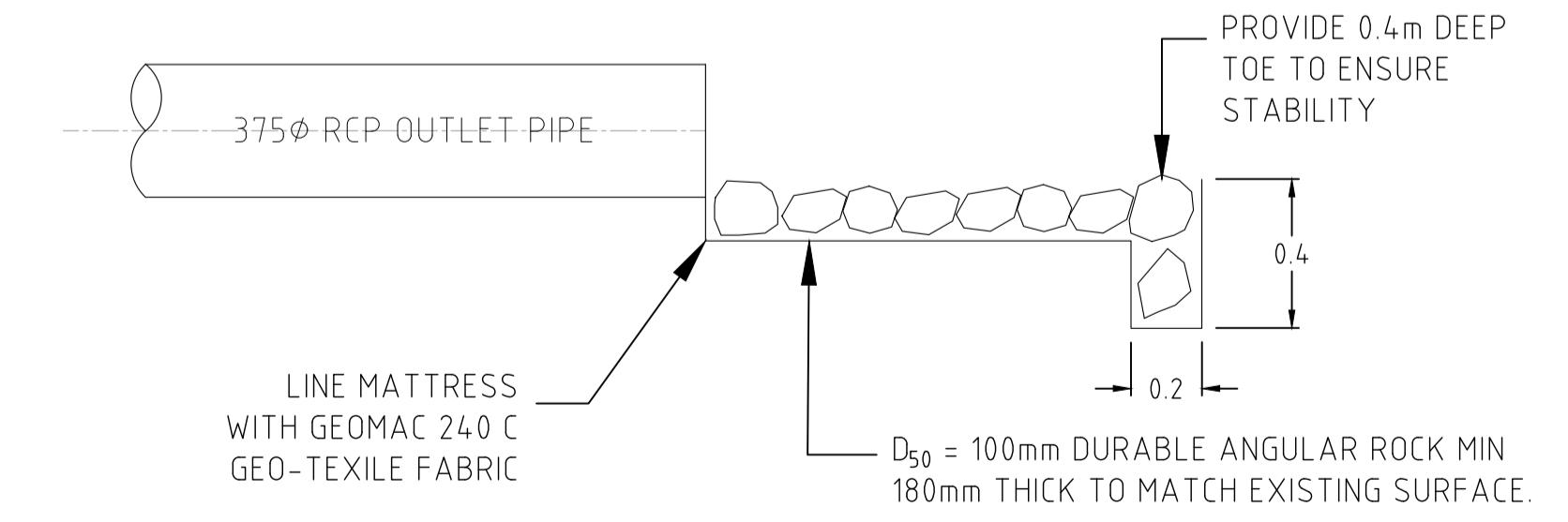
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**HEADWALL SCOUR PROTECTION DETAIL**  
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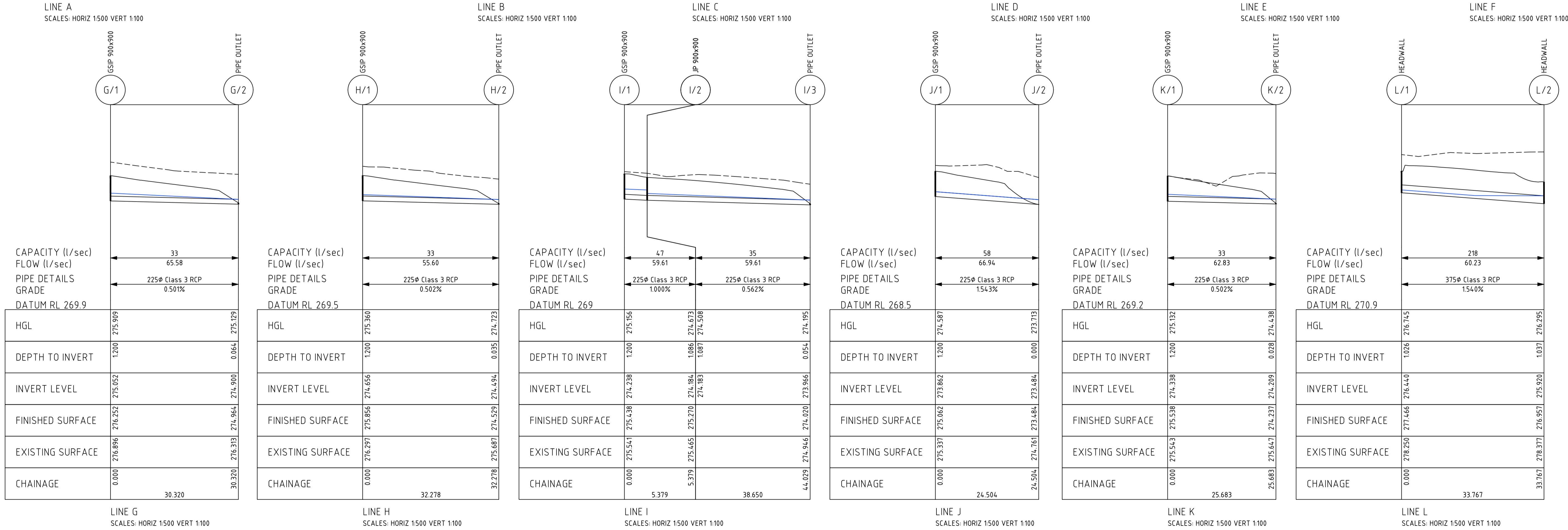
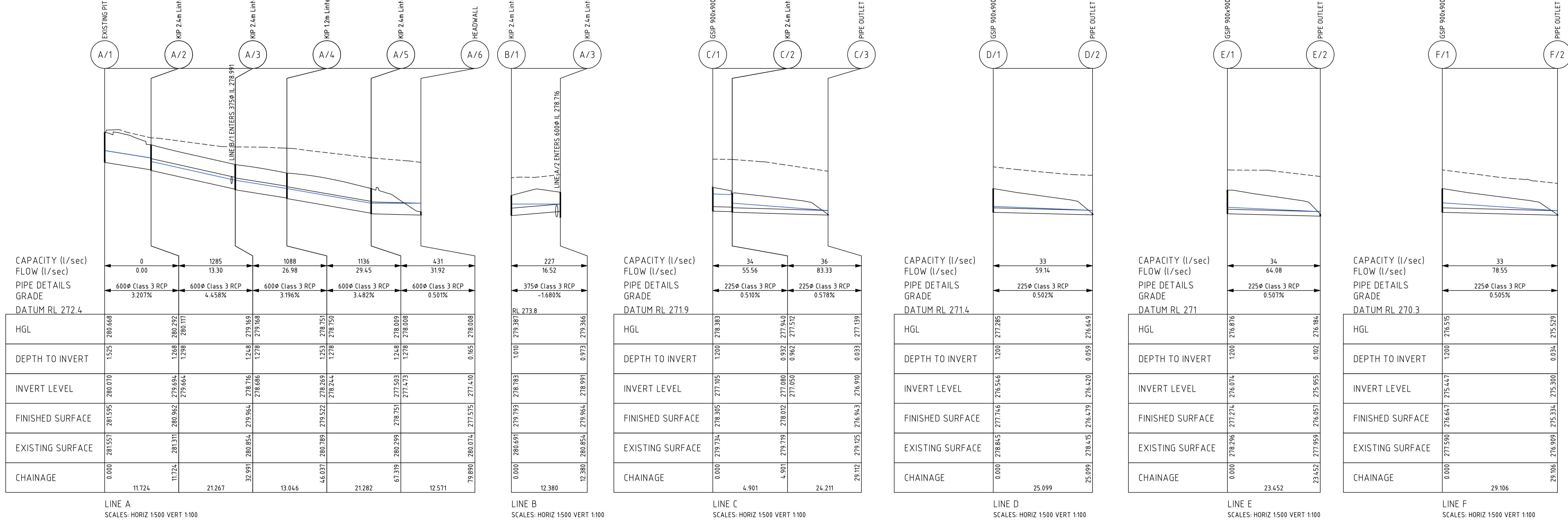


**PIPE OUTLET SCOUR PROTECTION DETAIL**  
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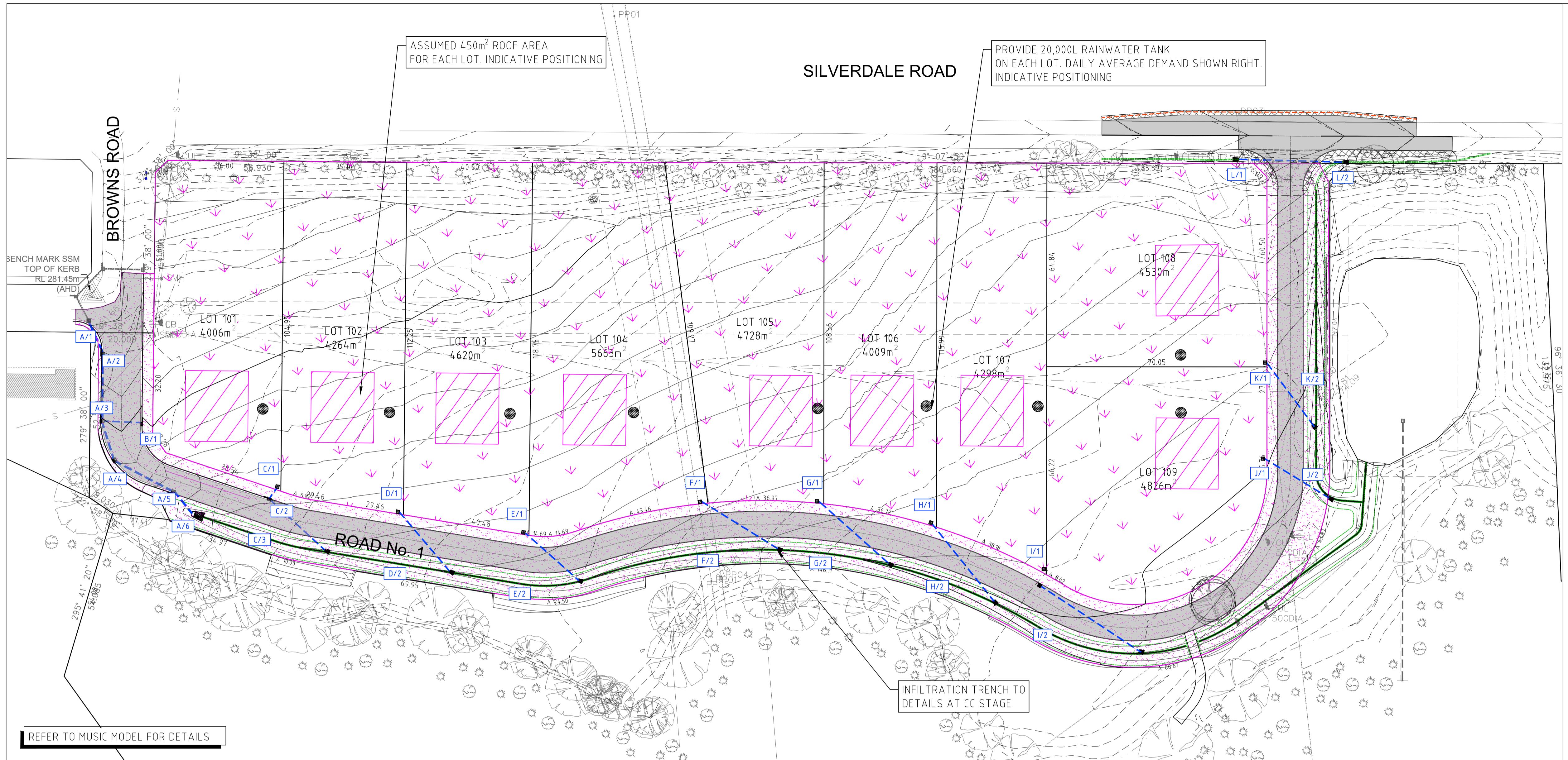
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---	B	REVISED EARTHWORKS		C	I.B.	A.C.	05.04.24							
---	C	REVISED TO COMMENTS			I.B.	A.C.	23.04.24							
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HGL Report - Site Drainage														Return Period: 20% yrs			Location: depths The Oaks-2016													
Pipe Connecting Pits (Downstream Upstream)			Pipe ID		Pipe Class		Pipe Diameter		Pipe Length		Pipe Design Flow		Mannings n	Pipe Velocity	Pipe Velocity Head	HGL at Downstream Pit	Pipe Friction Slope	HGL at Upstream Pit	Pit Loss Coefficient	Pipe Head Loss	Adopted Upstream Water Level	Pit Surcharge Level (Pit Inlet/Outlet Level)	Downstream Pipe Invert	Upstream Pipe Invert	Downstream Pipe Invert	Upstream Pipe Invert	Pipe Slope	Pipe Design Flow	Pipe HGL Capacity	Pipe Manning Capacity
A/2 A/1			Class 3 RCP	600	11.724	0.0	0.013	0.00	0.000	0.000	280.292	0.00	0.000	280.668	18.000	0.000	280.668	281.595	280.292	280.668	279.694	280.070	0.307	0.0	1500.5	0.0				
A/3 A/2			Class 3 RCP	600	21.267	13.3	0.013	0.05	1.478	0.000	279.169	0.00	0.000	280.117	22.000	0.000	280.117	280.962	279.314	280.262	278.716	279.664	4.458	13.3	1773.9	1284.9				
A/4 A/3			Class 3 RCP	600	13.046	27.0	0.013	0.10	1.634	0.000	278.751	0.00	0.000	279.168	2.650	0.001	279.169	279.964	278.867	278.284	278.269	278.686	3.196	27.0	14.97.9	1088.0				
A/5 A/4			Class 3 RCP	600	21.282	29.5	0.013	0.10	1.727	0.001	278.009	0.00	0.000	278.750	10.14	0.001	278.751	279.522	278.101	278.842	277.503	278.244	3.482	29.5	1564.6	1135.6				
A/6 A/5			Class 3 RCP	600	12.571	31.9	0.013	0.11	0.900	0.001	278.008	0.00	0.000	278.008	1.000	0.001	278.009	278.751	278.008	278.071	277.410	277.473	0.501	31.9	578.9	430.8				
A/3 B/1			Class 3 RCP	375	12.380	16.5	0.013	0.15	1.195	0.001	279.366	0.00	0.001	279.367	17.659	0.020	279.387	279.793	279.366	279.158	278.991	278.783	-1.680	16.5	318.3	227.3				
C/2 C/1			Class 3 RCP	225	4.901	55.6	0.013	1.35	1.349	0.093	277.806	0.01	0.035	277.840	4.394	0.408	278.248	278.305	277.309	277.334	277.080	277.105	0.510	55.6	46.8	33.6				
C/3 C/2			Class 3 RCP	225	24.211	83.3	0.013	2.02	2.023	0.209	277.139	0.02	0.037	277.512	14.07	0.294	278.066	278.012	277.139	277.279	276.910	277.050	0.578	83.3	50.0	35.8				
D/2 D/1			Class 3 RCP	225	25.099	59.1	0.013	1.44	1.436	0.105	276.649	0.01	0.200	276.849	4.144	0.436	277.285	277.746	276.649	276.775	276.420	276.546	0.502	59.1	46.4	33.3				
E/2 E/1			Class 3 RCP	225	23.452	64.1	0.013	1.56	1.556	0.123	276.184	0.01	0.218	276.402	3.838	0.474	276.876	277.274	276.184	276.303	275.955	276.074	0.507	64.1	46.6	33.5				
F/2 F/1			Class 3 RCP	225	29.106	78.5	0.013	1.91	1.907	0.186	275.529	0.01	0.400	275.929	3.158	0.586	276.515	276.647	275.529	275.676	275.300	275.447	0.505	78.5	46.5	33.4				
G/2 G/1			Class 3 RCP	225	30.320	65.6	0.013	1.59	1.592	0.129	275.129	0.01	0.295	275.424	3.754	0.485	275.909	276.252	275.221	274.900	275.052	275.051	0.501	65.6	46.3	33.3				
H/2 H/1			Class 3 RCP	225	32.278	55.6	0.013	1.35	1.350	0.093	274.723	0.01	0.229	274.952	4.391	0.408	275.360	275.856	274.723	274.885	274.494	274.656	0.502	55.6	46.4	33.3				
I/2			Class 3 RCP	225	38.650	59.6	0.013	1.45	1.447	0.107	274.195	0.01	0.313	274.508	1.545	0.165	274.673	275.270	274.195	274.412	273.966	274.183	0.562	59.6	49.2	35.3				
I/1			Class 3 RCP	225	5.379	59.6	0.013	1.45	1.447	0.107	274.673	0.01	0.044	274.717	4.113	0.440	275.156	275.438	274.413	274.467	274.184	274.238	1.000	59.6	66.6	47.1				
J/2 J/1			Class 3 RCP	225	24.504	66.9	0.013	1.63	1.625	0.135	273.713	0.01	0.248	274.091	3.680	0.496	274.587	275.062	273.713	274.091	273.484	273.862	1.543	66.9	83.4	58.5				
K/2 K/1			Class 3 RCP	225	25.683	62.8	0.013	1.53	1.526	0.119	274.438	0.01	0.230	274.668	3.912	0.464	275.132	275.538	274.438	274.567	274.209	274.338	0.502	62.8	46.4	33.4				
L/2 L/1			Class 3 RCP	375	33.767	60.2	0.013	0.55	1.441	0.015	276.302	0.00	0.024	276.416	11.235	0.170	276.587	277.466	276.302	276.640	275.927	276.265	1.000	60.2	243.5	175.3				

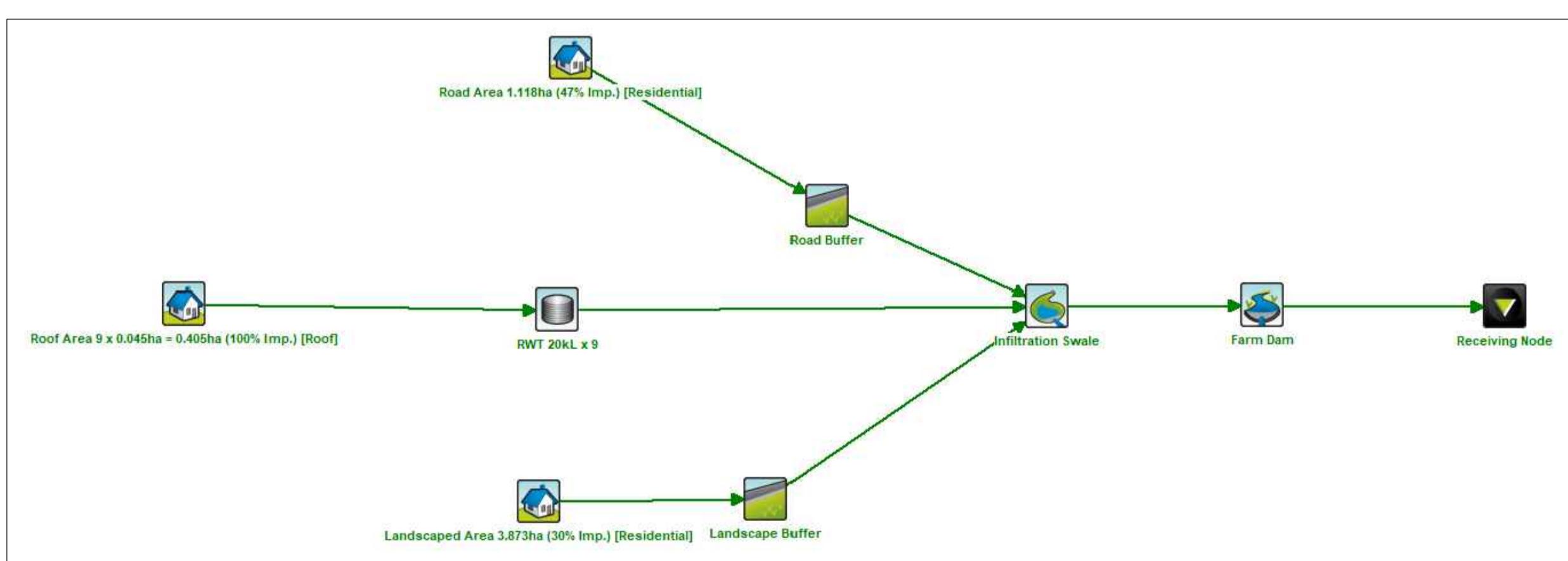
Pit Schedule - Site Drainage																						
Pit No	Pit Type		Pit Width		Pit Length		Outlet Diameter		Inlet Diameter		Inlet Invert RL		Pit Depth		Pit Lid Level		Easting		Northing		Comment	
A/6	HEADWALL						600		277.410		0.165		277.575		276228.01		6227528.060					
A/5	KIP 2.4m Lintel		600		900		277.473		600		277.503		1.278		278.751		276218.38		6227519.980			



No.	DESCRIPTION			WOLLONGONG - HEAD OFFICE			MR & MRS NOCERA C/- PROFICIENT CONSTRUCTIONS (AUST)			PROPOSED SUBDIVISION		Ref & Dwg No
A	PRELIMINARY CLIENT ISSUE			Shop 1, 18 Arrow Avenue Figtree NSW 2525 T 612 4227 4233 F 612 4227 4133 E info@siteplus.com.au			A.H.D			Dwg Title		Sheet No
B	REVISED EARTHWORKS						Drawn I.B.					09 of 14
C	REVISED TO COMMENTS						Designed A.C.					Scale
---	----						Checked A.C.					AS NOTED @ A1
---	----						Approved A.C.			Dwg Status		Date
---	----						DA			Local Authority		Rev
---	----						WOLLONDILLY					A1
												Sheet No
												09 of 14
												Scale



MUSIC CATCHMENT PLAN  
SCALE 1:750  
0 5 10 20 30 50 70 METRES  
SCALE 1:750 @A1  
1:1500 @A3

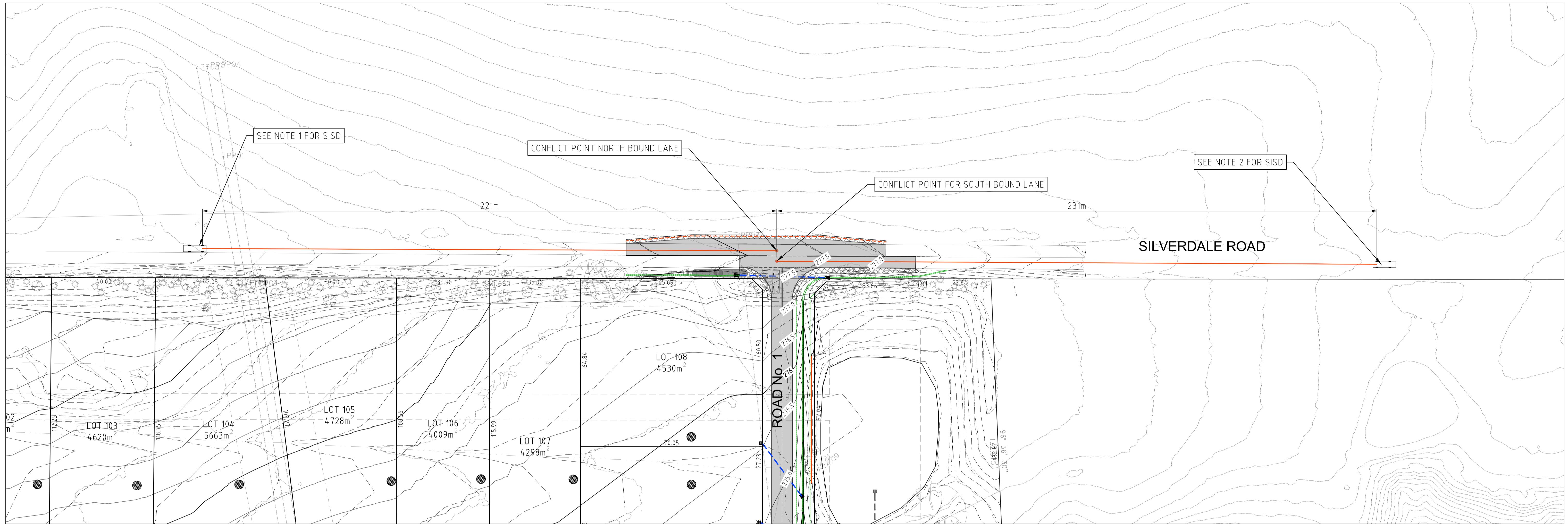


MUSIC SCHEMATIC

Treatment Train Effectiveness - Receiving Node			
	Sources	Residual Load	% Reduction
Flow (ML/yr)	39.6	13.4	66.2
Total Suspended Solids (kg/yr)	5440	399	92.7
Total Phosphorus (kg/yr)	10.2	1.79	82.4
Total Nitrogen (kg/yr)	81.9	21.7	73.5
Gross Pollutants (kg/yr)	907	0	100

MUSIC RESULTS

No.	DESCRIPTION	DRN	APP	DATE
A	PRELIMINARY CLIENT ISSUE	I.B.	A.C.	14.03.24
B	REVISED EARTHWORKS	I.B.	A.C.	05.04.24
C	REVISED TO COMMENTS	I.B.	A.C.	23.04.24
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**NOTE 1: HORIZONTAL SAFE INTERSECTION SIGHT DISTANCE**  
TABLE 3.2 AND TABLE 3.3 FROM Austroads UNSIGNALLED  
INTERSECTIONS SAFE INTERSECTION SIGHT DISTANCE (SISD):

RURAL SISD FOR 90km/h = 226 m

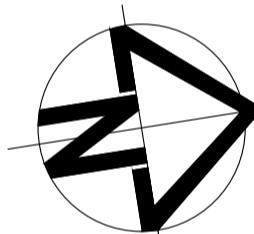
APPROXIMATE ROAD GRADIENT = 1.8 %  
UPGRADE CORRECTION TO SISD = -5 m

THEREFORE SISD FOR 90km/h = 221 m

**SAFE INTERSECTION SIGHT DISTANCE**

SCALE 1:750

0 5 10 20 30 50 70  
SCALE 1:750 @A1  
1:1500 @A3  
METRES



**NOTE 2: HORIZONTAL SAFE INTERSECTION SIGHT DISTANCE**  
TABLE 3.2 AND TABLE 3.3 FROM Austroads UNSIGNALLED  
INTERSECTIONS SAFE INTERSECTION SIGHT DISTANCE (SISD):

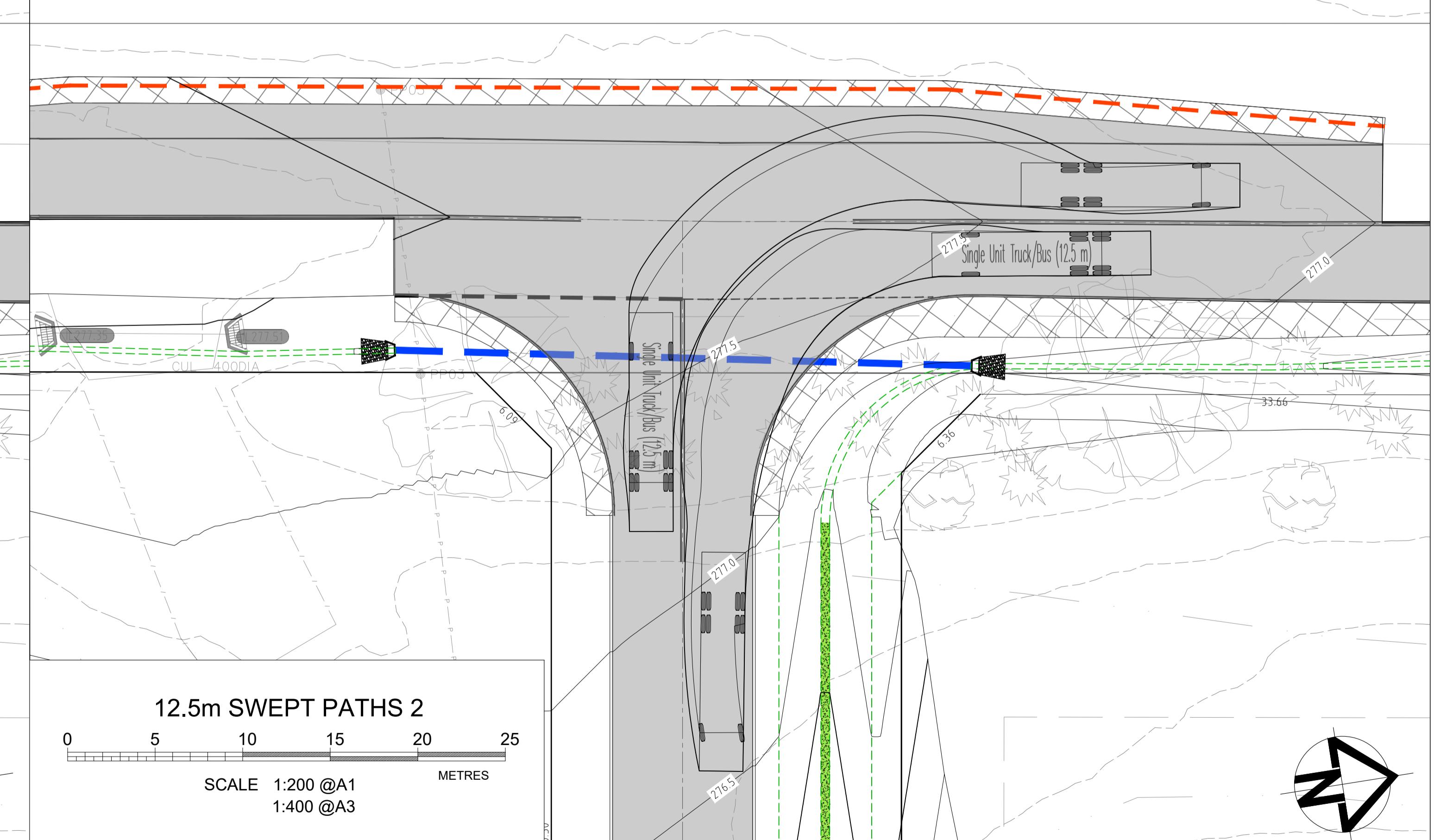
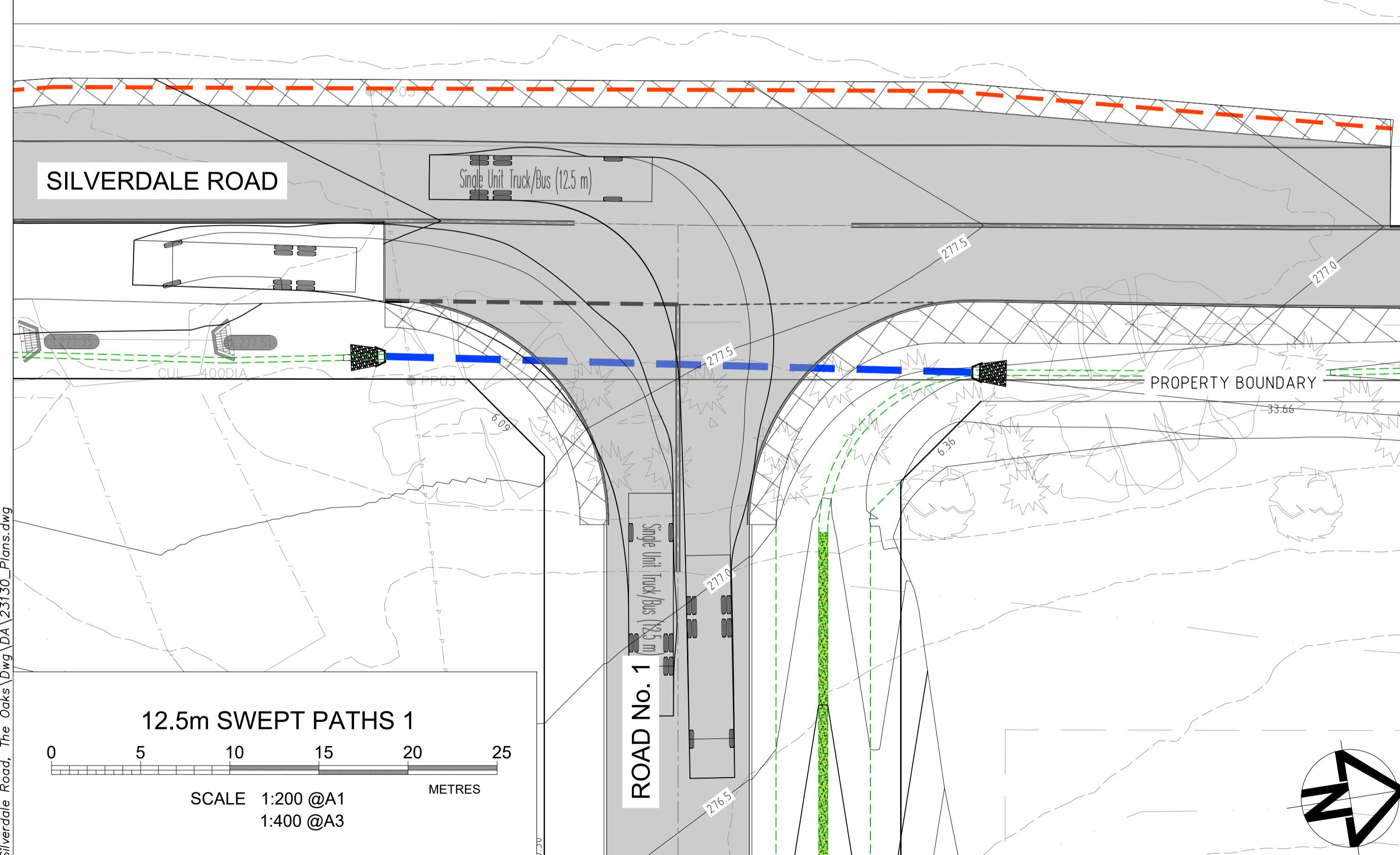
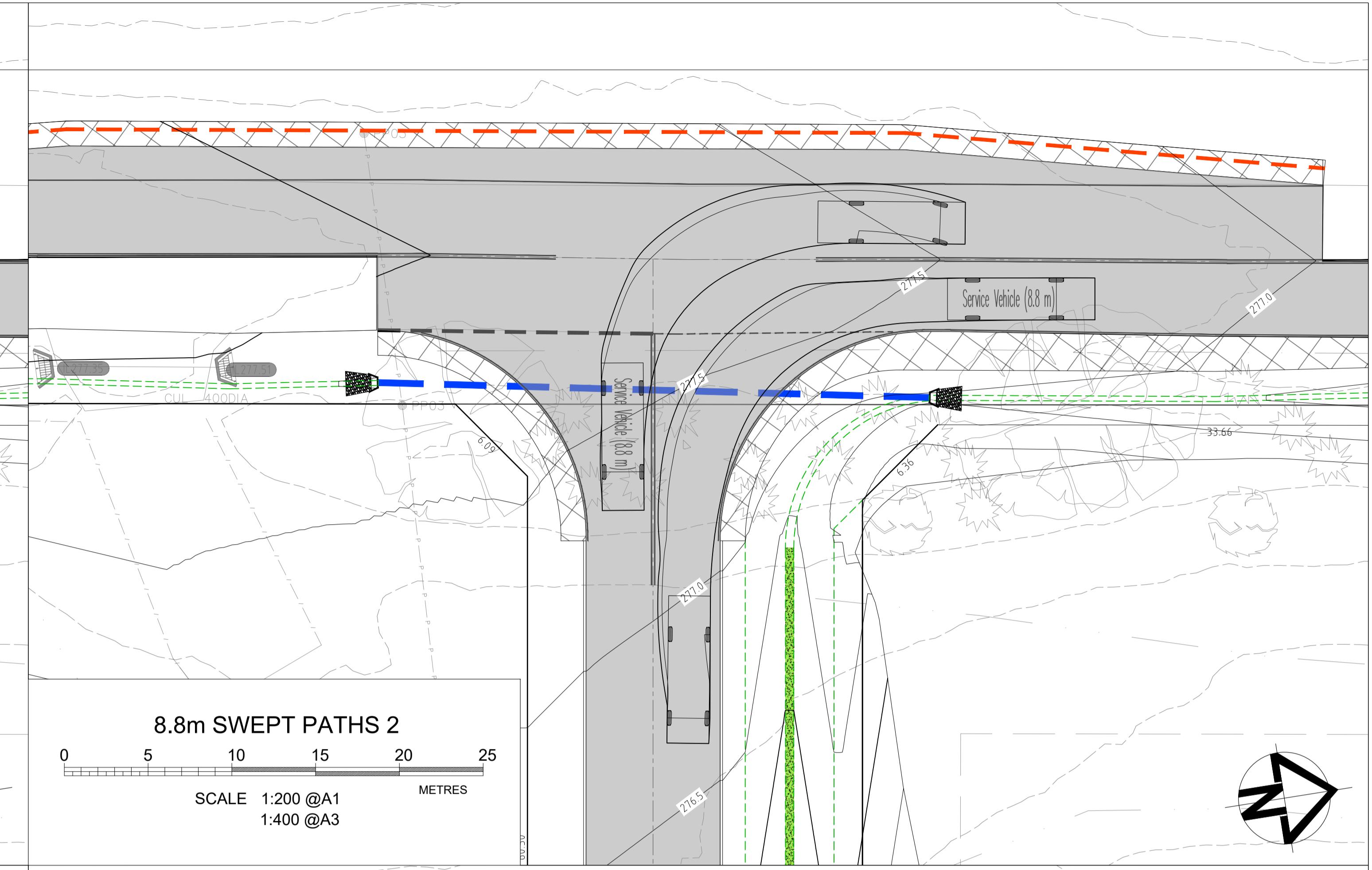
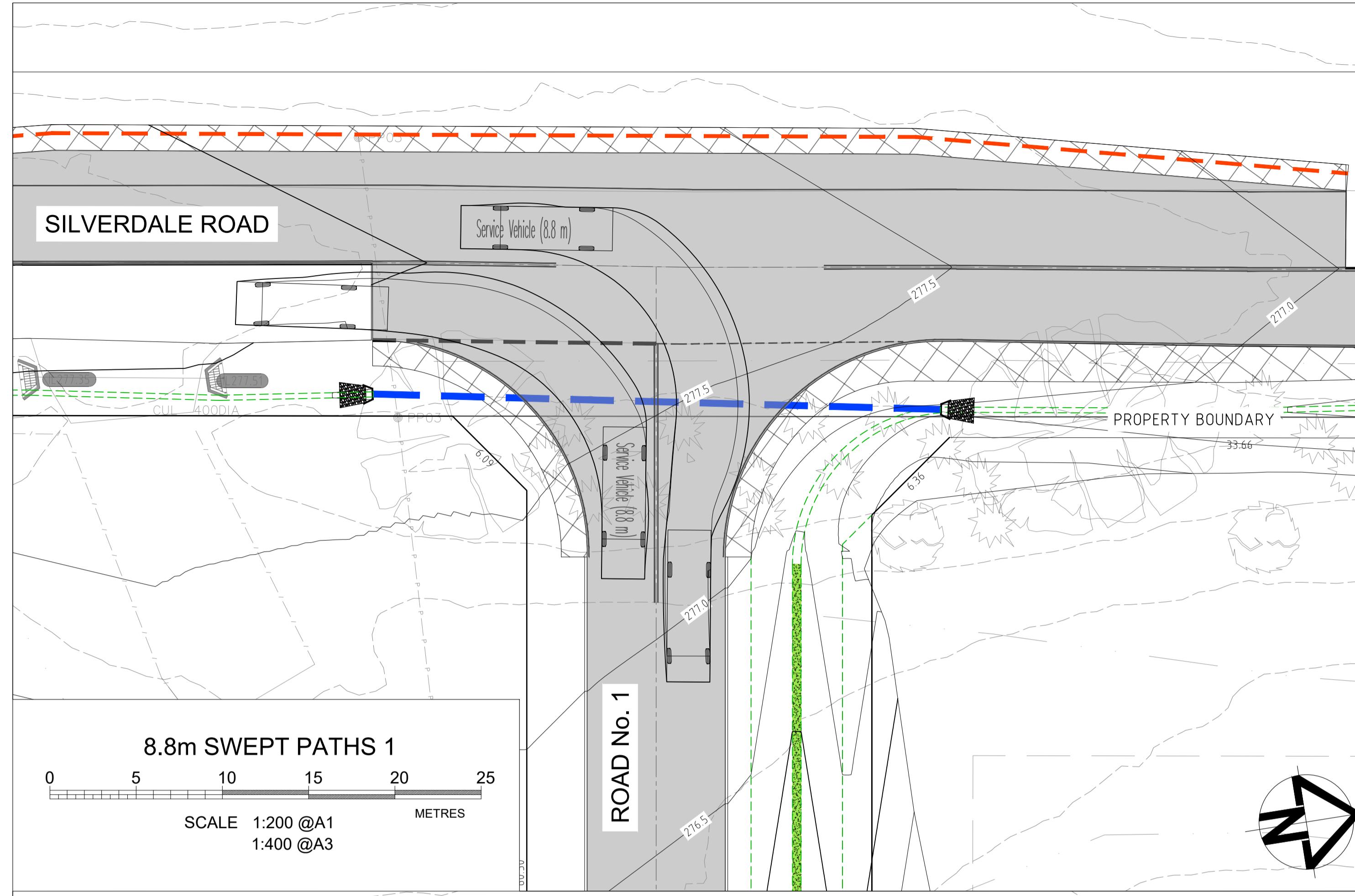
RURAL SISD FOR 90km/h = 226 m

APPROXIMATE ROAD GRADIENT = -2.0 %  
DOWNGRADE CORRECTION TO SISD = +5 m

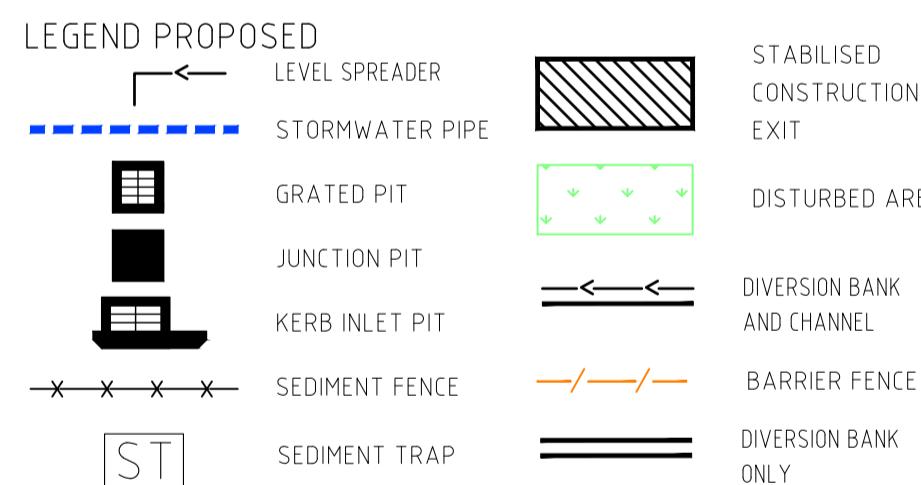
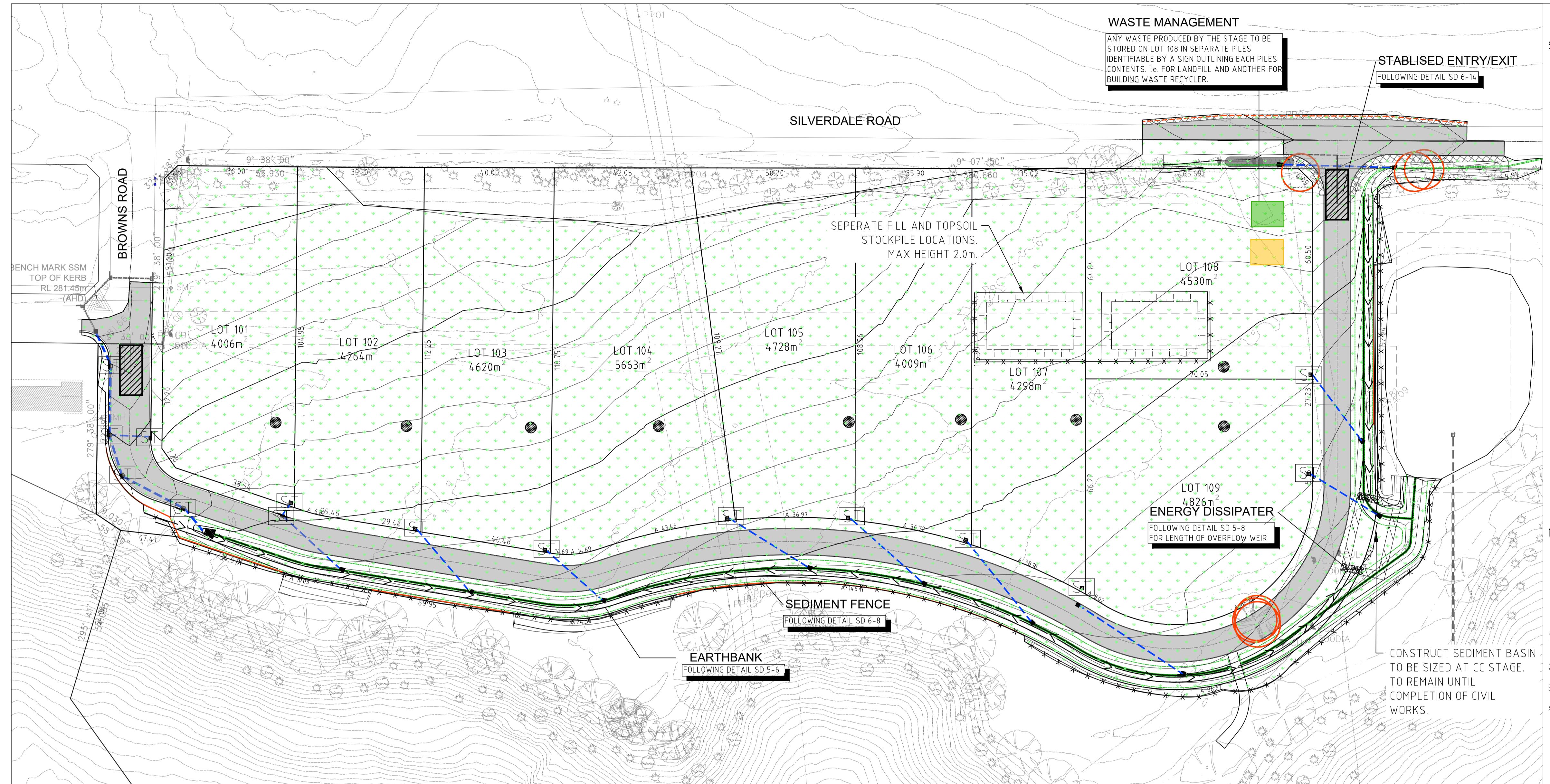
THEREFORE SISD FOR 90km/h = 231 m

No.	DESCRIPTION
A	PRELIMINARY CLIENT ISSUE
B	REVISED EARTHWORKS
C	REVISED TO COMMENTS
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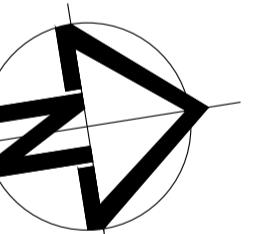
DRN	APP	DATE
I.B.	A.C.	14.03.24
I.B.	A.C.	05.04.24
I.B.	A.C.	23.04.24
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REVISIONS			DESCRIPTION		
A	DRN	APP	DATE	I.B.	PRELIMINARY CLIENT ISSUE
B	I.B.	A.C.	14.03.24	I.B.	REVISED EARTHWORKS
C	I.B.	A.C.	05.04.24	I.B.	REVISED TO COMMENTS
---	---	---	I.B.	A.C.	23.04.24
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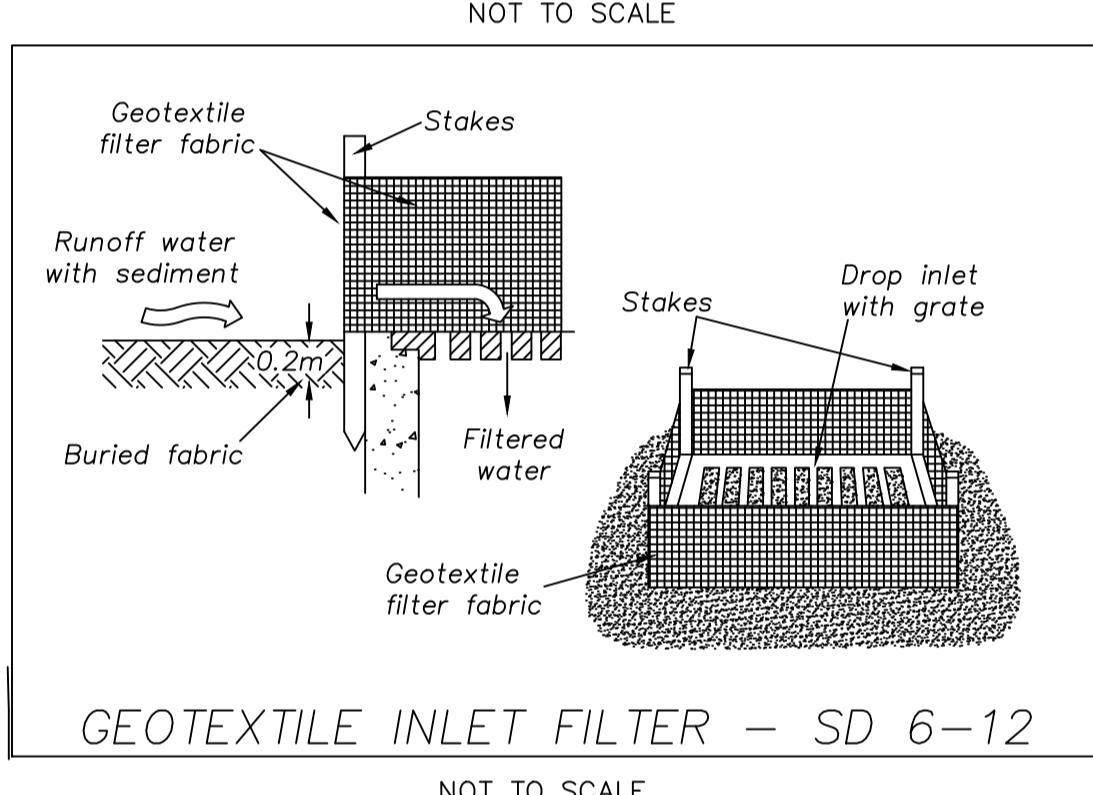
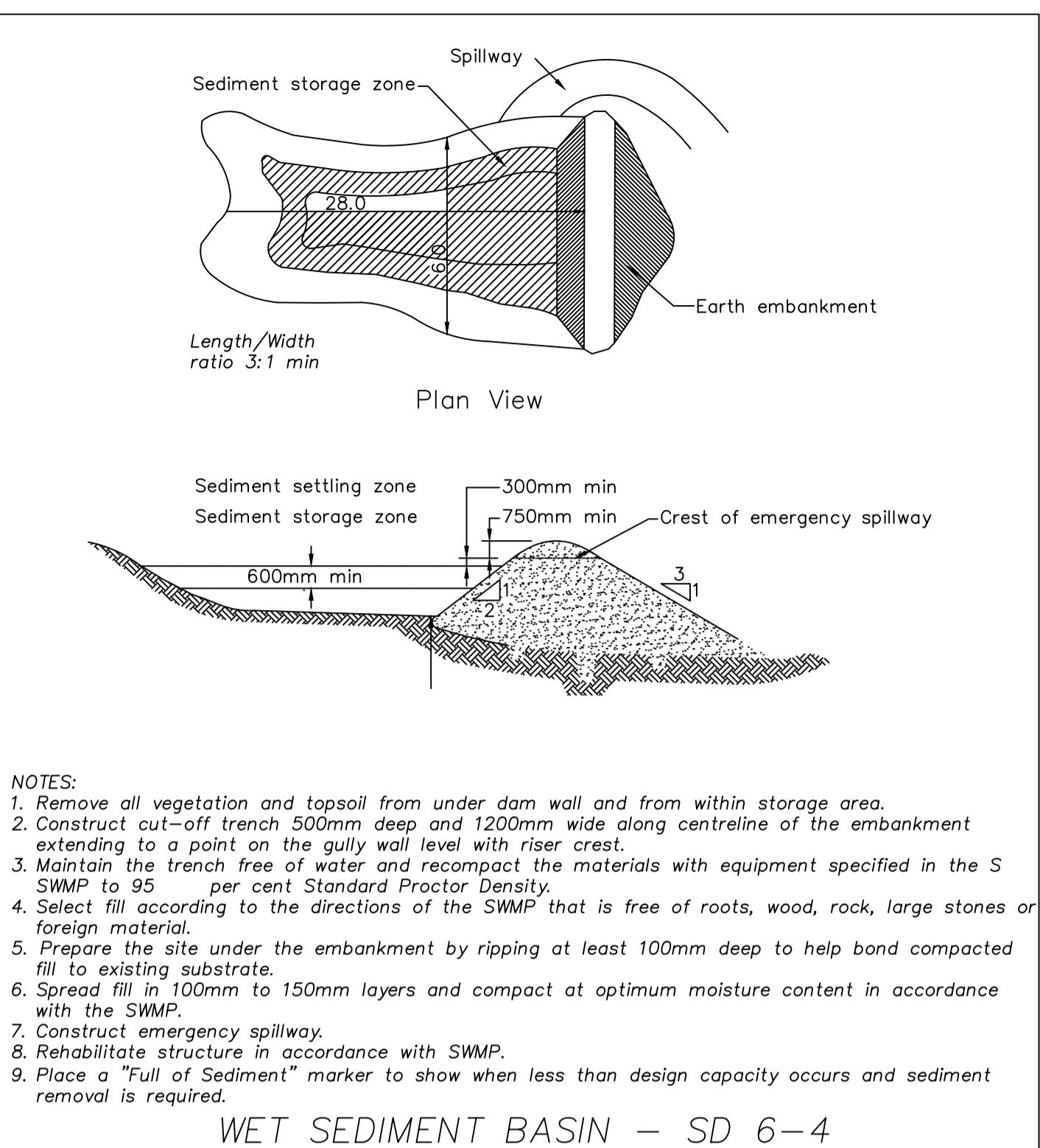
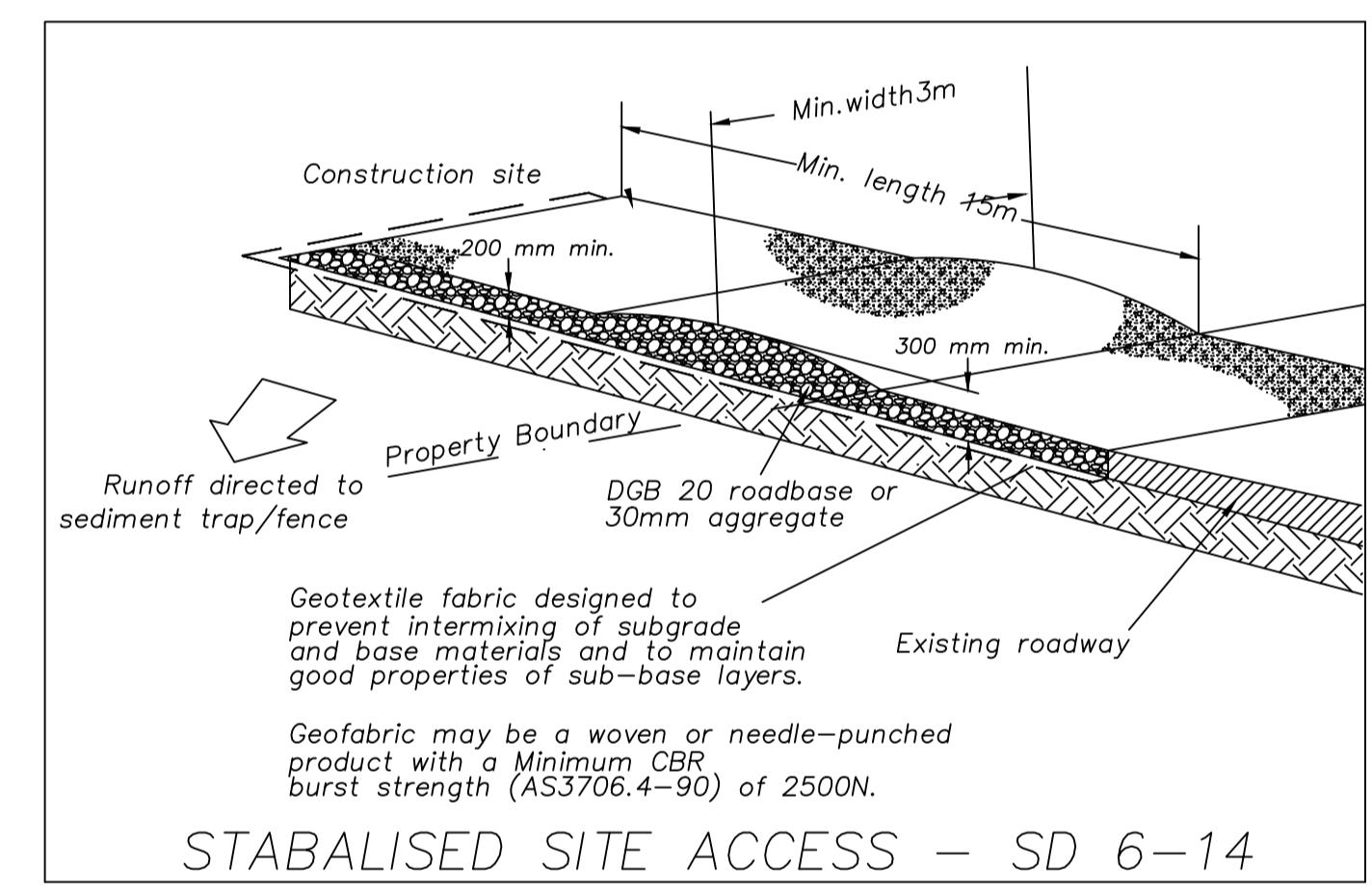
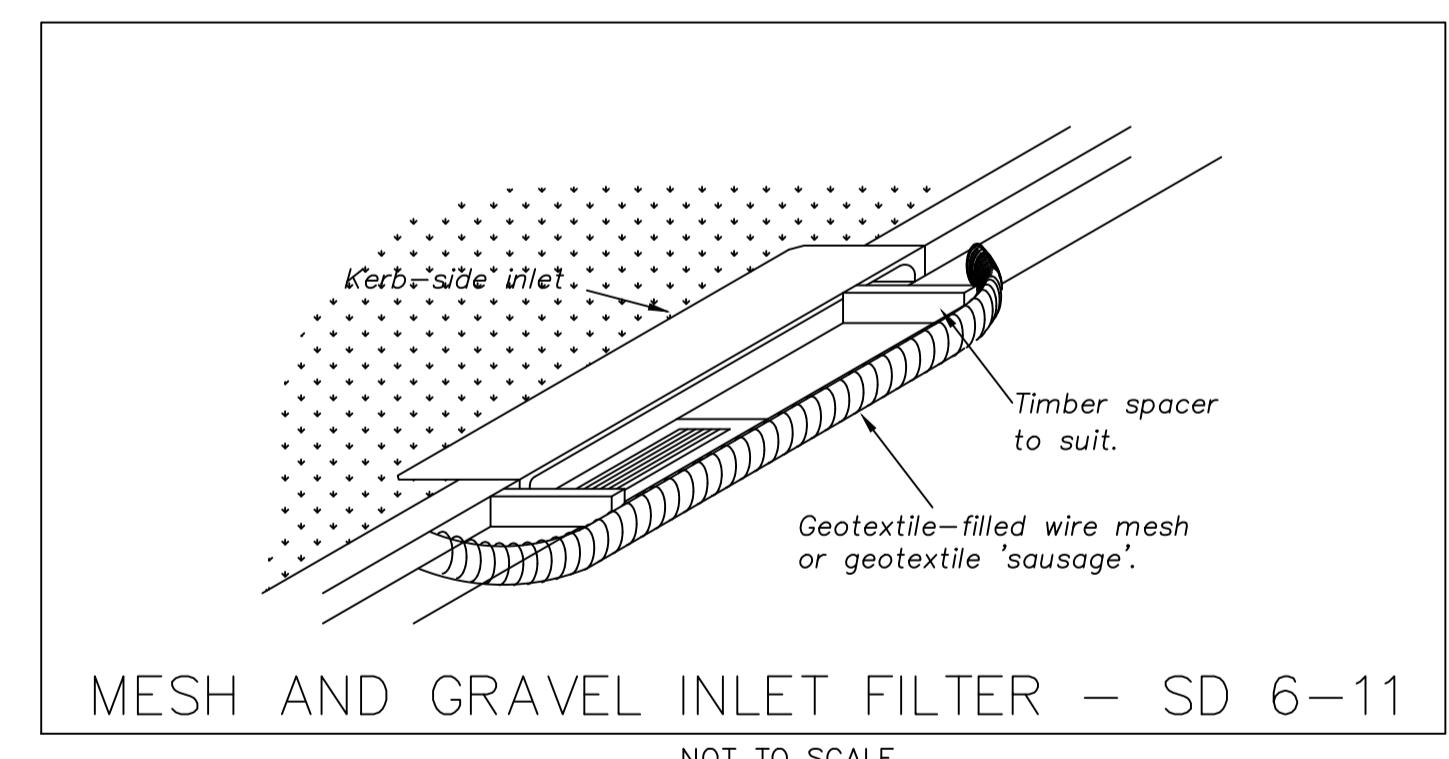
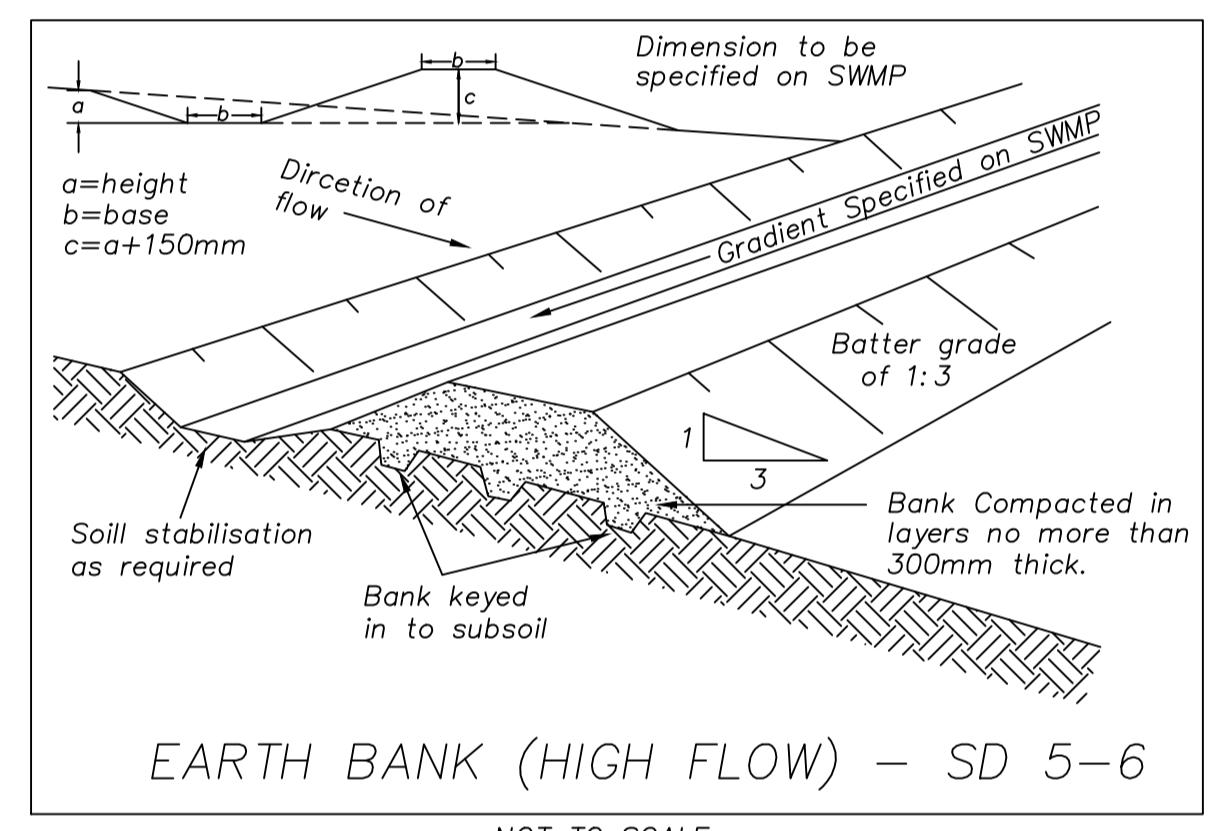
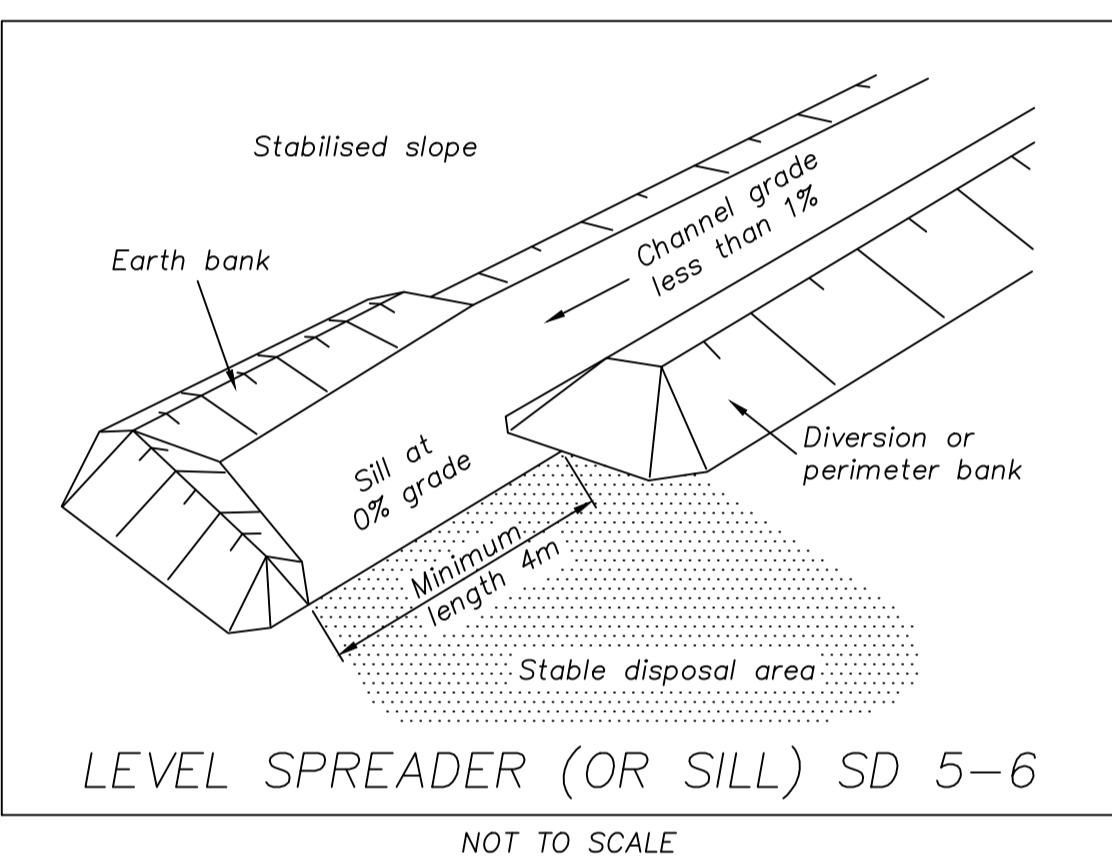
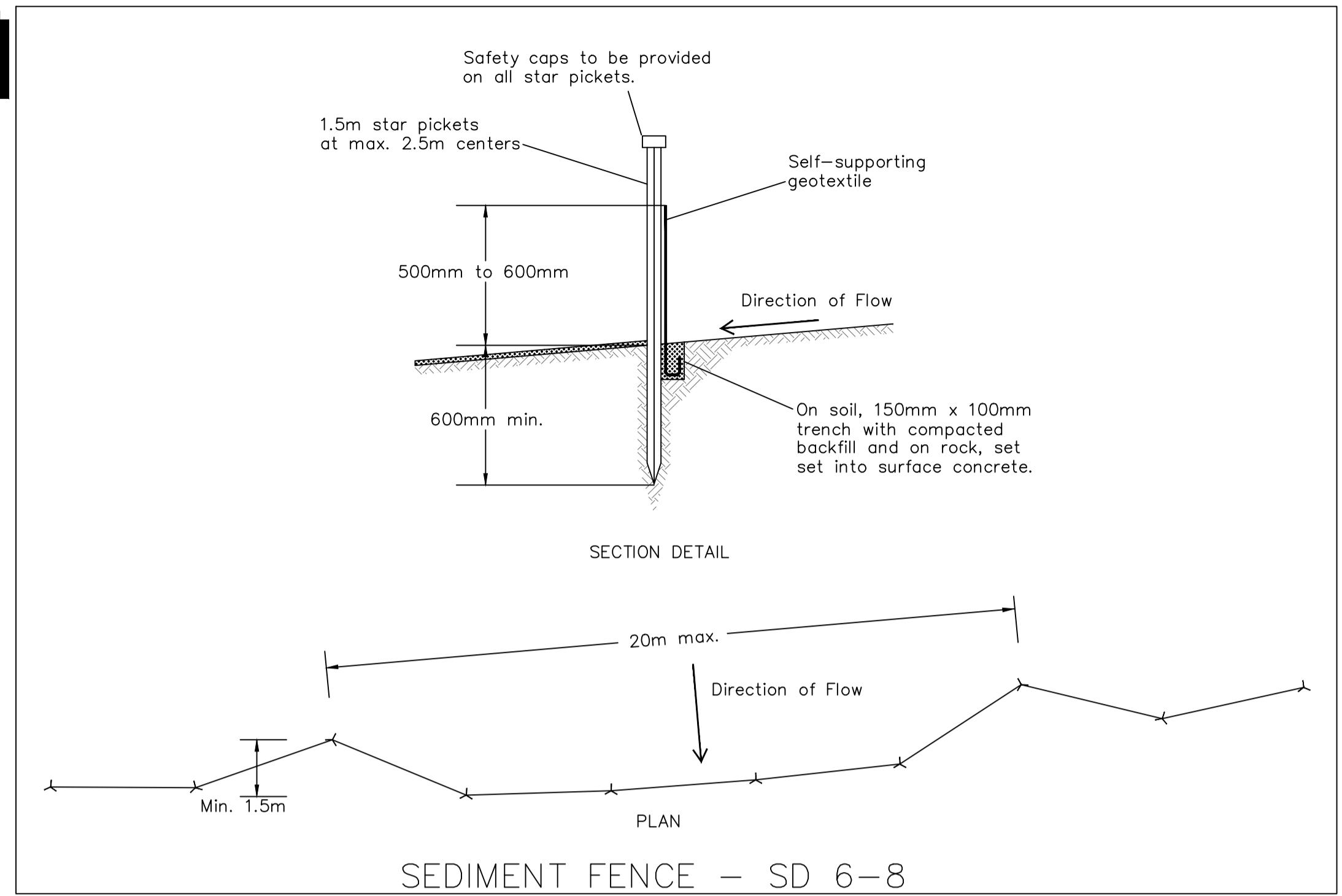
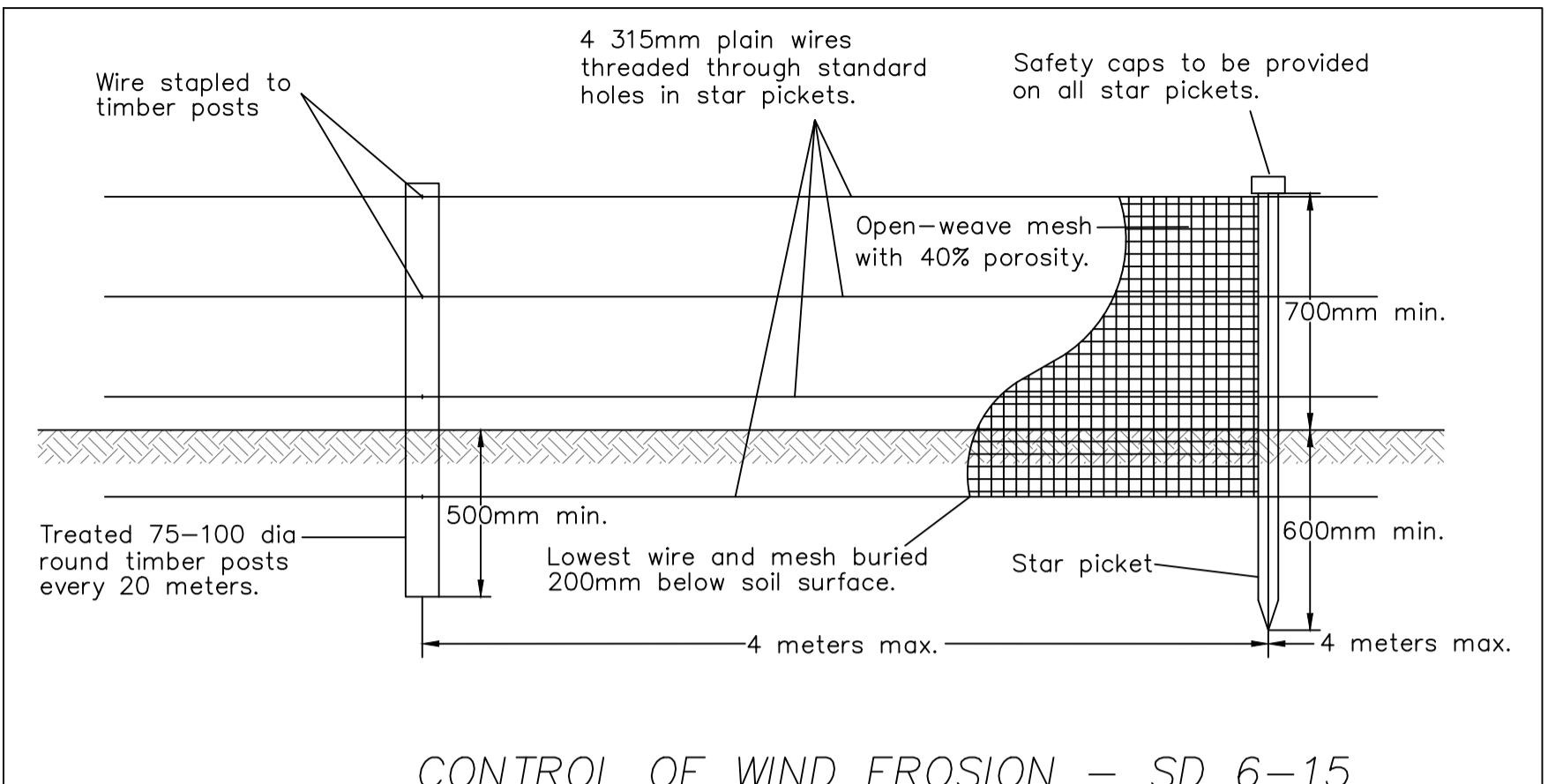
**SOIL AND WATER MANAGEMENT PLAN**  
SCALE 1:750  
0 5 10 20 30 50 70  
SCALE 1:750 @A1 METRES  
1:1500 @A3



**NOTE:** All erosion and sediment controls must be in accordance with Landcom's Managing Urban Stormwater, Soils and Construction, Volume 1, 4th Edition, March 2004

REVISIONS	No.	DESCRIPTION	DRN	APP	DATE
A		PRELIMINARY CLIENT ISSUE	I.B.	A.C.	14.03.24
B		REVISED EARTHWORKS	I.B.	A.C.	05.04.24
C		REVISED TO COMMENTS	I.B.	---	23.04.24
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**NOTE:** All erosion and sediment controls must be in accordance with Landcom's Managing Urban Stormwater, Soils and Construction, Volume 1, 4th Edition, March 2004



BASIN TO BE TREATED WITH GYPSUM FLOCCULANT AT THE RATE OF 32 kg/100 m<sup>3</sup> OF STORED WATER. THE BASIN SHOULD THEN BE DRAINED FOLLOWING A PERIOD OF AT LEAST 3 DAYS, PROVIDING WATER ANALYSIS TESTS SHOW SUSPENDED SEDIMENT CONCENTRATIONS ARE BELOW 50 mg/l.

Flocculation

NOT TO SCALE

No.	DESCRIPTION	DRN	APP	DATE
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B	REVISED EARTHWORKS	I.B.	A.C.	05.04.24
C	REVISED TO COMMENTS	I.B.	A.C.	23.04.24
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